AD NUMBER ADC018374 **CLASSIFICATION CHANGES** TO: unclassified FROM: secret LIMITATION CHANGES TO: Approved for public release, distribution unlimited FROM: Controlling DoD Organization: U.S. Naval Electronic Systems Command, Washington, DC 20360. **AUTHORITY** ONR ltr, 31 Jan 2006; ONR ltr, 31 Jan 2006

Y	4_3+7+8-fand fubilities-	~ *	-
	MOORED SURVEILLANCE SYSTEM FIELD VALIDATION	TEST	Γ
1	SENSOR PERFORMANCE ANALYSIS		
	WINDER, VERNIER RESOLUTION DATA PRODUCTS	(U) •	
1	VOLUME TIL	سيلا	
4	TO ANOTHORIO	77	7

SECRET (This page is UNCLASSIFIED.)

SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

REPORT DOCUMENTATION PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
1 REPORT NUMBER 2. GOVT ACCESSION NO	2. 3. RECIPIENT'S CATALOG NUMBER
MOORED SURVEILLANCE SYSTEM FIELD VALIDATION TEST SENSOR PERFORMANCE ANALYSIS. VELOCITE, VERNIER RESOLUTION DATA PRODUCTS (U)	final report. 10 JAN 77 - 31 MAR 78 FERFORMING ORG. REPORT NUMBER ARL-TR-78-3
Steven L./Watkins Judith L./Winterkamp	NOO039-77-C-0003
9 PERFORMING ORGANIZATION NAME AND ADDRESS	10. PROGRAM EL EMENT, PROJECT, YASK AREA & WORK UNIT NUMBERS
Applied Research Laboratories The University of Texas at Austin Austin, Texas 78712	Items 0003 and 0004
11. CONTROLLING OFFICE NAME AND ADDRESS	12 REPORT DATE
Naval Electronic Systems Command	31 December 1973
Department of the Navy	13. NUMBER OF PAGES
Washington, DC 20360 14 MONIYORING AGENCY NAME & ADDRESS(If different from Controlling Office)	403
	18. SECURITY CLASS. (of this report) SECRET
(14) ARL-TR-72-3	
	15. DECLASSIFICATION/DOWNGRADING
14. DISTRIBUTION STATEMENT (of this Report)	See reverse side
17. DISTRIBUTION STATEMENT (of the abetract entered in Block 20, of different fr	om Report)
18 SUPPLEMENTARY NOTES	
TAPIDLY ACROSTONITION OF TOVERS RIDE IT NECESSARY and Identify by block number rapidly deployable surveillance system	······································
moored surveillance system DIFAR	
(U) Volume III of this report contains the detailed resolution data products used to analyze candid formance based on the Moored Surveillance Systemetry. In addition, this volume contains a brie each type of display and the methods used to ge	vernier frequency ate sensor per- m Field Validation f diacussion of
	9 7

UNCLASSIFIED SECURITY CLASSIFICATION OF THIS PAGE(When Date Entered) 15a. DD 254, 12/10/76, Cont. NOO039-77-C-0003 CLASSIFIED BY OPNAVINST S5510.72C, 4 Sep 73 EXEMPT FROM GDS OF E.O. 11652 EXEMPTION CATEGORY 3
DECLASSIFIED ON 31 Dec 2007 *BATIONAL SECURITY INFORMATION* *Unauthorized Disclosure Subject to Griminal Sauctions Accession For NTIS GRALI DDC TAB Unannounced Justification_ Ву____ Distribution/ Availability Codes Avail and/or special Dist.

TABLE OF CONTENTS

	Page
LIST OF TABLES	v
LIST OF FIGURES	vii
I. INTRODUCTION	1
II. cw DATA PRODUCTS	3
III. AMBIENT SOUND FIELD DATA PRODUCTS	17
IV. DISCUSSION	21
REFERENCES	23
APPENDICES	25

(The reverse of this page is blank.)
UNCLASSIFIED

LIST OF TABLES

<u>Table</u>	<u>Title</u>	Page
III-1	Vernier Resolution Data Base (U)	4
III-2	Vernier Resolution Processing Parameters (U)	5
III-3	cw Projector Characterisitics for Vernier Resolution Data Products	6
III-4	Vernier Resolution Line History Plots	8
111-5	Vernier Resolution Propagation Loss or Signal, Noise, and Array Gain versus Range Plots	10
111-6	Vernier Resolution Probability of Detection versus Range Plots	12
III-7	Vernier Resolution Bearing Error versus Signal-To-Noise: Ratio Plots	14
8-111	Vernier Resolution Signal-To-Noise Ratio versus Range Plots	15
111-9	Lines Deleted from Clutter Measurements (U)	19

LIST OF FIGURES

Figure No.	Title	Appendix
III-1 - III-23	Summary Detection Curves (U)	A
111-24 - 111-163	Line History Curves (U)	В
III-164 - III-171	Propagation Loss versus Range Curves (U)	С
111-172 - 111-199	Array Gain versus Range Curves (U)	D
111-200 - 111-235	Percentage Detection versus Range Curves (U)	E
III-236 - III-257	Bearing Error versus Signal-to-Noise Ratio Curves (U)	F
111-258 - 111-293	Signal-to-Noise Ratio versus Range varves (U)	G
111-294 - 111-301	Noise Gain Timeseries Curves (U)	H
111-302 - 111-312	Clutter Timescries Curves (U)	I
111-313 - 111-354	Ambient Sound Field Level versus Frequency Curves (U)	J

(The reverse of this page is blank.)

UNCLASSIFIED

I. INTRODUCTION

- (C) During November 1975, the Moored Surveillance System (MSS) Field Validation Test (FVT) was conducted under the sponsorship of the MSS Project Office (PME 124-30) of Naval Electronic Systems Command.

 Applied Research Laboratories, The University of Texas at Austin (ARL:UT), participated in the processing and analysis of the acquired ACODAC data.
- (C) The results of this work, performed under Contract N00039-77-C-0003, are contained in a four volume report describing the measurements and analyses of candidate sensor performance based on data from the MSS-FVT. Volume I describes the data collection system and the measurement system used to obtain the results. Volume II contains data products obtained with standard frequency resolution processing. This volume, Volume III, contains the data products obtained with vernier frequency resolution processing. Volume IV contains the background information, summary data products, and analysis.
- (U) Since the MSS-FVT was completed, the name of the MSS program has been changed to Rapidly Deployable Surveillance System (RDSS). To avoid ambiguity, the term MSS will be used throughout this report. However, the issues addressed here are those specified by the MSS Project Office and are those issues that were of nurrent interest to RDSS at the time that this report was written.
- (U) This volume, III, which contains the detailed vernier frequency resolution data products, is partitioned into four sections. The first is this introduction. The second section describes the cw data products. The third section describes the ambient sound field (ASF) data products. The fourth and final section briefly discusses the utilization of these data products. Much of the text in this volume is similar to that found

(U) in Volumes I and II, but it is repeated here so that each volume can be used independently of the others.

II. cw DATA PRODUCTS

- (U) The detailed vernier frequency resolution cw data products contained in this volume were extracted from the data intervals shown in Table III-1. A summary of the processing parameters is shown in Table III-2. The cw projector characteristics used in performing these measurements are summarized in Table III-3. The cw projector source levels for the CFAV KAPUSKACING are higher than those reported previously (Ref. 1). These revisions were made in order to reconcile the propagation loss curves from the CFAV KAPUSKACING with those from the other sources. A detailed description of the measurement system can be found in Volume I.
- (C) Several different types of cw data products are contained herein.

 Each type is described briefly, and a table of the curves is given. The abbreviations used in these tables and the text are:
 - QT CFAV QUEST
 - KP CFAY KAPUSKACING
 - CH R/V CHAIN
 - Omnidirectional Sensor
 - SC Single Cardioids Sensor
 - MGL Maximum Gain Limacons Sensor
 - VD Vertical Dipole Sensor
 - DC Differenced Cardioids Sensor

These curves were included in this report to substantiate the observations in Volume IV, and to furnish a data base for future issues not addressed by this report. For completeness, each curve containing any data was included, even though the small number of samples may minimize its statistical significance.

(C)

TABLE III-1

VERNIER RESOLUTION DATA BASE (U)

Low Band (46 to 84 Hz) Single and Differenced Arrays

Site Al 12002 17 Nov[321] - 00392 18 Nov[322]

Site A2 1200Z 17 Nov[321] - 1859Z 17 Nov[321]

Site A3 1200Z 17 Nov[321] - 2359Z 21 Nov[325]

Midband (145-183 Hz) Single and Differenced Arrays

Site Al 12002 17 Nov[321] - 23592 17 Nov[321]

Site A2 1200Z 17 Nov[321] - 1859Z 17 Nov[321]

Site A3 1200Z 17 Nov[321] - 2359Z 17 Nov[321]

12002 21 Nov[325] - 2359Z 21 Nov[325]

High Band (300-338 Hz) Single Array

Site Al 12002 17 Nov[321] - 05292 18 Nov[322]

Site A2 12002 17 Nov[321] - 18592 17 Nov[321]

Site A3 | 1200Z | 17 Nov[321] - 2359Z | 21 Nov[325]

^[] Julian Day

I Greenwich Mean Time

SECRET

(S)

TABLE 111-2

VERNIER RESOLUTION PROCESSING PARAMETERS (U)

Value
100 Hz (obtained from zero crossings of tape servo signal)
46 to 84 Hz (low band) 145 to 183 Hz (midband) 300 to 338 Hz (high band)
81.92 sec (8192 samples)
Hanning
0.0122 Hz
0.0176 Hz
0.0183 Hz
50%
S min
Rectangular Integration
7
5.76
13.4
$1u_{-2}$
-14.6 dB//Hz

TABLE III-3

CM PROJECTOR CHARACTERISTICS FOR VERNIER RESOLUTION DATA PRODUCTS

	The Activity of the Sample, 7 - Sample Sampl	LINKLIKAL,	VOMINAL.	TY NOW FIFTED TVENT	10 1757	19 NOV FIELD EVENT	LD EVENT	21 NOV FIELD FVENT	ELD FVENT
	HOL	FREQUENCY	LEVEL	140/NO	NOW I KAL	ON/OFF	NOMINAL	ON/OFF	NCMINAL
7	PLATFORM	(Hz)	(dB//nba)	TIMES (2)	DEPTH (m)	TIMES (2)	DEPTH (m)	TIMES (2)	рерти (ш)
<u> </u>	λ×	<u>بر</u> بر	1.41	1230/2230	110	1224/2215	95	1217/2030	110
8	QUEST	155	134	1230/2230	011	1 1	,	1217/2030	110
		305	1.36	1230/2230	110	1224/2215	56	1217/2050	110
5	CFAV	79	162	1230/2318	110	1230/2230	115	1230/2030	120
<u> </u>	KAPUSKACING	160	- L	1230/2318*	110	; !	!!!	1230/2030	120
6	>	Ç	156	1525/2200	100	1225/2200	5	1230/2030	ن «۵
<u> </u>	CIMIN	170	156	1225/2200	100) i	1230/2030) oc
		355	154	1645/2200	100	1225/2200	56	1230/2030	85

*FREQUENCY VARYING 1 CYCLE

UNCLASSIFIED

- (\mathfrak{C}) Data products of the first type are termed summary detection plots (Appendix A, Figs. III-1 - III-23). These are plots of each detected line within a frequency band as a function of time. The solid symbols indicate that the line was detected in multiple cells and/or on multiple beams of the sensor. The X symbols indicate that the line was only detected in a single cell on a single beam of the sensor. The solid line emanating from each symbol indicates the maximum signal-to-noise ratio (S/N) of any cell of the line. If the sensor provides bearing information, the solid line also indicates the estimated bearing, norch being toward the top of the plot. The dashed lines indicate which of the detections were linked by the tracking algorithm. These displays are intended to provide qualitative information about the environment in which the processor must function in terms of line loading and relative clutter density between sensors and frequency regimes. More quantitative information will be found in section III of this volume.
- Data products of the next type (Appendix B, Figs. III-24 III-163) are (C) termed line history plots, and are cataloged in Table III-4. These are plots of the estimated aw signal parameter values as a function of time. The top portion of the plot contains a solid line indicating ground truth source-to-receiver range in nautical miles and X's indicating the number of equivalent degrees of freedom for each ALI. The second portion contains a solid line denoting ground truth receiver-to-source bearing, X's indicating the estimated signal bearing and D's indicating the estimated noise bearing. Caps in the solid ground truth lines indicate intervals of missing data, such as calibration signal intervals. The third portion contains the estimated ambient sound field (ASF) levels in $dB//\nu Pa/Hz^{1/2}$. The omnidirectional (0) and vertical dipole (VD) sensor curves contain a single trace of connected X's. The single cardioids (SC), maximum gain limatons (MGL) and differenced cardioids (DC) curves contain a trace for each beam. Each beam is labeled by the first letter of its main axis bearing (north, east, south, and west). ASF level estimates were displayed only when the signal was detected. The fourth portion of the plot contains the estimated sound pressure level (SPL) in dB//wPa of the received signal. The O and VD sensor curves each contain

TABLE III-4
VERNIER RESOLUTION LINE HISTORY PLOTS

1 1	_		т			_					
		٤	142	149	157	ž	153	161		;	
(325)	Site A3	5	£	148	156	Ş.	152	160	;	;	
21 NOV	Sit	92	141	147	155	143	151	159	145	163	
7		С	Ş	146	154	S.	150	158	144	162	
	-	2	Ę	134	133		:	:		:	
(323	Site A3	αΛ	9	133	137		;	i		:	
19 NOV (323)	Sit	SC	Ę	132	136	;	i	:	5	140	
 		0	8	131	135		;	ļ	5	1 39	
		Z	86	112	122	102	117	127	:	:	
		ΛD	86	111	121	103	116	126		;	
	Site A3	MGL	97	110	120	102	115	125	107	130	
	S	SC	96	109	119	101	114	124	106	129	
		0	95	108	118	100	113	123	105	128	
		2	63	76		89	81	91	:	<u> </u>	
(E)		ć,	Ş.	7.5	85	67	80	06	;	;	
17 NOV (321	Site A2	1321	29	74	Z	99	7.9	o:	7.1	56	
17 X	S	SS	61	73	83	65	78	80	70	93	
		0	9	72	82	49	11	87	69	6	
		ĸ	28	41	5.1	33	46	25		;	
		6	27	40	<u>ک</u> ر	3.2	25	55	:	;	
	Site A?	MGL VD	26	39	49	15	ग ग	3	36	89	
	S	R	25	38	48	30	43	53	35	28	
		0	5 2	37	4.7	39	7	25	ĸ	57	
	Source	Frequency	5.5	3	7.0	155	160	176	305	335	
	Source	Platform	5	2	5	ᅜ	Х	ъ	৳	ð	

W - Not Detect

Ξ

UNCLASSIFIED

- (C) two traces: the X's denote the levels for the cell with the highest S/N (most detectable); the +'s denote the levels summed over all detected cells, as is normally done when computing propagation loss. The SC, MGL, and DC sensor curves each contain four traces, each giving the levels for the most detectable cell on a beam and annotated in the same manner as the ASF levels. The fifth portion of the plot contains the S/N in decibels relative to a 1 Hz noise band. The traces are defined in the same manner as the SPL curves. The dashed line denotes the detection threshold. The bottom portion of the plot contains two traces: the X's denote the estimated signal frequency, and the \(\Pi's\) denote the line's bandwidth. These displays contain all of the information known about the signal. All of the remaining cw data products are derived from these data.
- (C) is to products of the next type (Appendix C, Figs. III-164 - III-171) are termed propagation loss plots, and are cataloged under the O sensor columns of Table III-5. These plots contain curves of the estimated cw propagation loss in decibels as a function of range in nautical miles. Below these are other traces denoting the associated signal excess, (S+N)/N, at each range bin in decibels relative to the noise level in the analysis bandwidth. These traces indicate the confidence associated with the measurements. The bottom traces denote the estimated background ASF levels associated with each range bin. These measurements were derived for a 1 nmi range bin, and smoothed with a 3-bin sliding average. The received signal power was estimated from that cell with the highest S/N of any detected cell on any beam. Since these are single cell measurements, they will show more loss than the total received SPL technique, such as was used in Ref. 2. This difference is discussed in Volume IV.
- (C) Data products of the next type (Appendix D, Figs. III-172 III-199) are termed signal, noise, and array gain plots, and are cataloged in Table III-5 under the sensors other than O. These are plots of measured

TABLE 111-5

	•			į				17 %	17 208 (321	(1)							61	Š	19 NOV (323)		21	21 NOV (325)	(323)	
UTCO	Source		S	Sire Al				S	Site A2	2			Si	Site A3		-		Site A3	A3.	 		Site A3	15	
tform	form Frequency	0	8	KCL	ç	×	٥	ß	MCL	Z GX	يخ	0	ည	NGL NGL	αN	٤	0	SC	1	×	C	3.		۲
5	\$5	164	172	173	174	175	2	172	173	NO T	17.5	164	172	173	174	175	ę	8	î.	Ş	S	_~	1	175
3	3	165	176	177	178	6:1	165	176	177	178 179		165	176	177	178	179	165	176	178	179	165	176	178	179
ă	7.0	3	166 160 187	181	162	183	991	180	181	182 183		166	180	181	182	183	991	180	182					183
5	55. 10.	157	7	185	186	187	167	184	185	186 18	187	167	184	185	186	187	1:	;		+	} 9	124	5	Ę
 5	091	991	185	189	190	191	168	188	189	190 191	—-	168	188	189	190	191	;	;	:					5 5
ñ	170	169	192	193	154	195	169	192	193	194 195		169	192	193	194	195	;	;	i	·				195
٦	305	170	196 197	197		1	170	19%	197		 	170	196	197	1	1	2	2		+-	j	ŀ	1	
ř	135	171	198	199	;	;	171	193	199	:		171	198	199	1	:	171	198						:
																								_

ND - Not Detected

3

UNCLASSIFIED

- (C) sensor signal, noise, and S/N levels relative to those of an omnidirectional sensor (0) as a function of range. The top portion of the plot indicates how many samples (0 sensor detections) occurred in each range bin. The next portion contains traces denoting the measured signal gain of the sensor, where signal gain is the ratio of the received SPL of this sensor over that of the 0 sensor. The next portion contains traces denoting the measured array gain of the sensor, where array gain is the ratio of the S/N of this sensor over that of the 0 sensor. The bottom portion contains traces denoting the measured noise gain of the sensor, where noise gain is the ratio of the ASF level of this sensor over that of the 0 sensor. Since signal gain is primarily a function of range, whereas noise gain is a function primarily of time, this display allows array gain to be interpreted in terms of both range and time. All of the traces were computed with 1 nmi range bins and smoothed with a 3 nmi sliding average.
- (C) When computing average S/N as a function of range, if the signal is not detected during every LLI, the resultant average will be biased high. This bias occurs because only the highest S/N ratios are detected. In order to reduce this bias, the detection threshold (Table III-2) has been substituted for the missing S/N wherever the target was not detected. This debiasing technique was used both for computing array gain and for generating curves of S/N versus rarge.
- termed percentage detection plots, and are cataloged in Table III-6.

 These curves of single line defection percentages were calculated as the number of independent detection opportunities (ALI intervals) that the specified source was within a given integer 1 mile range interval and that resulted in detection, divided by the number of such opportunities. For multibeam sensors, detection on any beam was considered a detection for the sensor. If the number of equivalent degrees of freedom for an ALI was less than that specified in Table III-2 (some portion of the ALI interval was missing), and the signal was not detected.

		٤	204	217	227	Ş.	222	232	-	:	
(325)	Site A3	Ş	5	216	226	2	221	231	;	:	
NON	Sit	ۍ.	201	214	224	206	219	229	211	234	
21		c	Ş	213	223	Š	218	228	210	233	
		ع	Ş	217	227		;	;	;	;	
NOV (323)	Site A3	6	Š	216	226	;	į	:		ţ	
VON 61	Sit	SC	Ş	214	224	;	:	1	2	234	
_		0	윷	213	223	:	;	:	Š	233	
		S.	204	217	227	509	222	232	;	:	
	₩.	ć,	203	216	226	208	221	231	!	:	
	Site A3	MCI.	202	215	225	202	220	230	212	235	
	S.	SC	201	214	224	206	219	229	2112	234	
		C	200	213	223	202	218	228	210	233	
		٤	204	217	227	505	222	232	;	;	
21)	7	G.	Q.	216	326	208	221 222	231	;	;	
17 NOV (321	Site A2	7. 1.1.	202	215	225	207	220	230	212	235	
7	S	Sc	201	214	224	206	219	229	211	234	
		0	700	213	223	205	218	228	210	233	
		Z	204	217	227	209	222	232	:	;	
		MGL VD	203	216	226	208	221	231	:	;	
	Site Al	TOX.	202	215	225	202	220	230	212	235	
	5	Š	201	214	224	206	219	229	211	234	
		0	200	213	223	205	218	228	210	233	_
	Source	Frequency	\$\$	I	7.0	551	160	170	305	\$35	
	Source	latform	5	<u>a</u>	ō	٦	6	ð	5	õ	

ND - Not Detected

â

12 UNCLASSIFIED

- (C) then the ALI was not counted as a valid detection opportunity. These editing criteria were required because the detection threshold for each ALI was determined by its number of degrees of freedom. All of the traces were smoothed with a 3 nmi sliding average. If the sensor furnished a bearing estimate, its rms bearing error was also plotted as a function of range.
- are termed bearing error plots, and are cataloged in Table III-7. These are curves of the number of bearing estimates (detections), the mean bearing error (estimated bearing minus ground truth bearing), the rms bearing error, and the bearing error standard deviation, all plotted as a function of S/N in dB//1 Hz noise band. The ground truth bearing was computed from the navigation reconstruction as the great circle receiverto-source bearing at the receiver and at the beginning of the ALI. The estimated bearings were corrected for magnetic variation and acoustically debiased (see Volume I). Each trace was smoothed with a 3 dB sliding average.
- (C) Data products of the last type (Appendix G, Figs. III-258 III-293) are curves of S/N (dB//1 Hz noise band) versus range (nmi), and are cataloged in Table III-8. These measurements were obtained from the detected cell with the highest S/N on any beam. As described earlier, these results are partially debiased by substitutions of the detection threshold during ALI intervals without signal detections. The detection threshold is drawn on each plot. Each trace was smoothed with a 3 nmi sliding average.

VERNITR RESOLUTION BEARING LIREAR VERSUS STGMAL-TO-NOTS. RATTO PLOTS

TABLE 111-7

	_									
		` `	238	246	252	£	249	255	1	;
5	Site A5	Î,	;	;	;	;	;	:		:
(\$2.5) NOV 12	511	SC 1/1) 1K.	236	244	250	239	247	253	242	256
~·. 		=!	i	:	;	;	:	;	:	:
		2	ĝ	246	252	:	:	:	1	;
(323	Site A3	SC VI) DC	:	;	252	;	;	;	;	:
19 NOV (323)	Sit			244	250	;	;	1 1	S	256
		=		:	;	;	;	;		1
		Ë		246	252	241	249	255	:	1 1
!	₩.	V) DC.	:	;	;	;	•	•	;	;
1	Site A3	 	237	245	251	240	248	254	243	257
i	 	Si	236	244	250	239	247		242	256
1		٦	236	:	:	::	:	253		-
!		MC), VI) INC.	238	246	252	241	249	255		:
21).	ابہ	ş	238	246	252	241	249	255	:	:
2	ite.	Ž,	237	24.5	251	240	248	254	243	257
17 NOV (321	Site A?	Ŋ.	236	244	250	239	247	253	242	256
l L	1	c	; ;	:	:	;	:	:	:	! !
1		Ä	238	246	252	24!	249	255	;	;
	_	\$:	:	;	1	:	;	;	;
	Site Al		237	245	251	240	248	254	243	257
1	55	×	 24.	244	250 251	239 240	247 248	253	242 243	256 257
i	_	0	:	:	;		:	;	;	:
	Source	ora Frequency o SC Mil VD	17	3	7.0	155	160	170	305	335
	-				ĺ					

ND - Not Detected

5 5 5 5 5 5 5

TABLE III-8
VERMIER RESOLUTION SIGNAL-TO-NOISE RATIO VERSUS RANGE PLOTS

ļ	7		: :	<u>.</u>		?	285	ŝ		i i	٠ ٠	, :	· !
!	3	Sire 13			à i	7	₹ X	C.	27.0	, ,	7	;	:
1	21 NOL (325)	2		f, 8			z.	264	1.		ė,	269	29.2
			: -	: : :			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	G.X.		, ,	0	890	167
İ			ļ	: : 5				:	:		. !		:
1 1	19 NOV (323)	Site 43	ŝ	! 5				;			:	:	
		J	S	2				-	:		:	ż	
		_	c	;				:	;	,	!	Š	
		i	VP PC	262	375			26.7	280	290	-	:	
!		٠	C.		, ,			265	279	8.3		;	:
		51 Cc .73	ACT.	259 260	5.73			265	278	288		270	293
			SC			50 50		204	277	28.7	İ	269	262
			٥	258	271	781		263	276	385	<u> </u>	268	162
		i	2	262	274 275	284 245		26h 267	279 280	269 290		:	:
321)] 2	;	5	G.	274		1	264	9:1	269	ļ	:	;
17 NOV (321	51.5		12.1	260	2.3		-	50.	278	268		היים	293
17			×	259	272	282		104	17.7	. 66		506	292
	 	-		258	77	281	 	263	3,76	386	-	30.5	20.1
!		F.	Z	262	275	285		26.	280	290		;	
	7	1		761		183 184	1	365 366	ς. 1.	289	i	;	
	Site Aj		756.6	760	13.5			505	100 7	-		0.	,
	•	1	<u>اي</u>	259		40	!	3	**	33	-	169	6.
		c	,	\$5.	<i>:</i> .	**		9	Ĭ,	186		*0	6
	Source	A Property of		\$ 5	73	۶	:	55.	160	0.1		505	N 19
:	Source	Flatform		5	\$	5		 	ù	č		- ·	č

. Not Defecte

3

(The reverse of this page is blank.)
UNCLASSIFIED

III. AMBIENT SOUND FIELD DATA PRODUCTS

- (U) Three types of ambient sound field (ASF) measurements were performed: sound pressure levels at an omnidirectional sensor, noise gains of directional sensors, and clutter (processor loading) statistics of each sensor. The vernier frequency resolution ASF data products herein span an interval of 4 1/2 days, but have limited frequency coverage. The standard frequency resolution ASF data products in Volume II cover a wide frequency range (40 to 600 Hz), but are of only 12 hours duration. Each data product set can be used to extrapolate the other to different frequencies or times.
- (U) Data products of the first type (Appendix H, Figs. III-294 III-301), are termed timeseries plots, and reveal the time dependence of the ASF measured in selected 1 Hz bands. The first three figures contain the omnidirectional ASF levels (dB//µPa/Hz^{1/2}) in each vernier band. The remaining figures contain the noise gains (dB) where noise gain is the ratio of the ASF level of this sensor over that of the omnidirectional sensor. These timeseries plots were derived from ASF meaurements summed over 1 Hz bands. The noise gains were derived for a 1 Hz band which was relatively free from contamination by tonals. The 1 Hz summation increased the number of equivalent degrees of freedom, and thus decreased the variance of the measurments.
- (C) Data products of the second type (Appendix I, Figs. III-302 III-312), are termed clutter timeseries plots. These are plots of the number of detected cells, the number of lines formed, and the number of lines linked, for each ALI interval as a function of time. These measurements were obtained during field events only, and a separate curve is provided for each such event. The measurements were performed for three contiguous 10 Hz bands of 819 cells each. The results for each band were similar and have been combined into a single 30 Hz band for these curves.

7

- The clutter timeseries plots are intended to portray the shore link and processor capacity required for operations in the absence of targets. In order to provide accurate clutter measurements, it is necessary to first eliminate the loading incurred due to the presence of the exercise vessels and projectors. Table III-9 lists those lines which have been deleted from the clutter measurements, along with their probable source.
- (U) Data products of the last type (Appendix J, Figs. III-313 III-354), are termed 3D plots. These are 3-dimensional representations of omnidirectional ASF levels (dB//\pa/Hz^{1/2}) as a function of time and frequency. Each trace represents the average over a 10 min interval and has been smoothed so as to maintain a constant number of equivalent degrees of freedom. Plots of data from the vertical dipole sensor are also included. These displays serve as a roadmap of the data since they reveal signatures, tones, artifacts, and broadband trends.

(C)	TABLE	111-9

LINES DELETED FROM CLUTTER MEASUREMENTS (U)

LOW FREQUENCY VERNIER (50 to 80 Hz)

55 Hz Scheduled QUEST Projector Line 64 Hz Scheduled KAPUSKACING Projector Line

70 Hz Scheduled CHAIN Projector Line

76 Hz ARL: UT Translator Artifact

79 Hz ARL:UT Translator Artifact

MIDFREQUENCY VERNIER (150 to 180 Hz)

155 Hz Scheduled QUEST Projector Line

160 Hz Scheduled KAPUSKACING Projector Line

170 Hz Scheduled CHAIN Projector Line

HIGH FREQUENCY VERNIER (305 to 335 Hz)

305 Hz Scheduled QUEST Projector Line

320 Hz KAPUSKACING Projector Harmonic (5×64 or 2×160)

324 Hz KAPUSKACING Projector Sum Frequency (64+260)

335 Hz Scheduled CHAIN Projector Line

(The reverse of this page is blank.)

CONFIDENTIAL

IV. DISCUSSION

- (U) The analysis of these data is contained in Volume IV. However, a brief discussion of some of their limitations may prevent those readers not having access to Volume IV from drawing unwarranted conclusions.
- (C) The curves in this volume denote the estimated averages of complex stochastic processes. The estimates are displayed as a function of a single variable, such as range, even though they may be highly dependent on another variable, such as the time dependence of S/N or array gain. The signal, noise, and array gain displays allow the time and range dependencies to be somewhat separated, whereas the percentage detection and S/N versus range displays do not. Even though the propagation loss and signal, noise, and array gain displays separate the time dependence of the ASF from the range dependence of the signal field, they do not isolate the time dependence of the signal field. However, since these curves are in good agreement for all three data intervals at Site A3, the day-to-day time dependence of the signal field, as observed with a 5 min ALI, is probably small.
- (U) Since the curves are estimated averages of complex stochastic processes (assumed to be stationary in a wide sense), the variance of these estimates is highly dependent on the number of sample measurements. For most of the cw curves, and particularly for the lower level signals, the number of samples is small (<10). The variance of each curve has been decreased by a smoothing window which effectively tripled the number of samples in each bin, but also decreased the resolution of the curve. However, the statistical fluctuation of these estimates does not entirely account for the apparently anemalcus results from the low level signals. As is discussed in Volume IV, these results are sometimes severely biased. This is because a fixed threshold detection process

- (U) was used to extract signal measurements, and thus only that portion of the signal SPL distribution lying above the threshold was used to estimate its average. For the higher level sources, more of the SPL distribution was detected and used to estimate its average. As was discussed earlier, a simple technique was used to partially debias the S/N results.
- (C) The results that appear most anomalous are those at 55 Hz, where the entire SPL distribution is undetectable. The 55 Hz detections occurred only when the ASF level in the signal cell exceeded the estimated ASF mean level sufficiently that it forced the signal-plus-noise level above the detection threshold. This results in erroneous cw measurements (Ref. 3). This phenomenon is discussed more fully in Volume IV. (pp. 62-65).

REFERENCES

- Steven L. Watkins, "MSS/FVT cw Projector Reconstruction," Applied Research Laboratories Technical Report No. 76-16 (ARL-TR-76-16), Applied Research Laboratories, The University of Texas at Austin, October 1976. UNCLASSIFIED
- 2. Steven L. Watkins, "MSS/FVT Ambient Sound Field and cw Propagation Measurements for Near-Bottom Sensors at Site A3" (U), Applied Research Laboratories Technical Report No. 76-52 (ARL-TR-76-52), Applied Research Laboratories, The University of Texas at Austin, December 1976. CONFIDENTIAL
- 3. Jack A. Shooter and Steven L. Watkins, "Estimation of Background Ambient Noise Level from the Spectral Analysis of Time Series with Application to cw Propagation Loss Measurements," J. Acoust. Soc. Am. 62, 84-90 (1977). UNCLASSIFIED

APPENDIX A

SUMMARY DETECTION CURVES (U)

(FIGURES III-1 - III-23)

(The reverse of this page is blank.)
UNCLASSIFIED

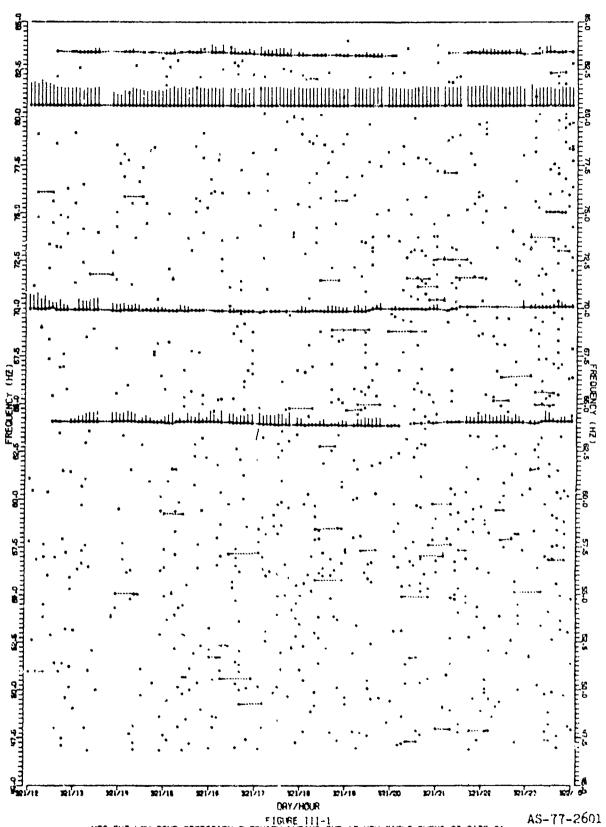


FIGURE 111-1

BSS-FVT LON-BAND DETECTION OVERVIEW DURING THE 17 NOV FIELD EVENT AT SITE AL

OBTRINGO VIA THE OMNIDIRECTIONAL SENSOR WITH VERNIER RESOLUTION (U)

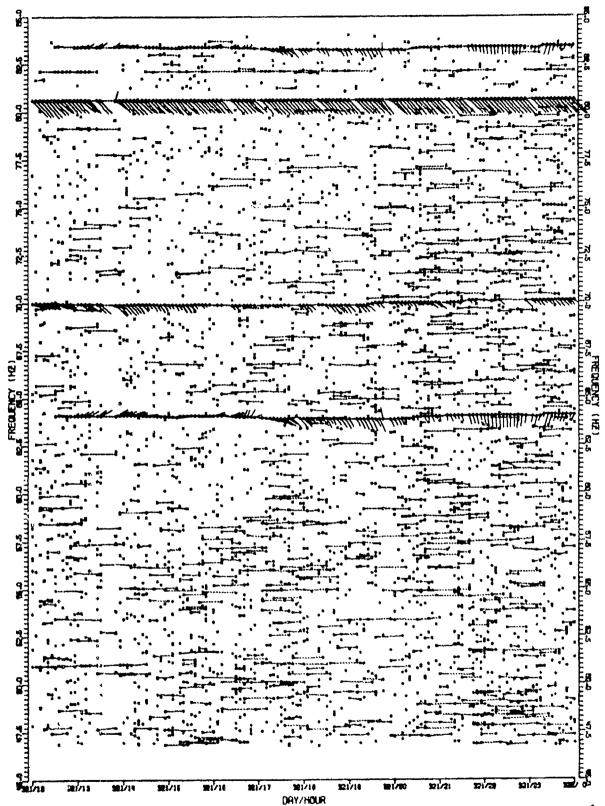


FIGURE 111-2

MSS-FVT LON-BAND DETECTION OVERVIEW DURING THE 17 NOV FIELD EVENT AT SITE AT OBTAINED VIA THE SINGLE CARDIOLOS SENSOR WITH VERNIER RESOLUTION (U)

AS-77-2602

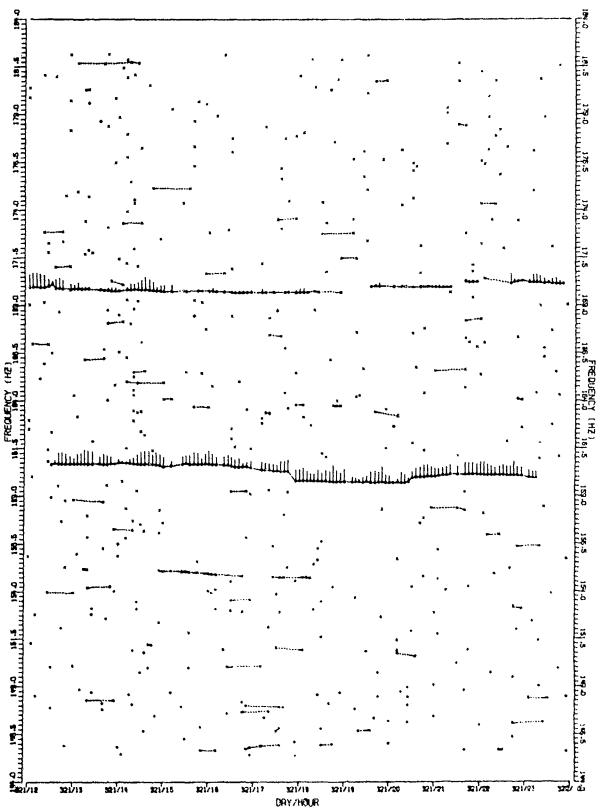


FIGURE 111-3

NSS-FVT HID-BAND DETECTION OVERVIEW DURING THE 17 NOV FIELD EVENT AT SITE AL AS-77-2603

OBTAINED VIA THE CHNIDIRECTIONAL SENSOR WITH VERNIFE RESOLUTION (U)

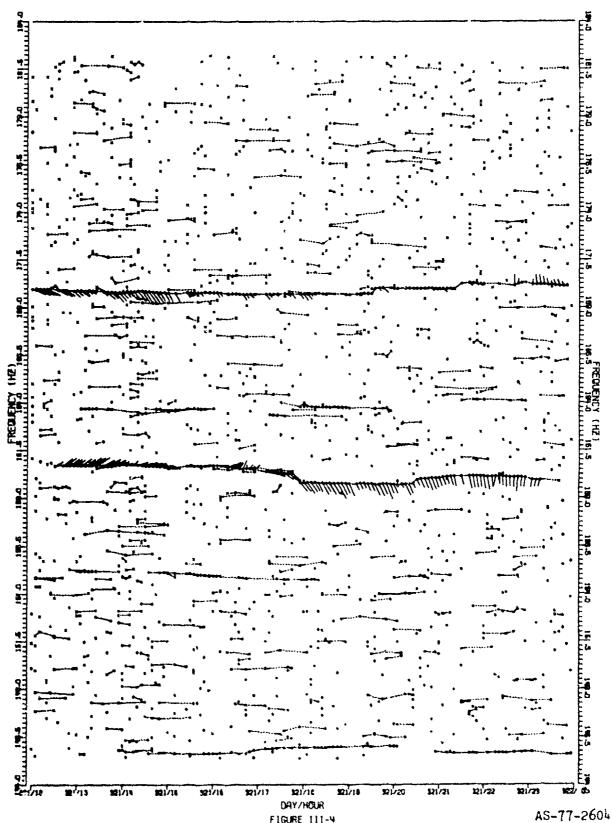


FIGURE 111-4
MSS-FVT MID-BAND DETECTION OVERVIEW DURING THE 17 MOV FIELD EVENT AT SITE AT OBTAINED VIA THE SINGLE CARDIDIOS SENSOR WITH VERNIER RESOLUTION (U)

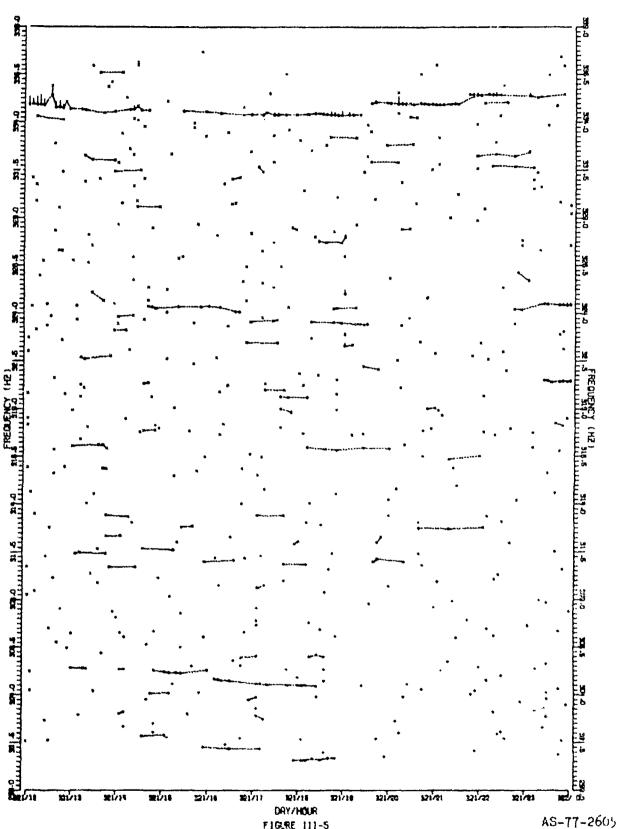


FIGURE 111-5
HSS-FVT HIGH-BAND DETECTION OVERVIEW DURING THE 17 NOV FIELD EVENT AT SITE AT OBTAINED VIA THE OWNIDIRECTIONAL SEASOR WITH VERNIER RESOLUTION (U)

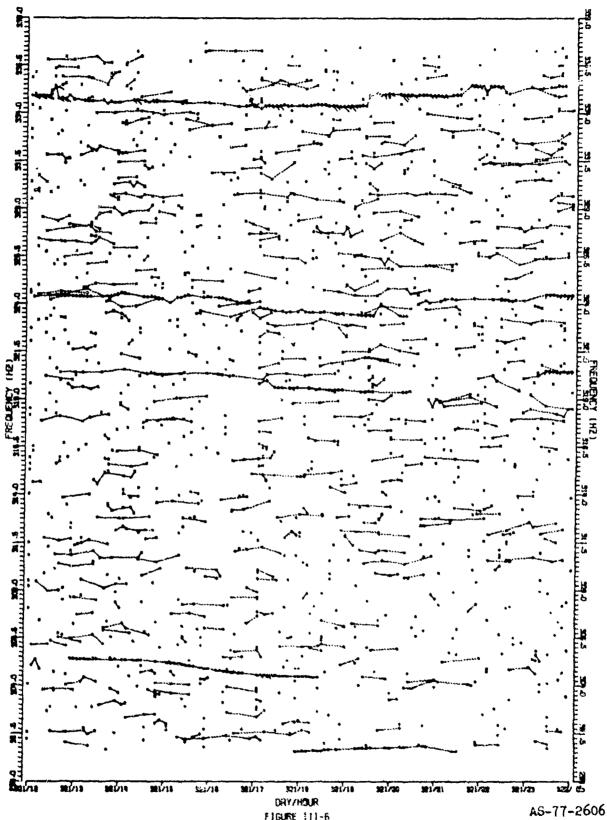


FIGURE 111-6
MSS-FYT HIGH-BAND DETECTION OVERVIEN DURING THE 17 NOV FIELD EVENT AT SITE AL
OBTAINED VIA THE SINGLE CARDIOLOS SENSOR MITH VERNIER RESOLUTION (U)

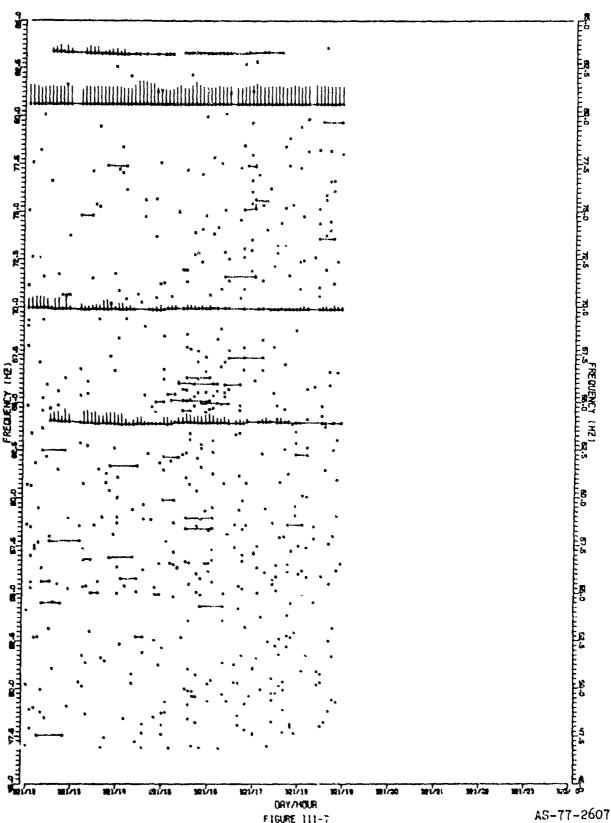


FIGURE 111-7

NSS-FVT LON-BAND DETECTION OVERVIEW DURING THE 17 NOV FIELD EVENT AT SITE R2

OBTAINED VIA THE OHNIDIRECTIONAL SENSOR WITH VERNIER RESOLUTION (U)

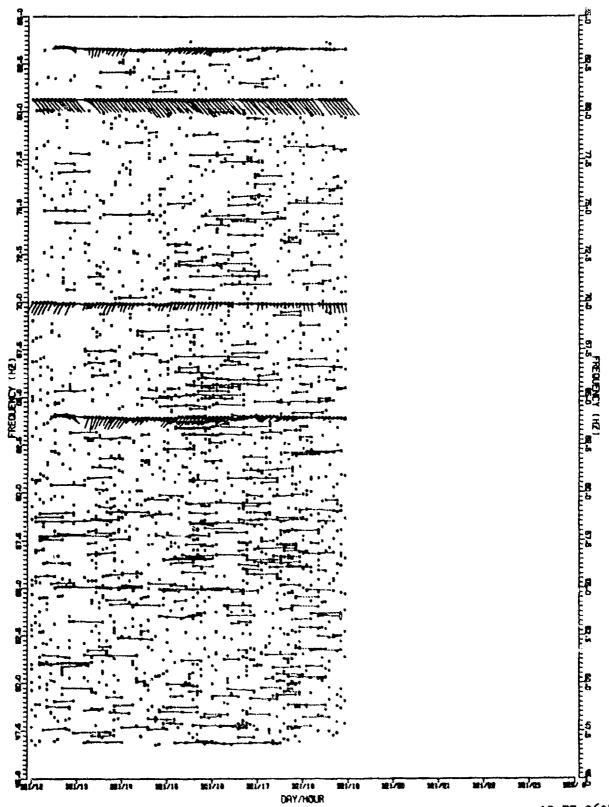
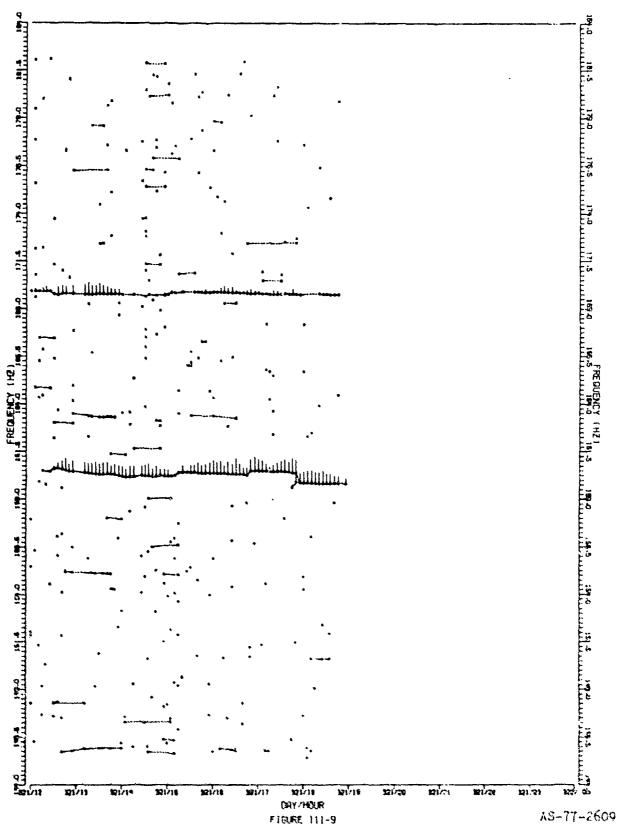


FIGURE 111-8

RSS-FVT LON-BOND DETECTION OVERVIEW DURING THE 17 NOV FIELD EVENT AT SITE AZ
OBTAINED VIA THE SINGLE CARDIOLOS SENSOR WITH VERNIER RESOLUTION (U)



Control of the second of the s

FIGURE 111-9

MSS-FVT NID-BRAD DETECTION OVERVIEW DURING THE 17 NOV FIELD EVENT AT SITE R2

DOTAINED VIR THE OMNIDIRECTIONAL SENSOR WITH VERNIER RESOLUTION (U)

CONFIDENTIAL

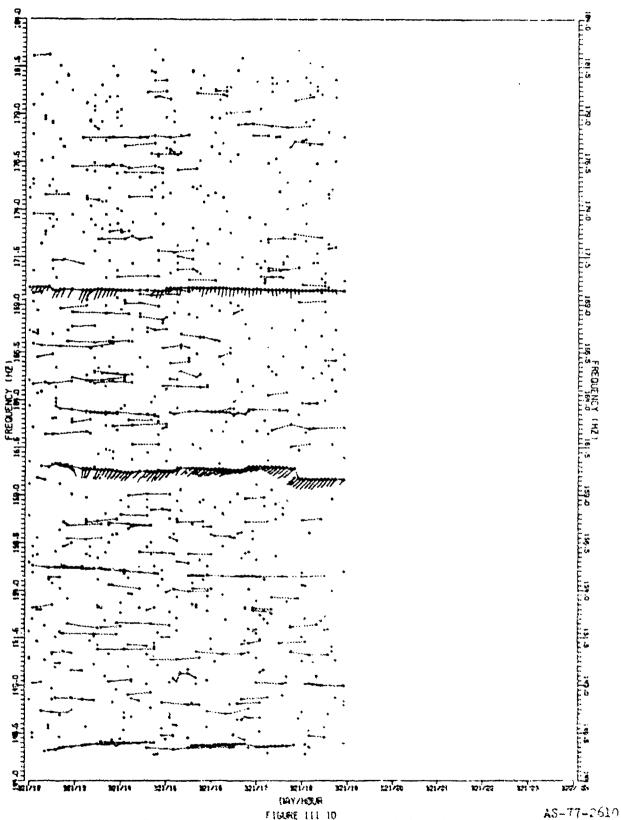


FIGURE 111 10
MSS-FYT MID-BRUD DETECTION OVERVIEW DURING THE 17 MBV FIELD EVENT RT SITE RE
ORTHINED VIA THE SINGLE CREDIDIDS SENSOR WITH VERNIER RESOLUTION (1)

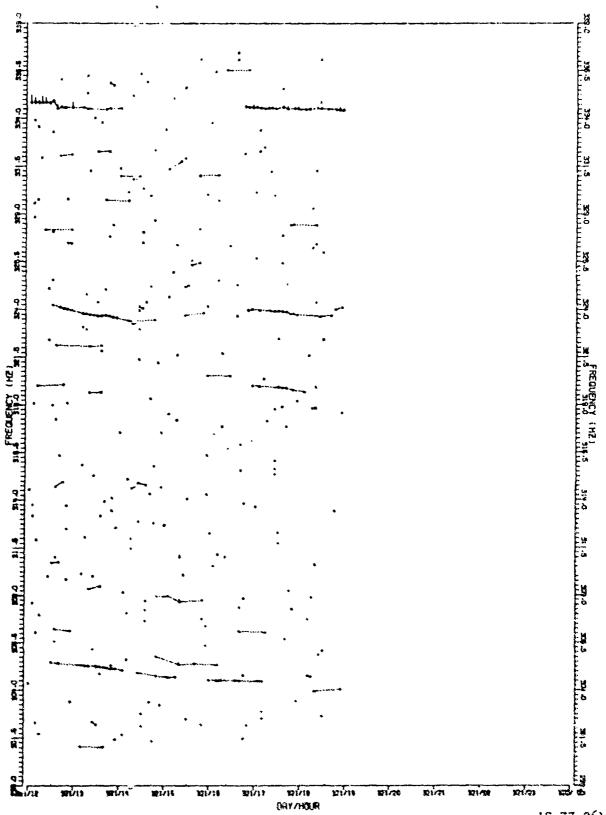


FIGURE 111-11

AS-77-2611

HSS-FVT HIGH-STARD DETECTION OVERVIEW DURING THE 17 NOV FIELD EVENT RT SITE R2

AD-PINED VIR THE OMNIDIRECTIONAL SENSOR WITH VERHIER RESOLUTION (11)

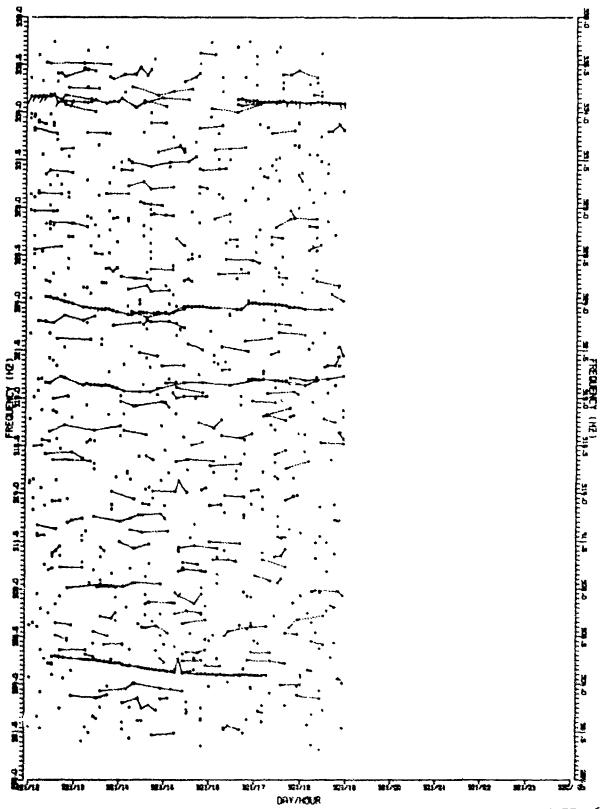
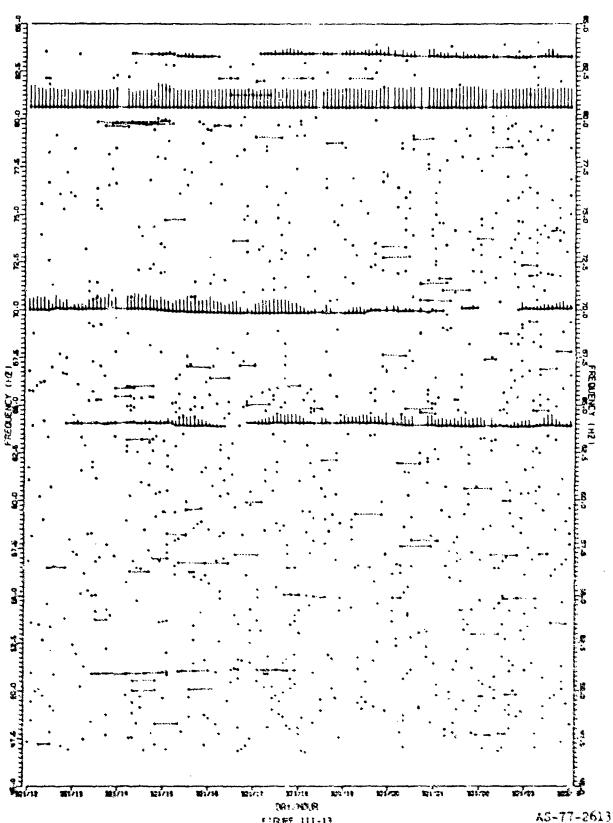


FIGURE 111-12

MSS-FVT HIGH-BAND DETECTION OVERVIEW DURING THE 17 NOV FIELD EVENT AT SITE A2

OBTAINED VIA THE STAND F CARRATORIES SEARCH WITH VERMIER RESOLUTION (III)

AS-77-2612



FIGHE 111-13

MSS-FVT LOW-DAND DETECTION OVERVIEW (MAINS THE 17 MSV FIELD EVENT AT SITE AS DETRINED VIA THE COMMIDINECTIONAL SERIOR WITH VERNIEU RESOLUTION (1))

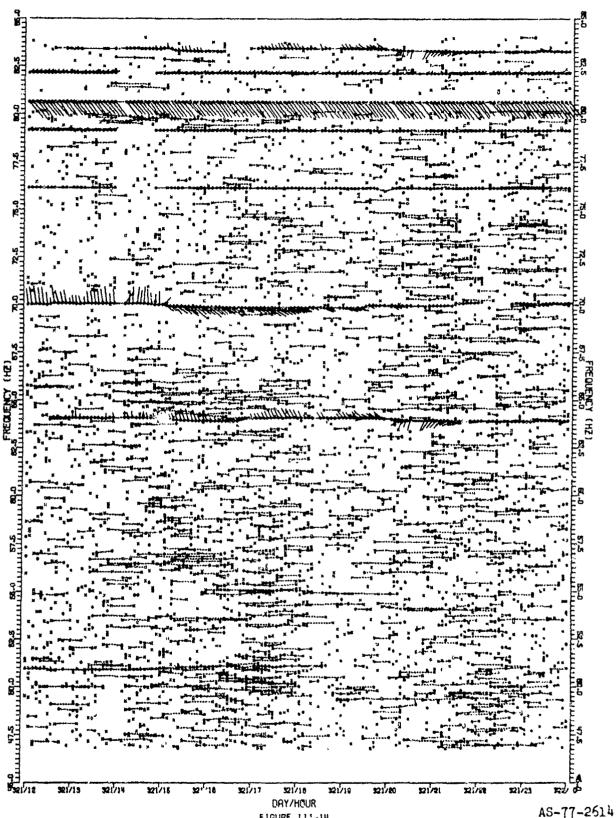


FIGURE 11'-14
MSS-FVT LON-BAND DETECTION OVERVIEW DURING THE 17 NOV FIELD EVENT AT SITE AS OBTAINED VIA THE SINGLE CARDIDIOS SENSOR WITH VERNIER RESOLUTION (U)

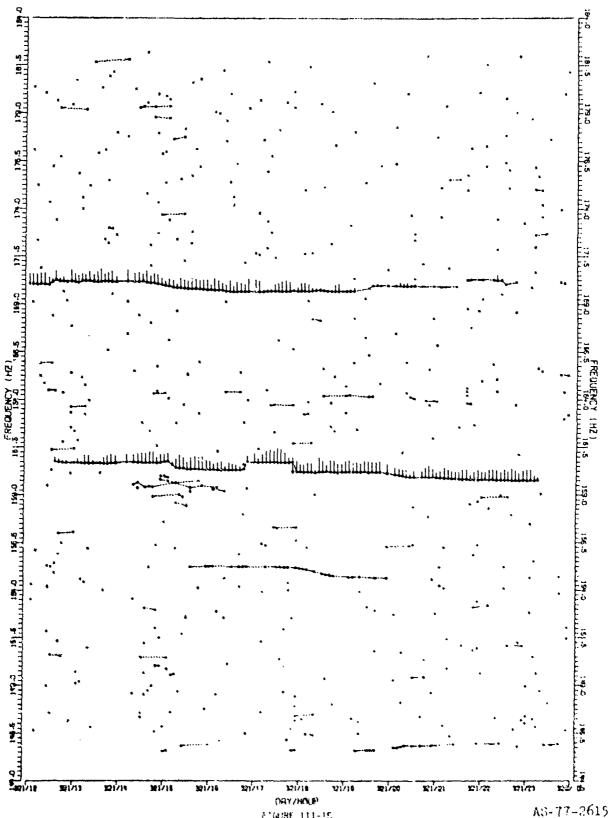


FIGURE 111-15

MSS-FVT MID-BRND DETECTION OVERVIEW DURING THE 17 NOV FIELD EVENT AT SITE AS

OBTAINED VIA THE OMNIDIRECTIONAL SENSOR WITH VERNIER RESOLUTION (U)

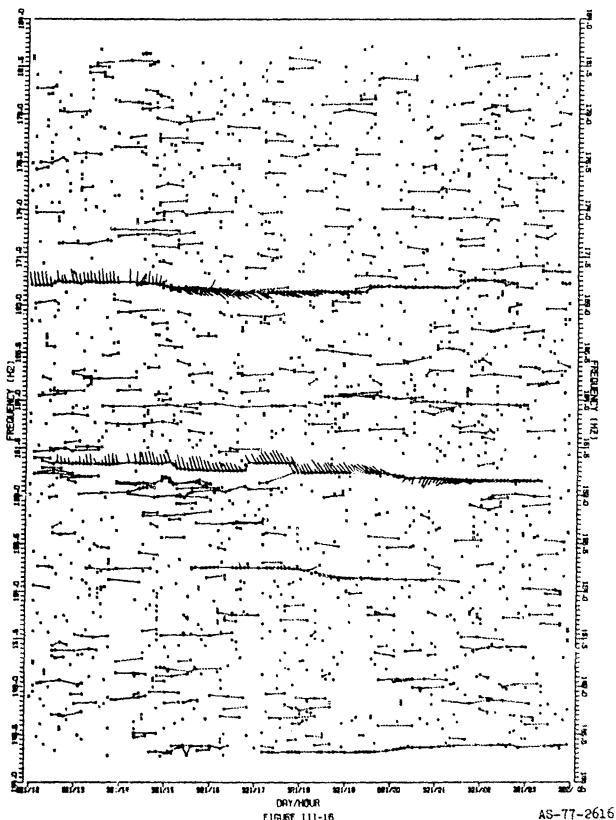


FIGURE 111-16

MSS-FVT HID-BAND DETECTION OVERVIEW DURING THE 17 MOV FIELD EVENT AT SITE AS OBTAINED VIA THE SINGLE CARDIDIOS SENSOR WITH VERNIER RESOLUTION (U)

CONFIDENTIAL

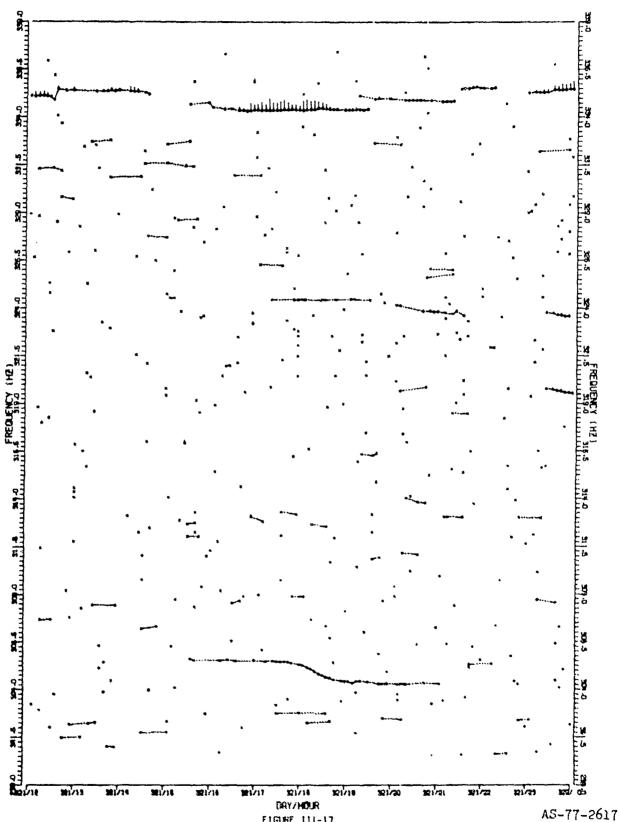


FIGURE 111-17

NSS-FVT HIGH-BAND DETECTION OVERVIEN DURING THE 17 NOV FIELD EVENT AT SITE R3
COTAINED VIA THE ONNIDIRECTIONAL SENSOR WITH VERNIER RESOLUTION (U)

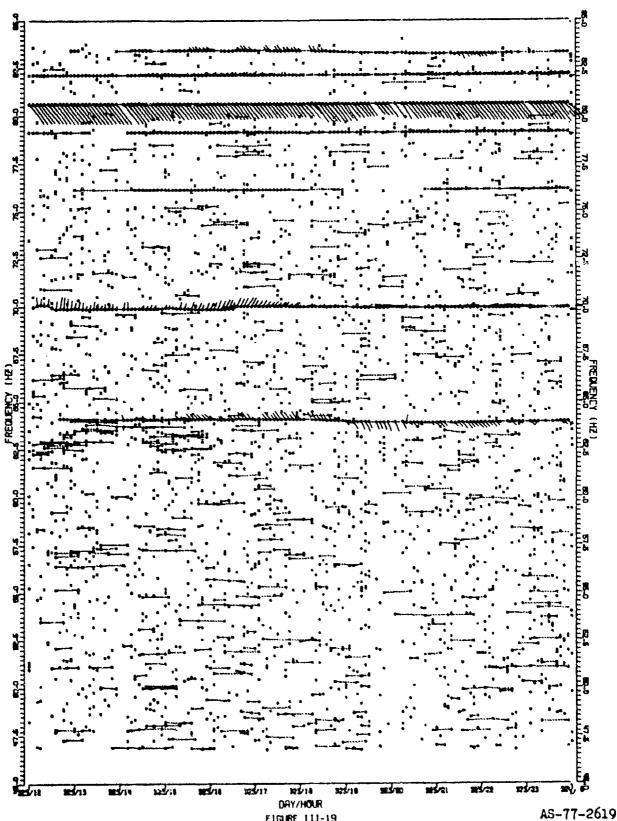


FIGURE 111-19
RSS-FVT LON-BAND DETECTION OVERVIEW DURING THE 19 NOV FIELD EVENT AT SITE A3
OBTAINED VIA THE SINGLE CARDIOLOS SENSOR WITH VERNIER RESOLUTION (U)

CONFIDENTIAL

The state of the s

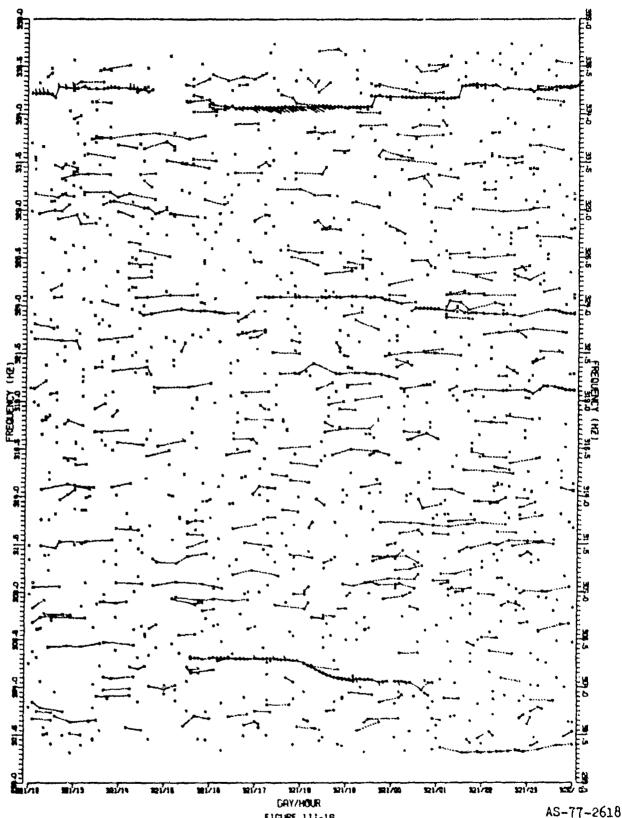


FIGURE 111-18

MSS-FVT HIGH-BAND DETECTION OVERVIEW DURING THE 17 NOV FIELD EVENT AT SITE AS
OBTAINED VIA THE SINGLE CARDIOLOS SENSOR HITH VERNIER RESOLUTION (U)

CONFIDENTIAL

1 N. C.

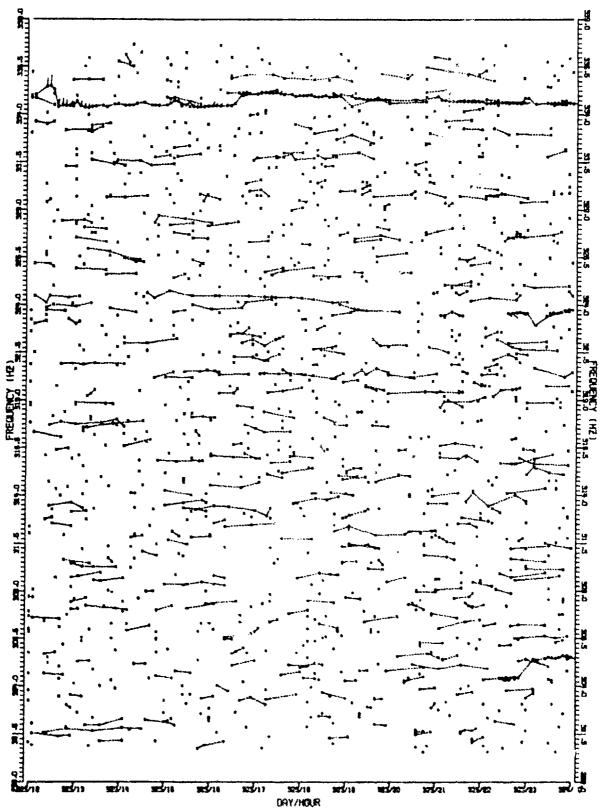


FIGURE 111-20
MSS-FVT HIGH-BAND DETECTION OVERVIEW DURING THE 19 MOV FIELD EVENT AT SITE AS
OBTAINED VIA THE SINGLE CHARDIOIDS SENSOR WITH VERNIER RESOLUTION (U)

AS-77-2620

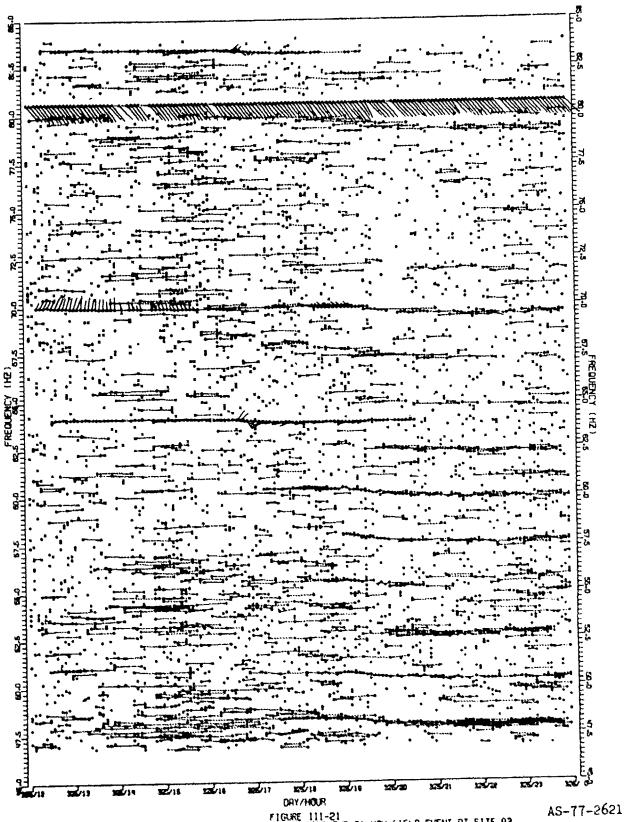


FIGURE 111-21

MSS-FVT LON-BAND DETECTION OVERVIEN DURING THE 21 NOV FIELD EVENT AT SITE A3

OBTAINED VIA THE SINGLE CARDIDIDS SENSOR WITH VERNIER RESOLUTION (U)

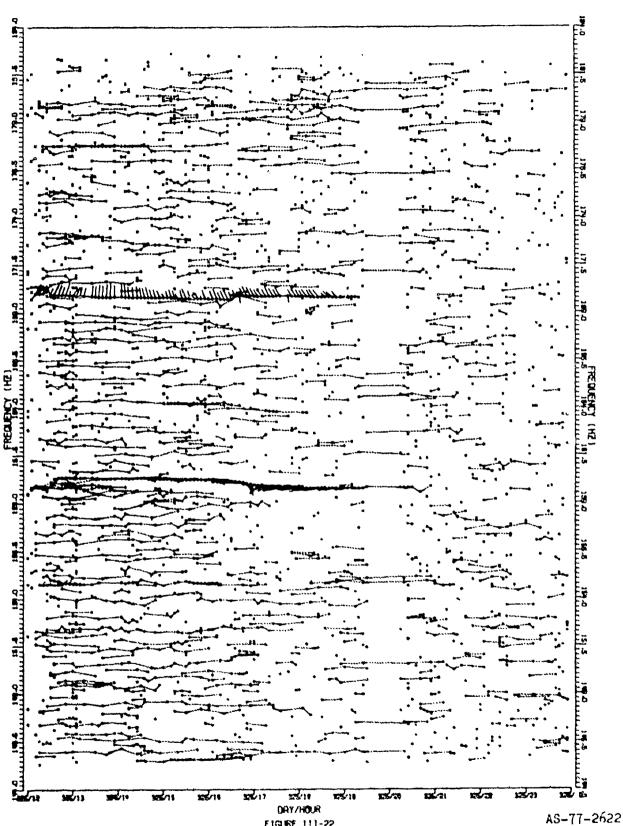


FIGURE 111-22

MSS-FVT MID-BAND DETECTION OVERVIEN DURING THE 21 MOV FIELD EVENT AT SITE AS OBTAINED VIA THE SHALE CARDIDIDS SENSOR WITH VERNIER RESOLUTION (U)

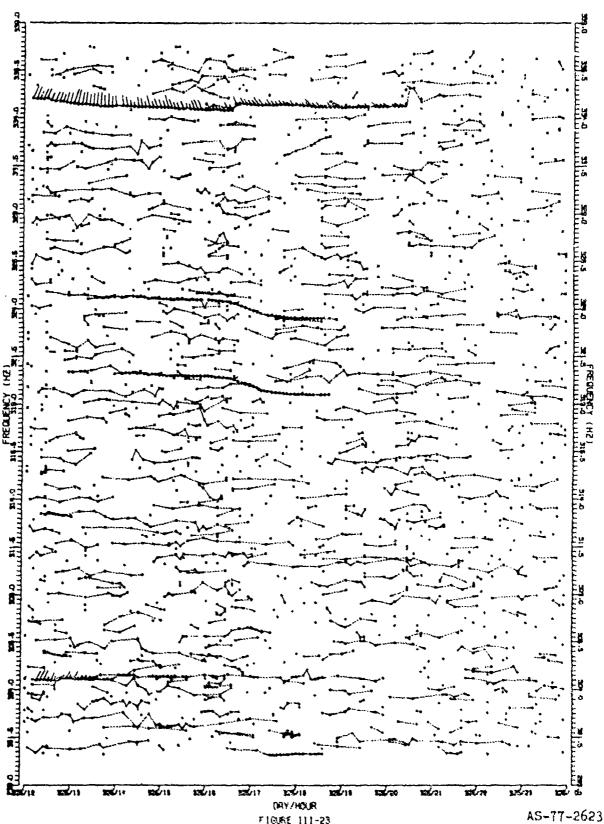


FIGURE 111-23
MSS-FVT HIGH-BAND DETECTION OVERVIEW DURING THE 21 MOV FIELD EVENT HT SITE AS OBTAINED VIA THE SINGLE CAROLOGICS FROM WITH WERNIER RESOLUTION (U)

(The reverse of this page is blank.)

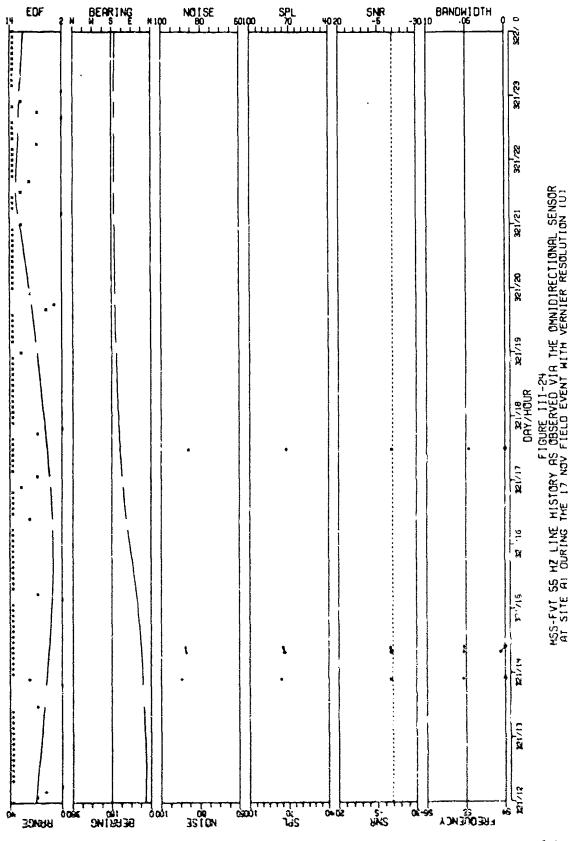
CONFIDENTIAL

UNCLASSIFIED

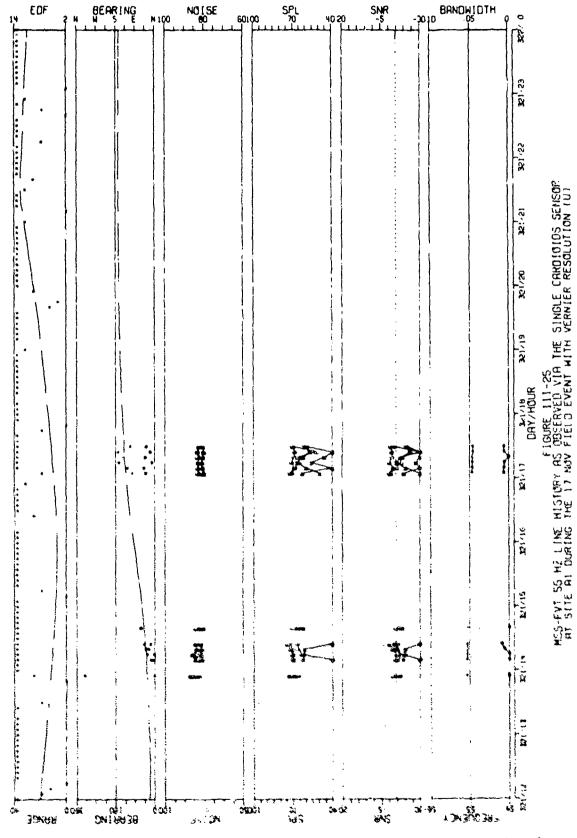
APPENDIX B

LINE HISTORY CURVES (U)

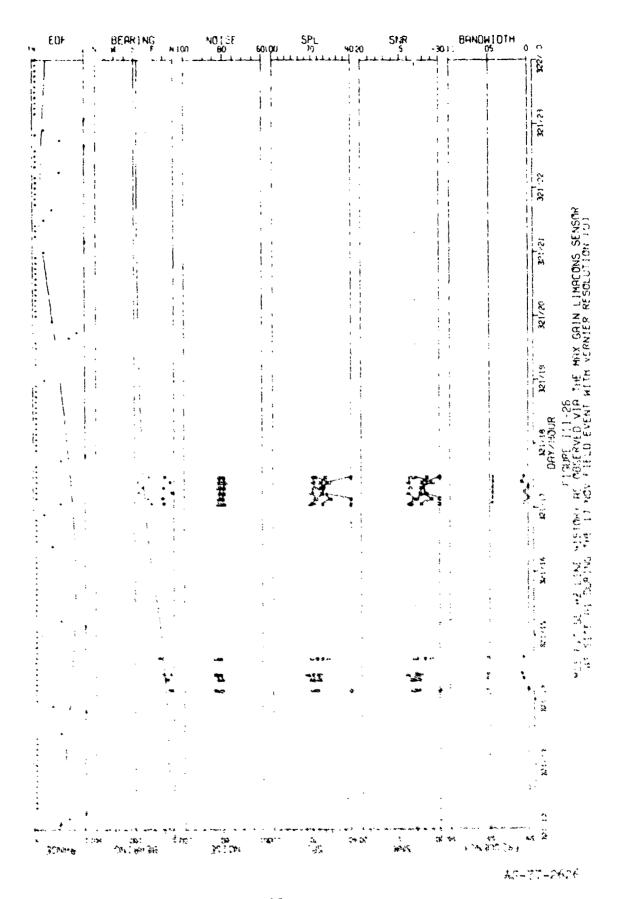
(FIGURES III-24 - III-163)

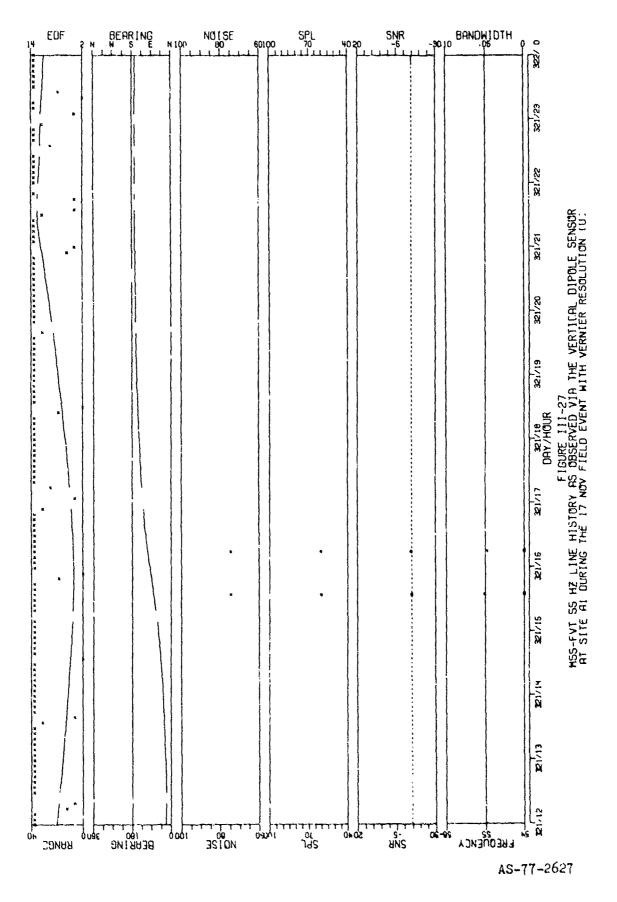


AS-77-2624

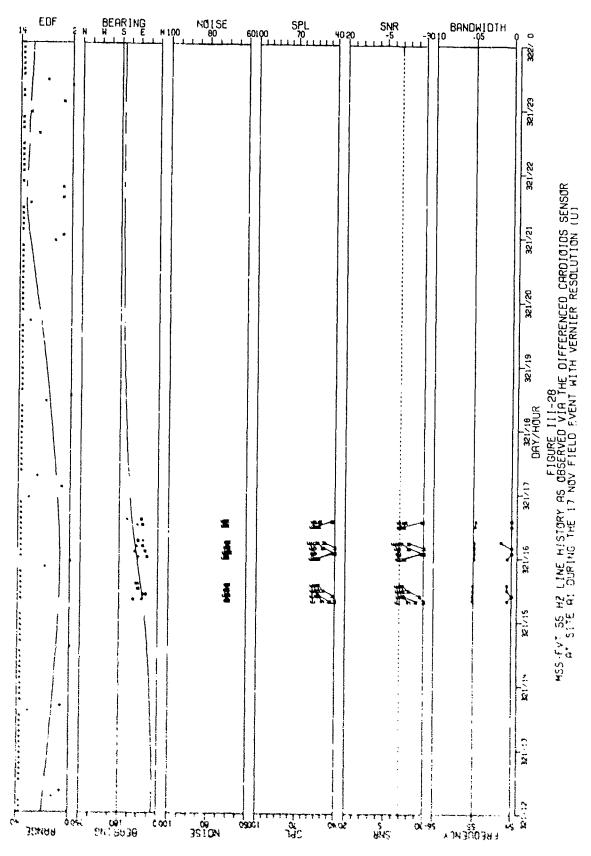


AS-77-2625

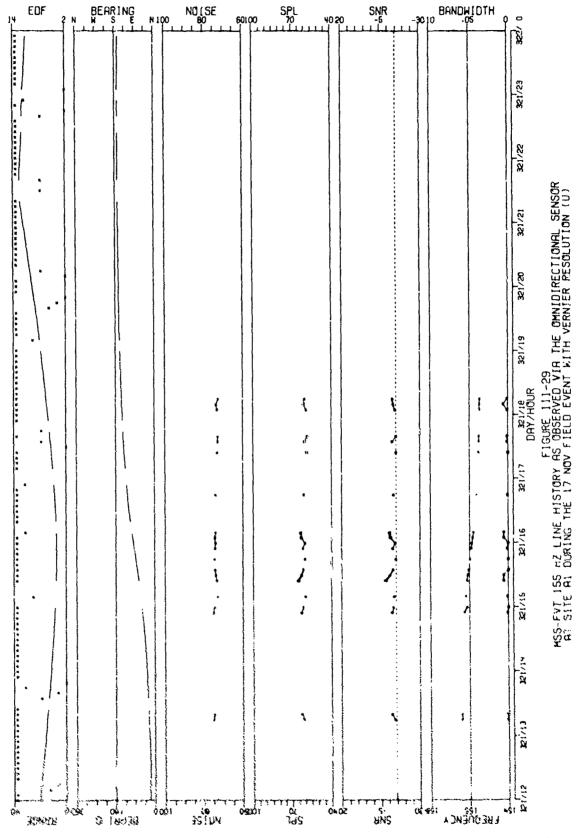




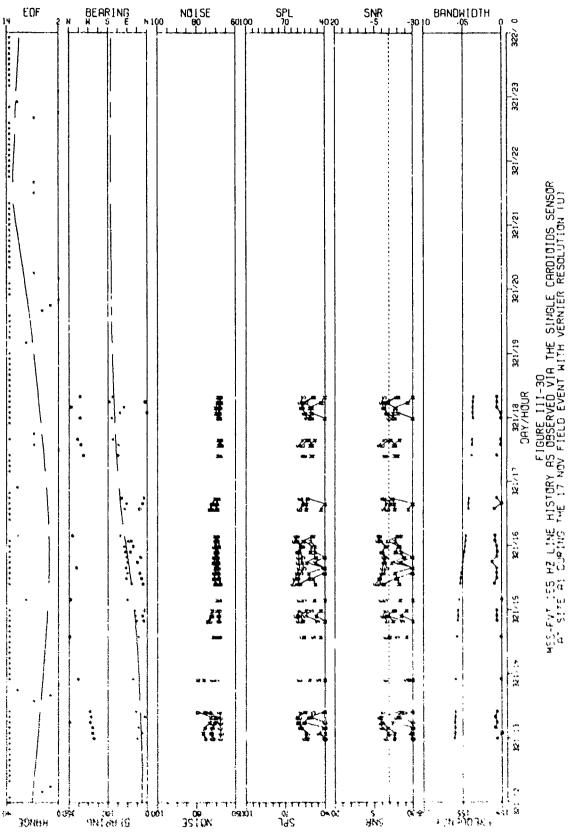
CONFIDENTIAL



AS-77-2628

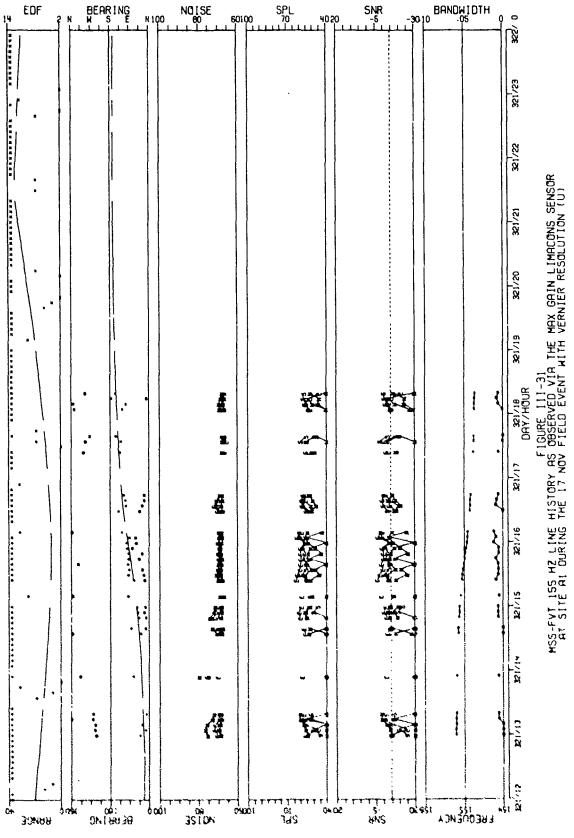


AS-77-2629

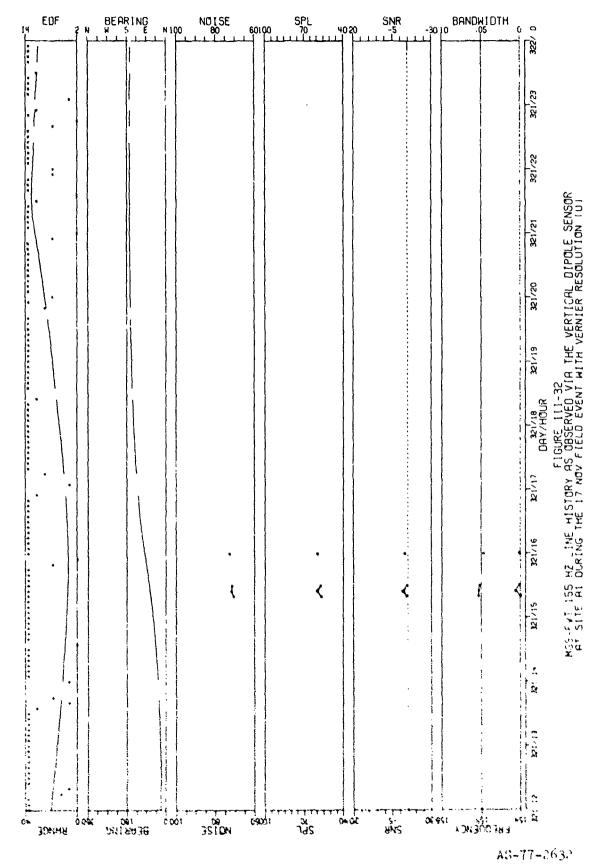


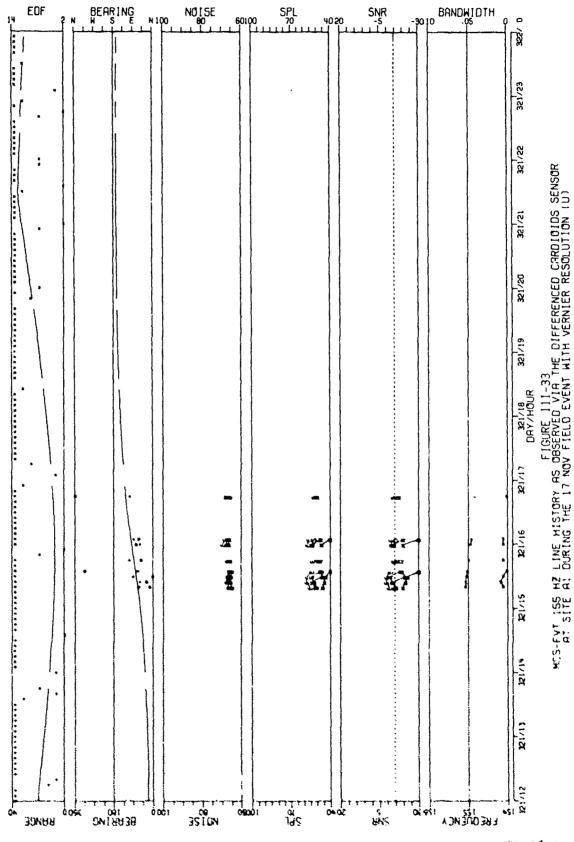
AS-77-2630

CONFIDENTIAL

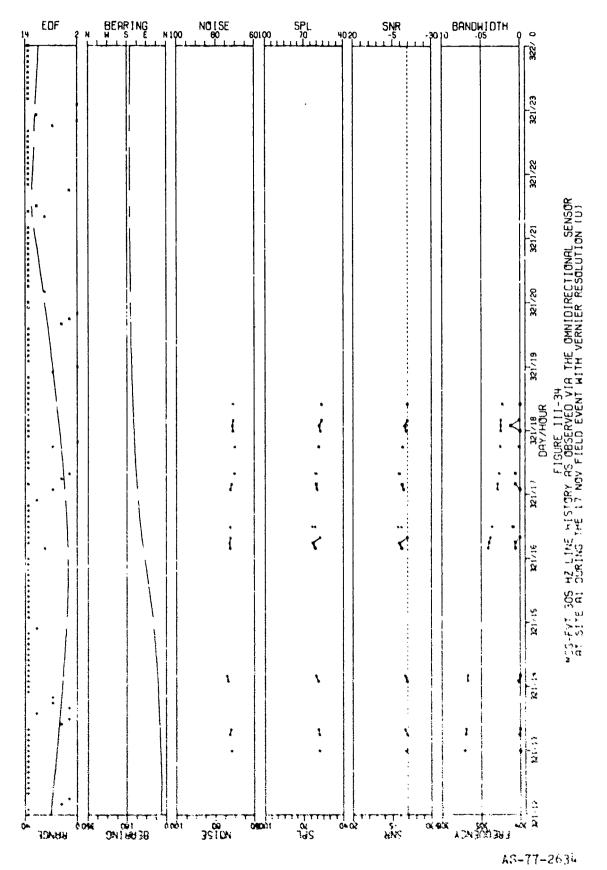


AS-77-2631

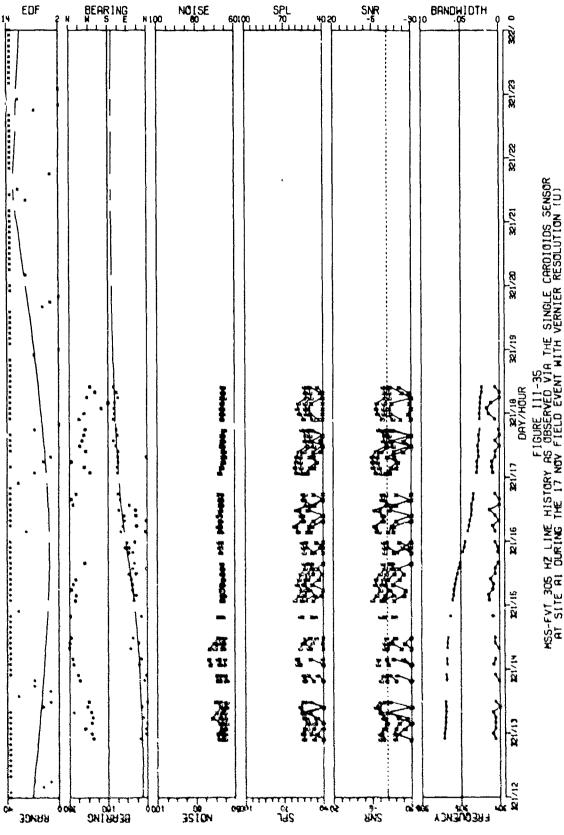




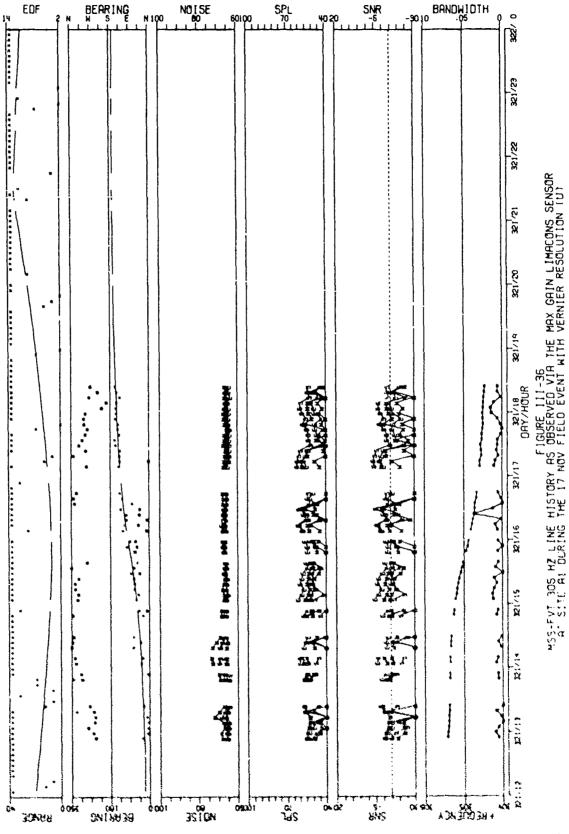
AS-77-2633



CONFIDENTIAL



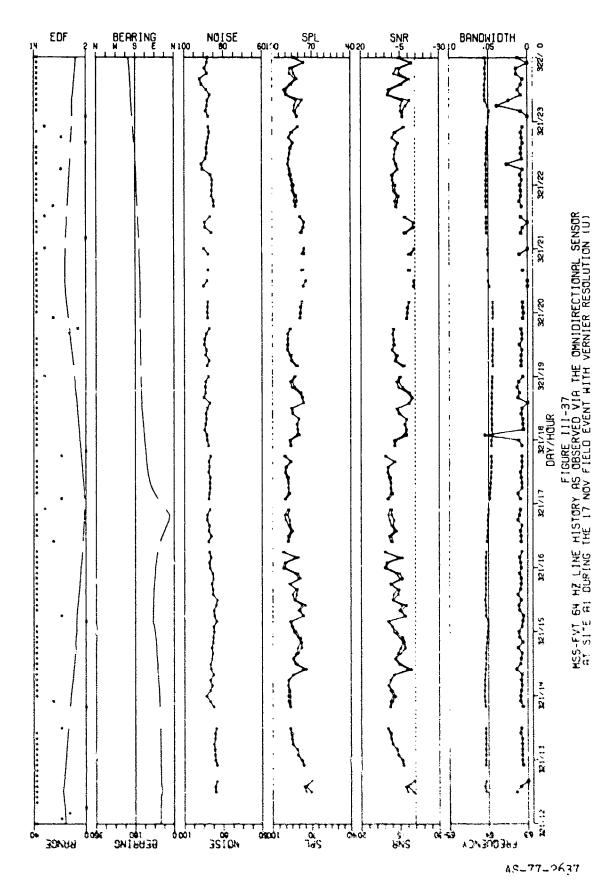
AS-77-2635

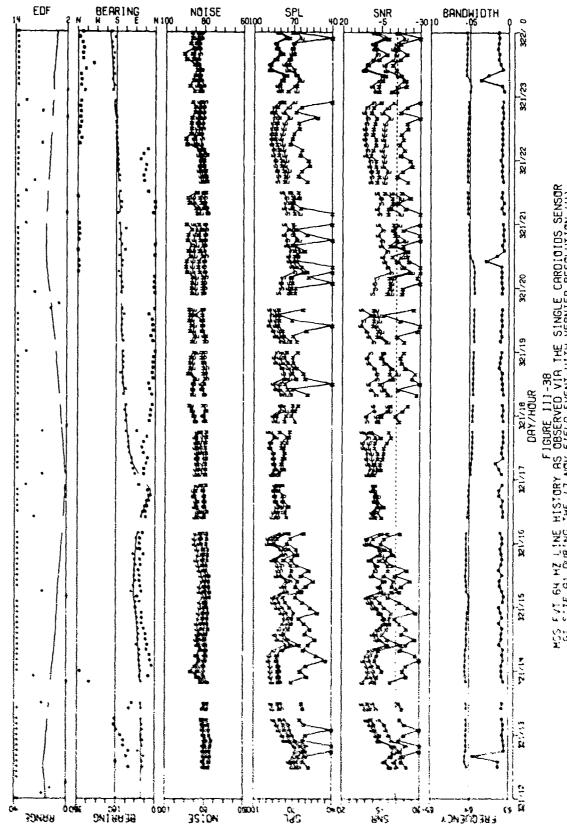


AS-77-2636

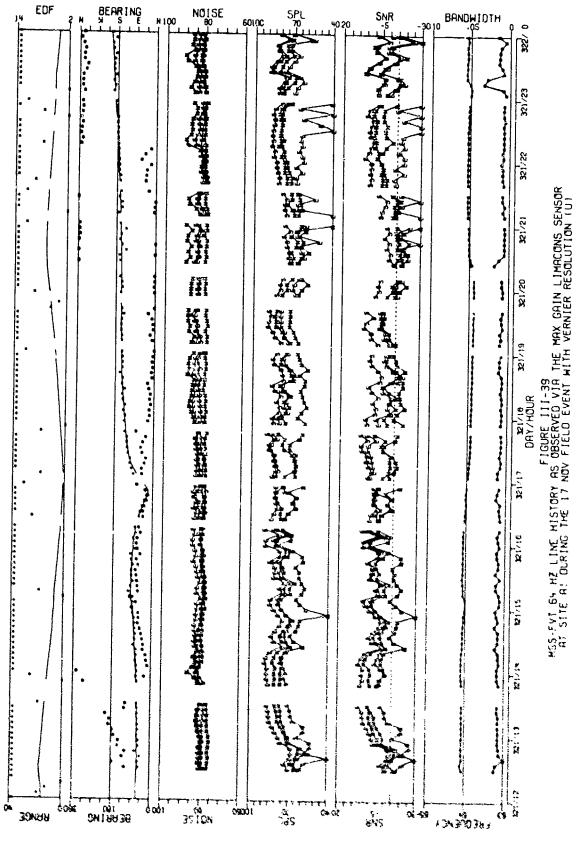
CONFIDENTIAL

the second second second second second second second second second second second second second second second se

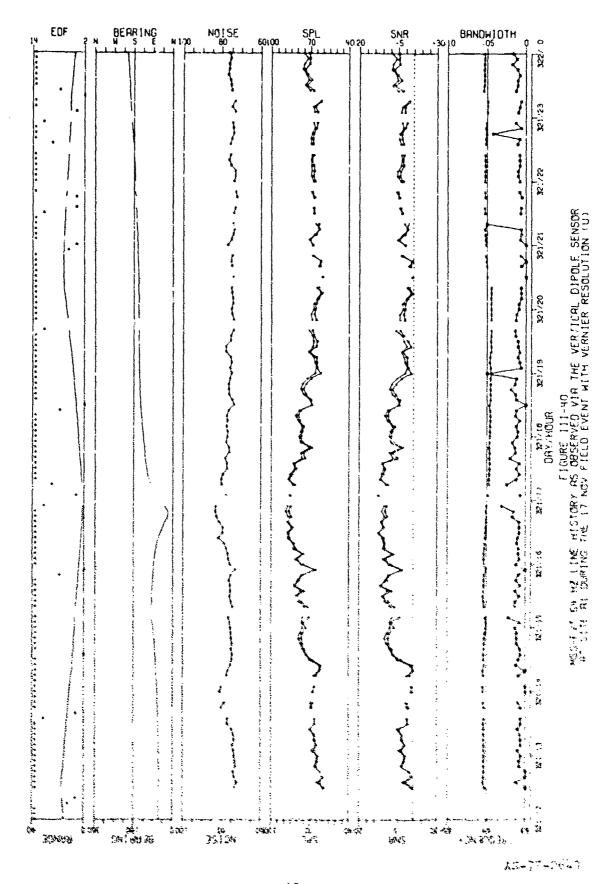


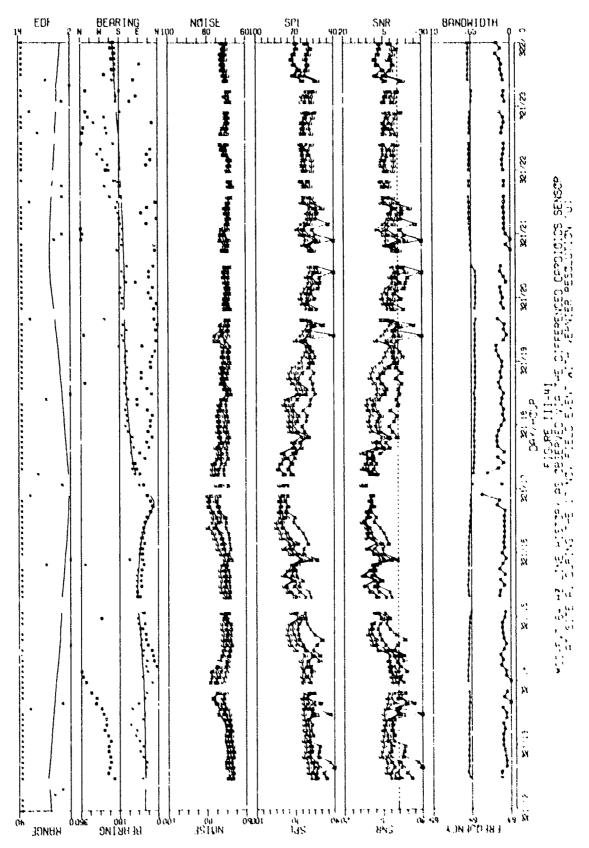


88-35-77-2A

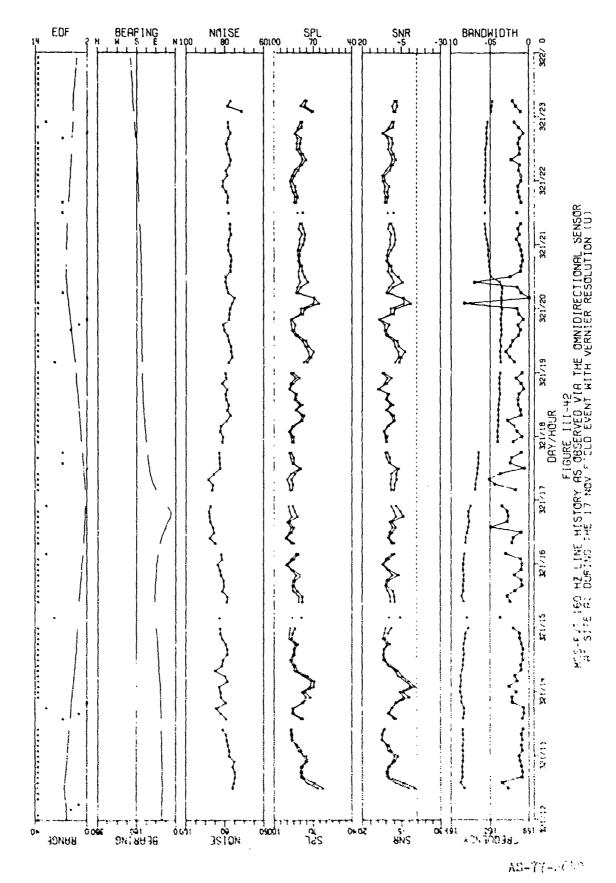


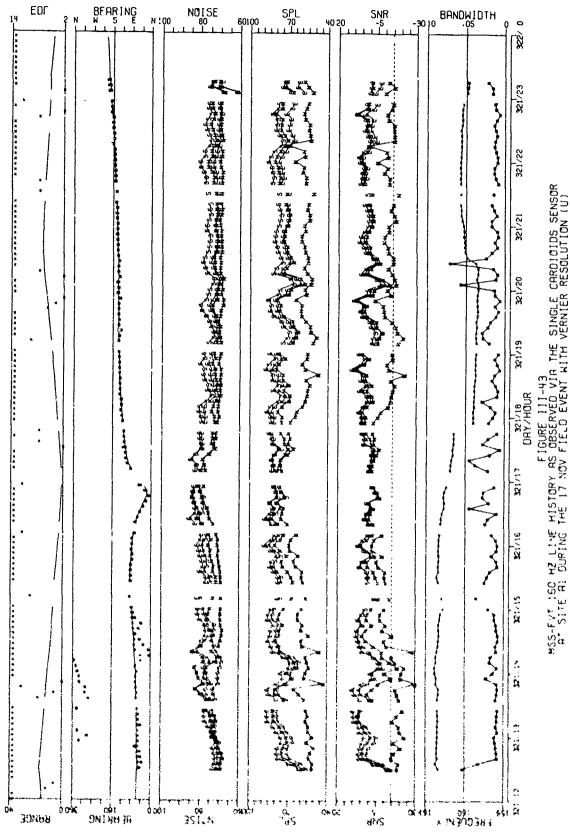
AS-77-2639



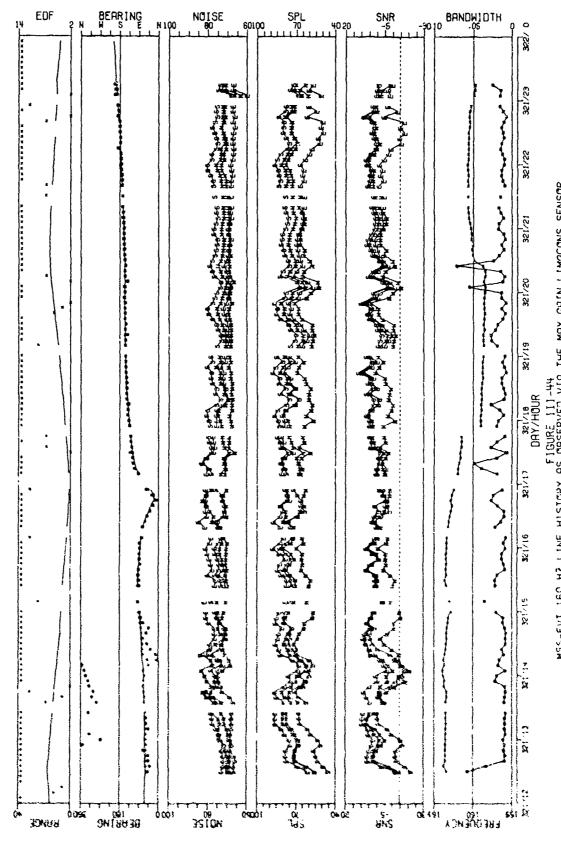


A3-77-2641

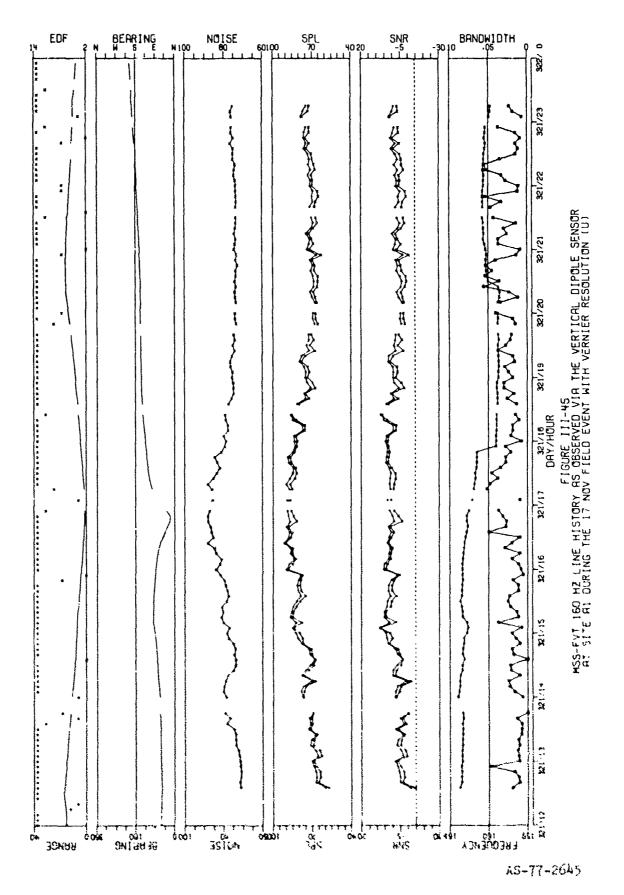




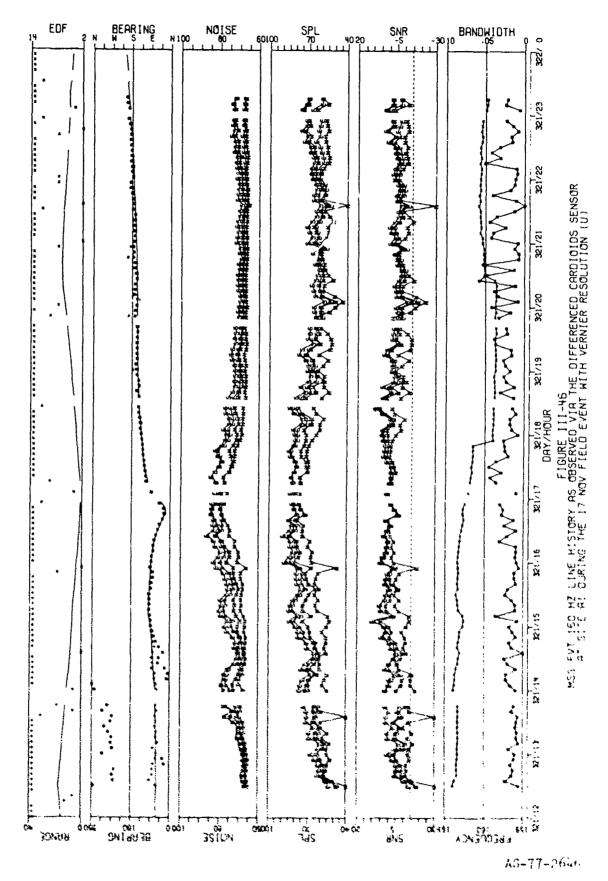
AS-77-2643

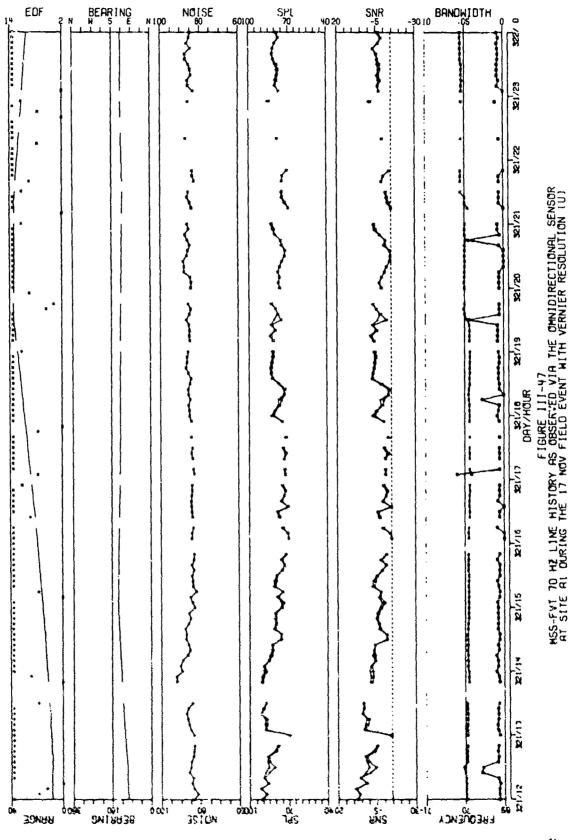


AS-77-2644

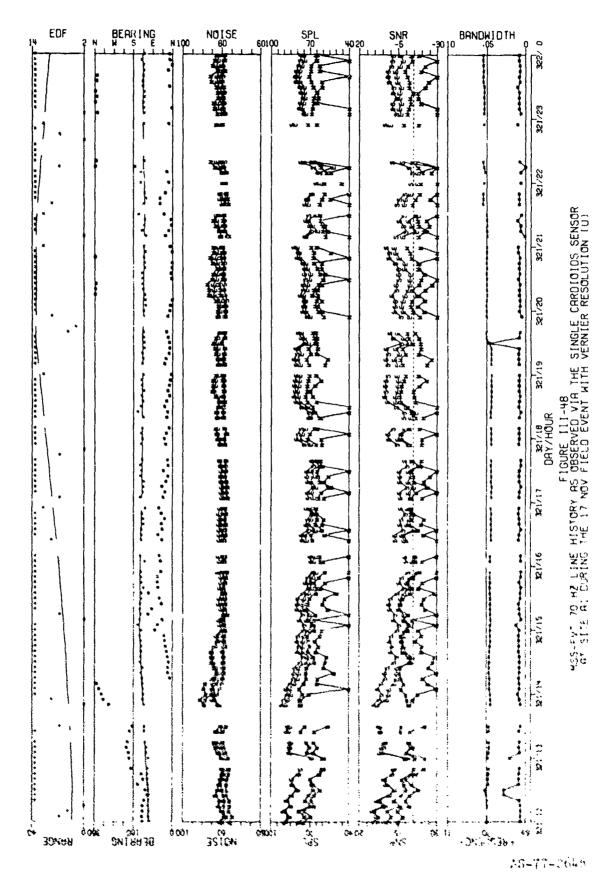


CONFIDENTIAL

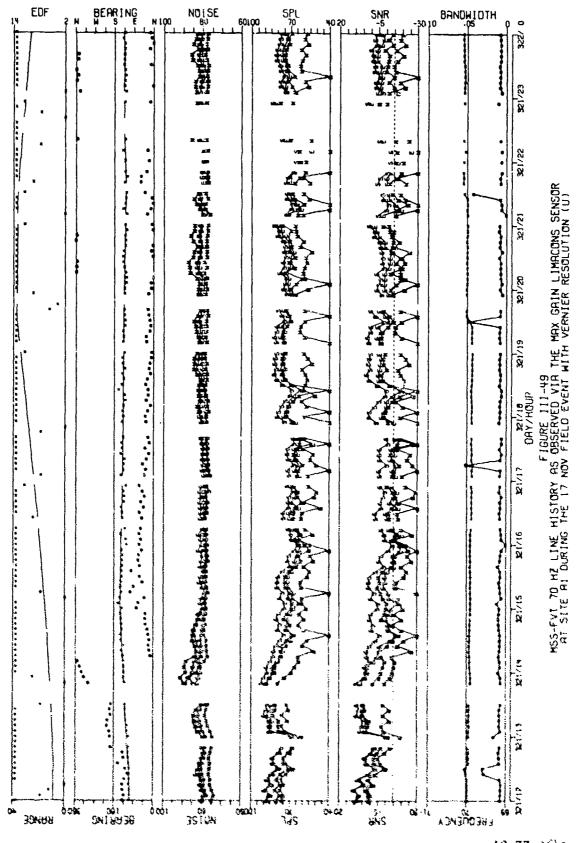




AS-77-2647



CONFIDENTIAL



CONFIDENTIAL

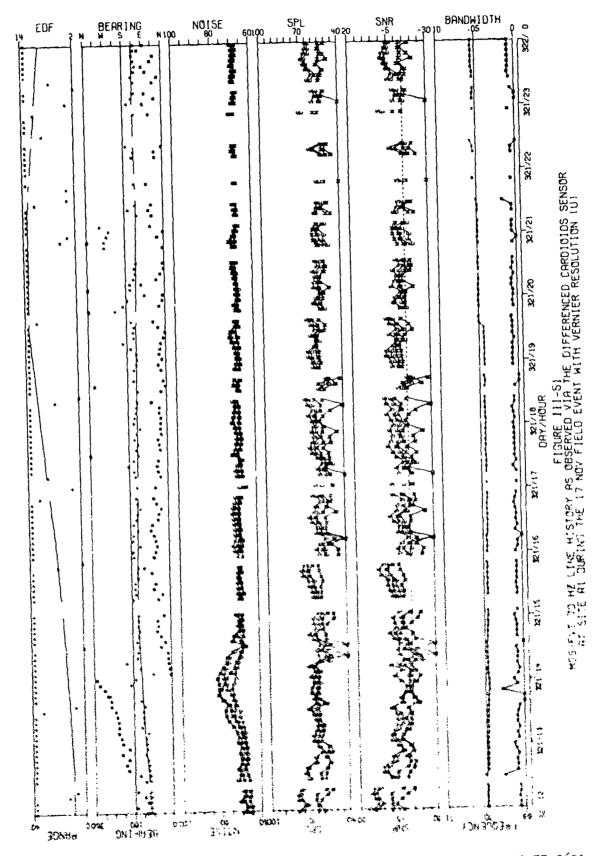
AS-77-2649

-

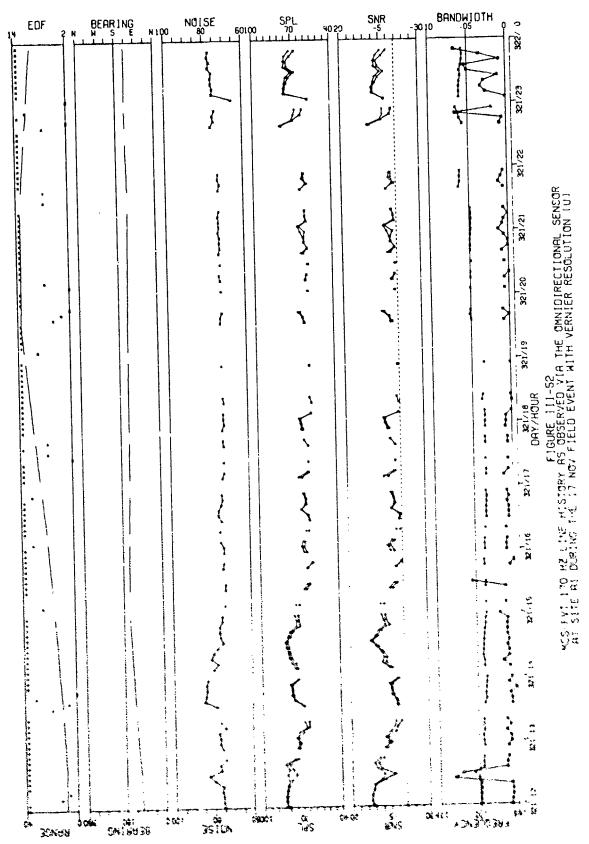
فقم

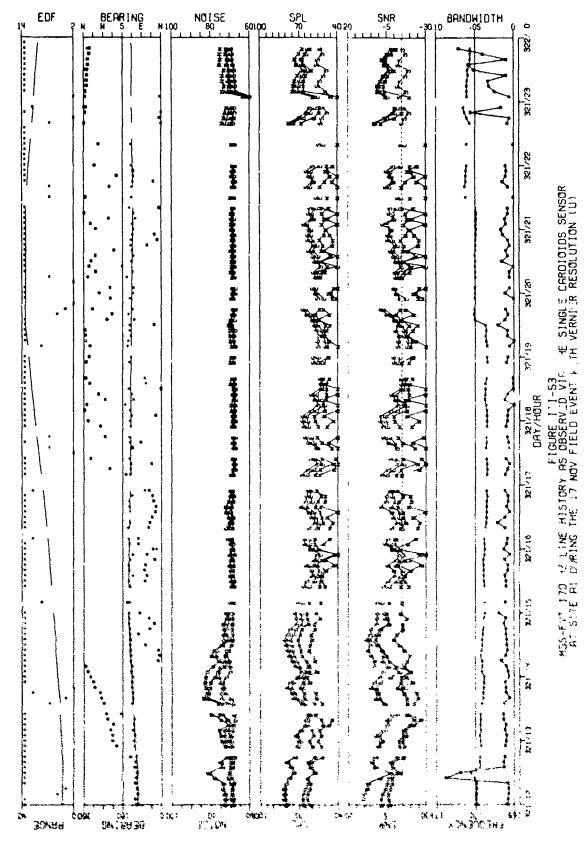


AU-77-2650

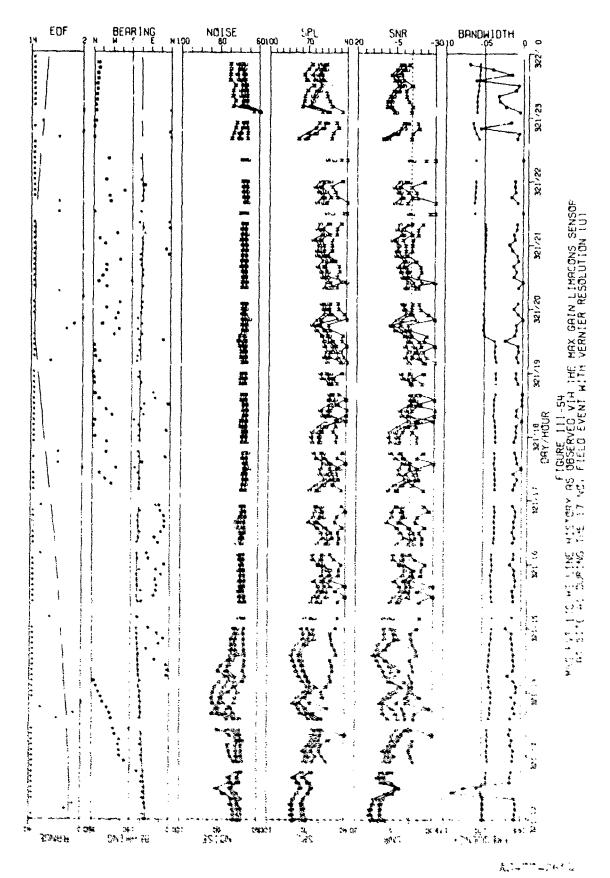


and the second second of the second second and the second second second second second second second second second

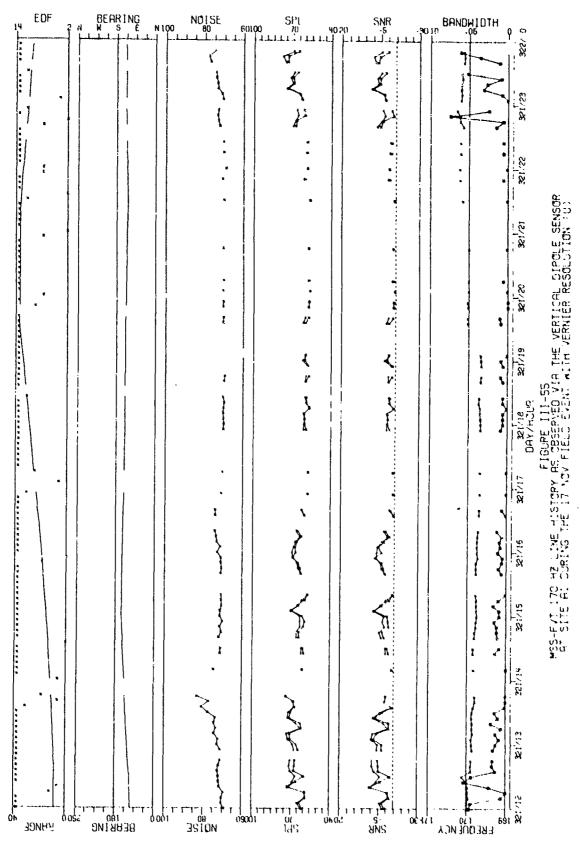


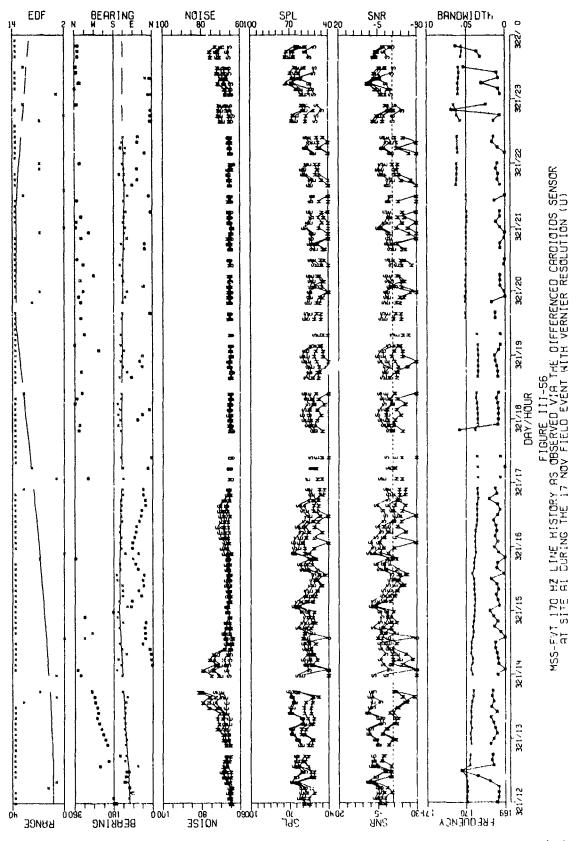


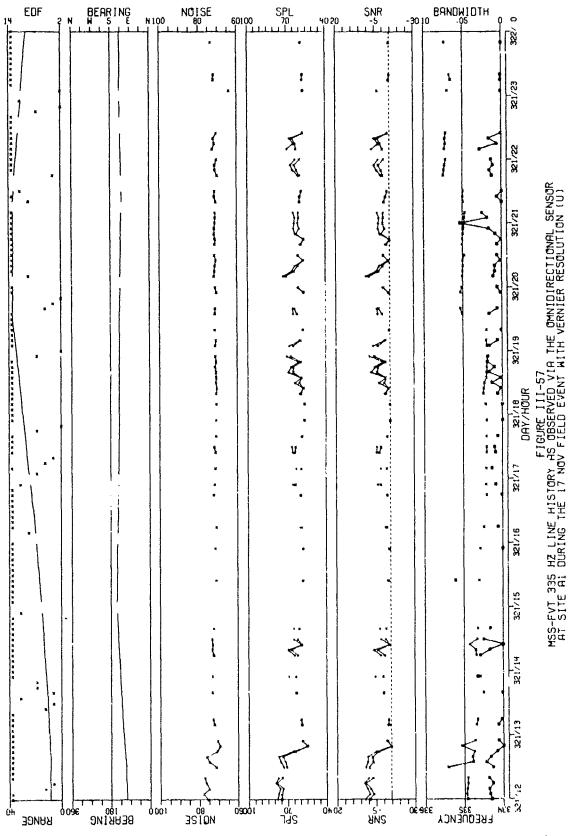
AS-77-2653

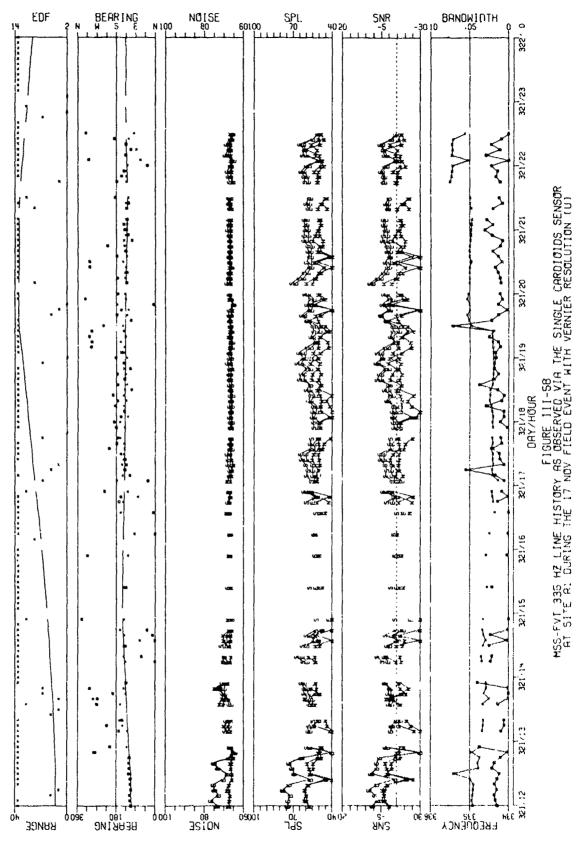


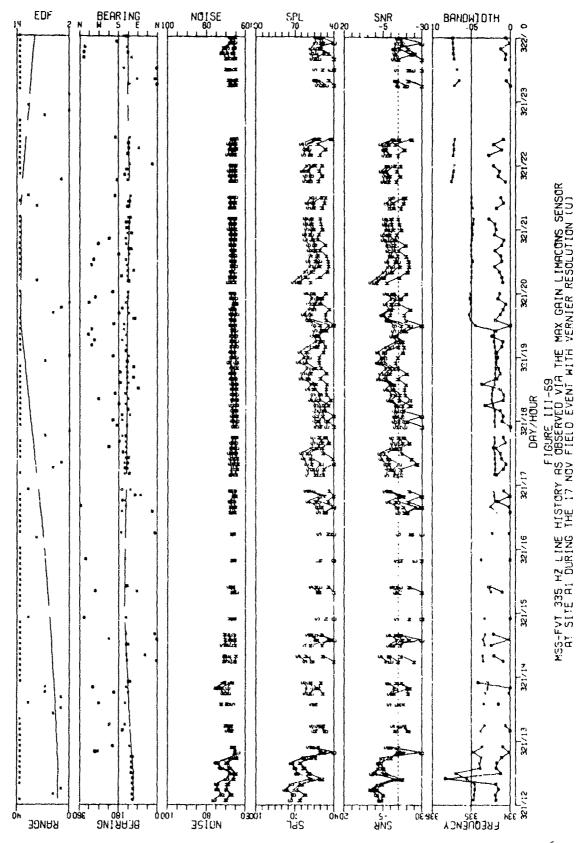
CONFIDENTIAL



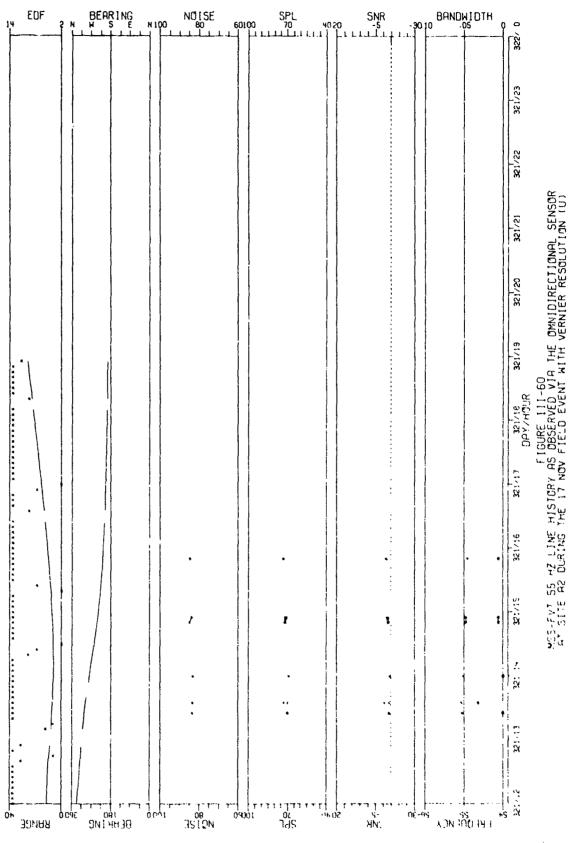




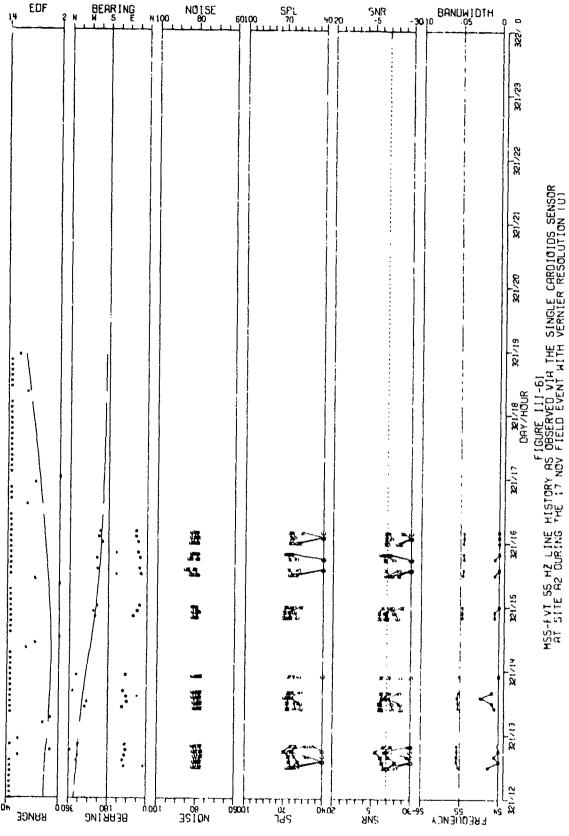


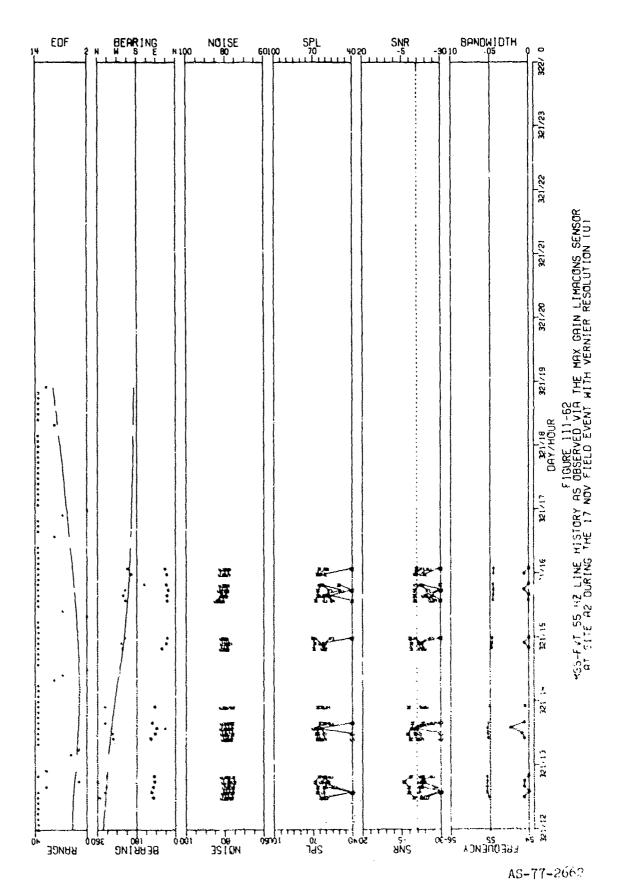


AS-77-2659



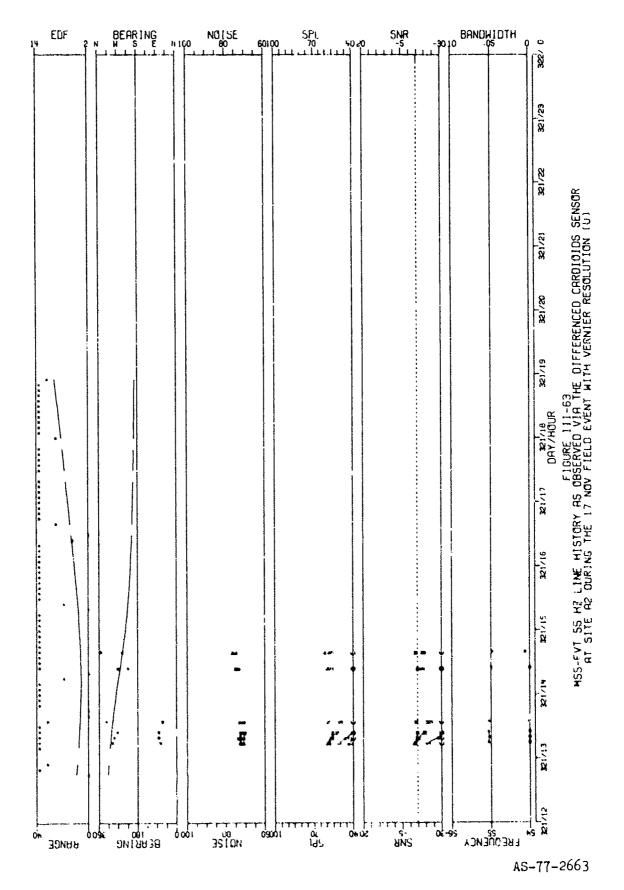
A8-77-2660

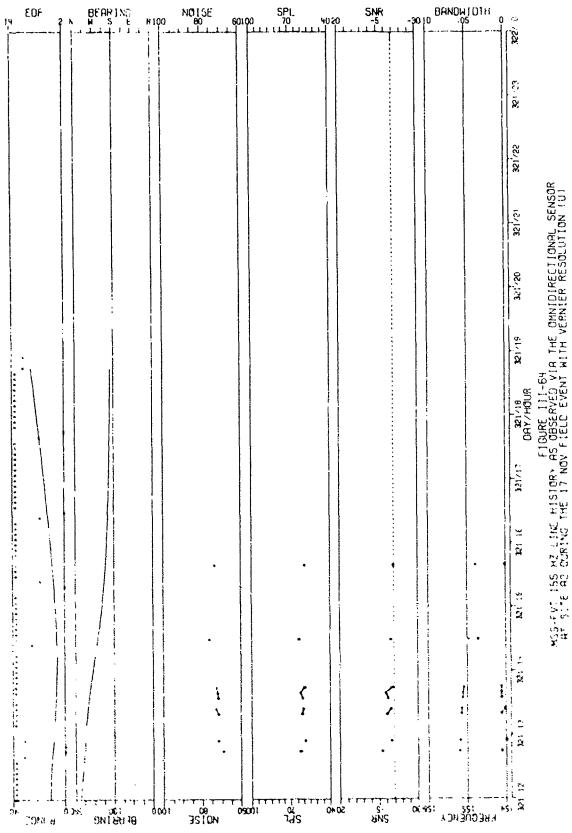


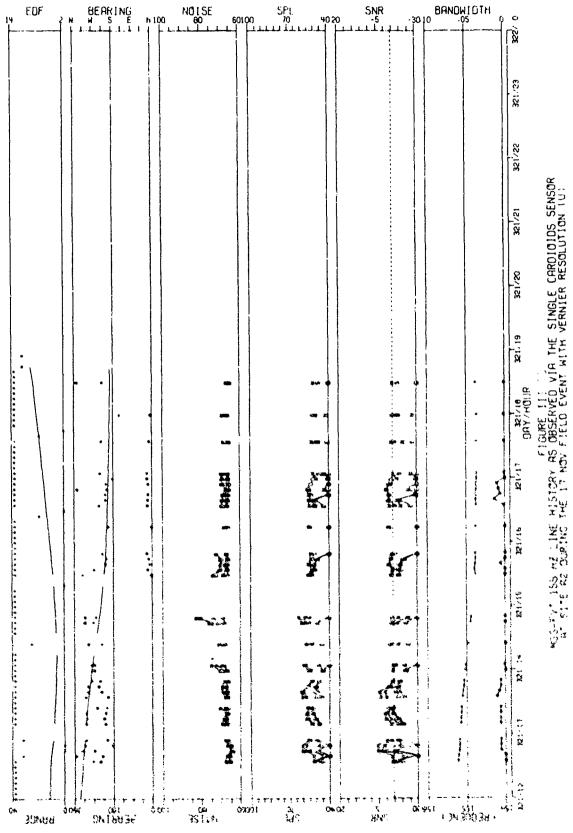


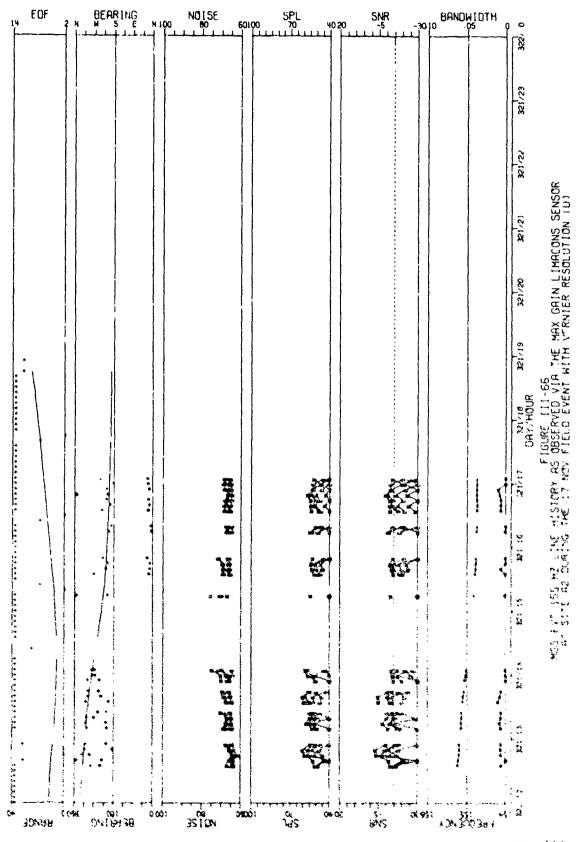
CONFIDENTIAL

91





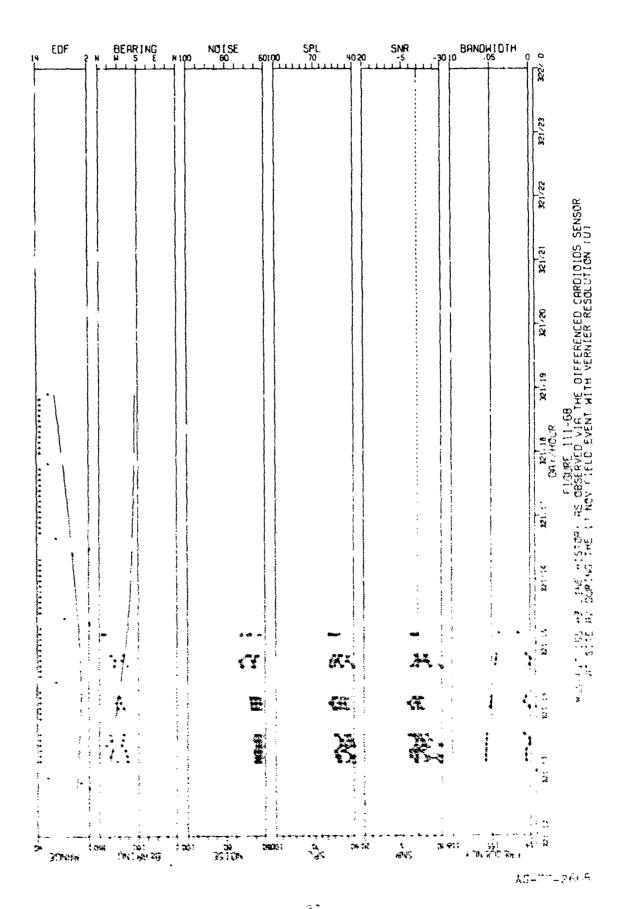


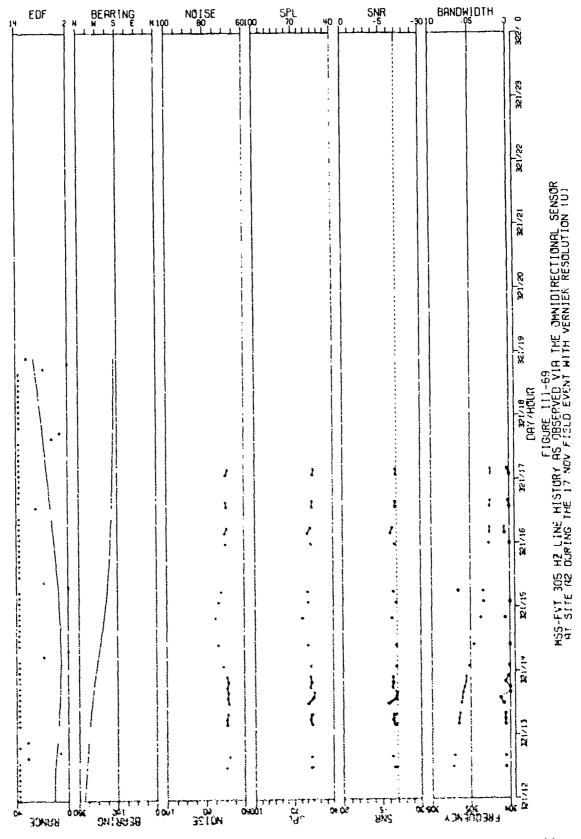


AG-77-2666

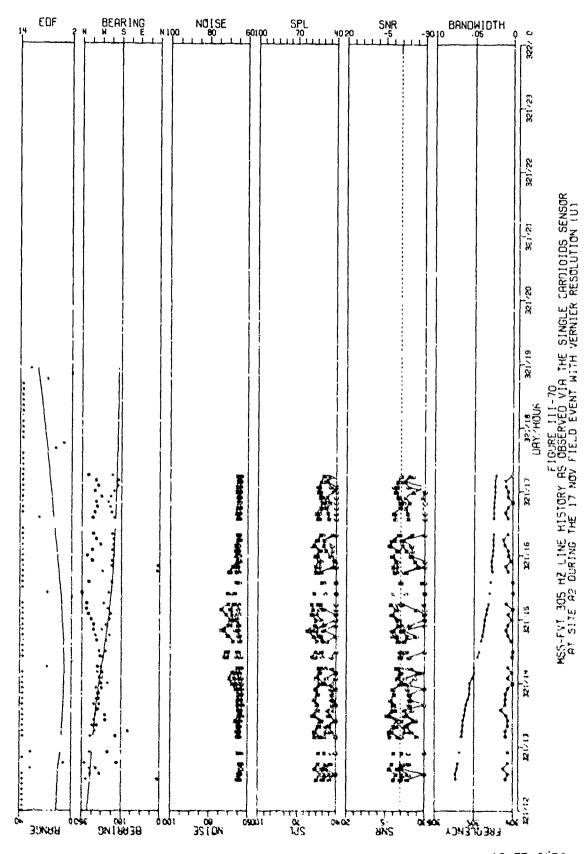
CONTRACTOR OF THE PROPERTY OF

EDF	BEARING N N S E N	NO 80 50	SPL :	5NR 1020 -5	BANDWIDTH US	35.5
						321/23
						281/28
						321/21
			\$1			321, 20
						321/19
						57.154 D34 Y60UR
						21:13
	manufacture of the state of the		} : : : :	. !		77. 778
Andrew Comments				! ! 		***
			•	· .	;	:
; ;		, , , , , , , , , , , , , , , , , , ,	·	₹		
· · ·		• !	•	•	•	· ;
		1		:		:
CMINER	de de la companya de la companya de la companya de la companya de la companya de la companya de la companya de La companya de la companya de	Selfu Selfu	TÉ LA LA LA LA LA LA LA LA LA LA LA LA LA	й кан тан жа Сжей (1914)	24 AC (144 AC) 24 AC (144 AC	<u>i</u>

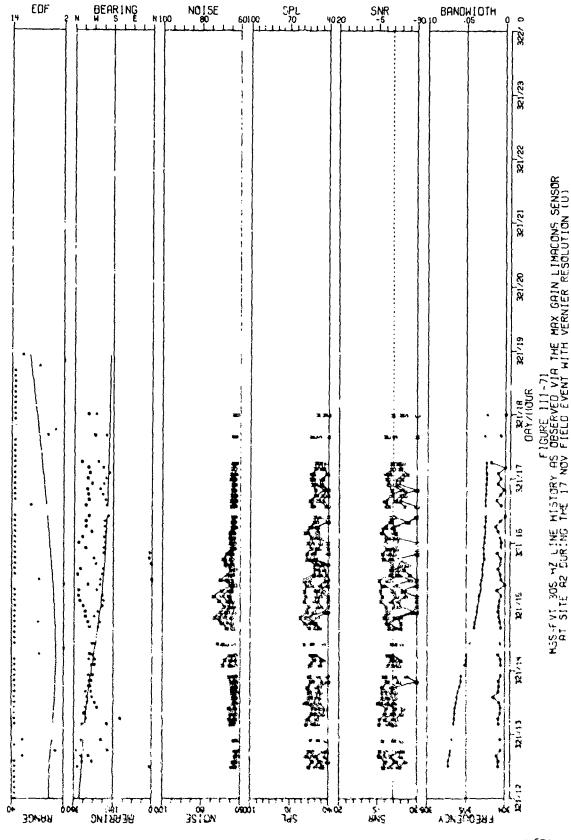




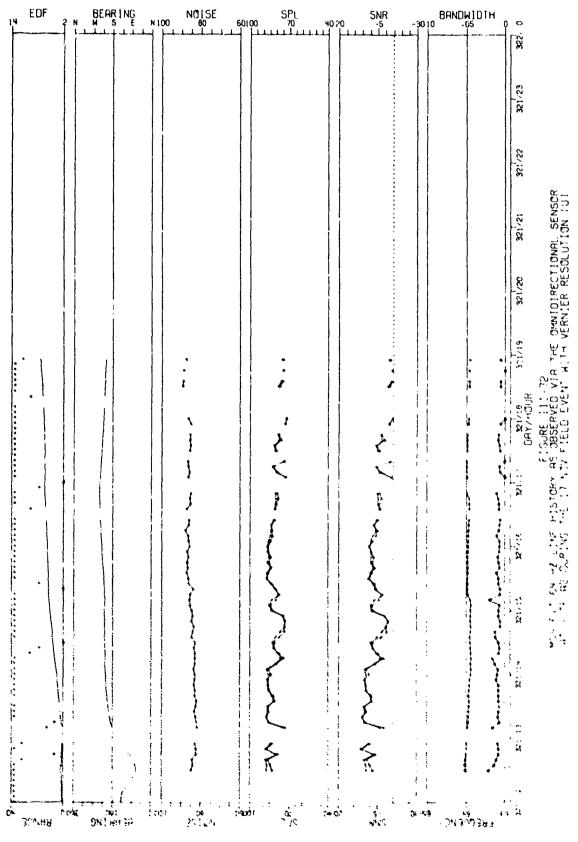
AS-77-2669



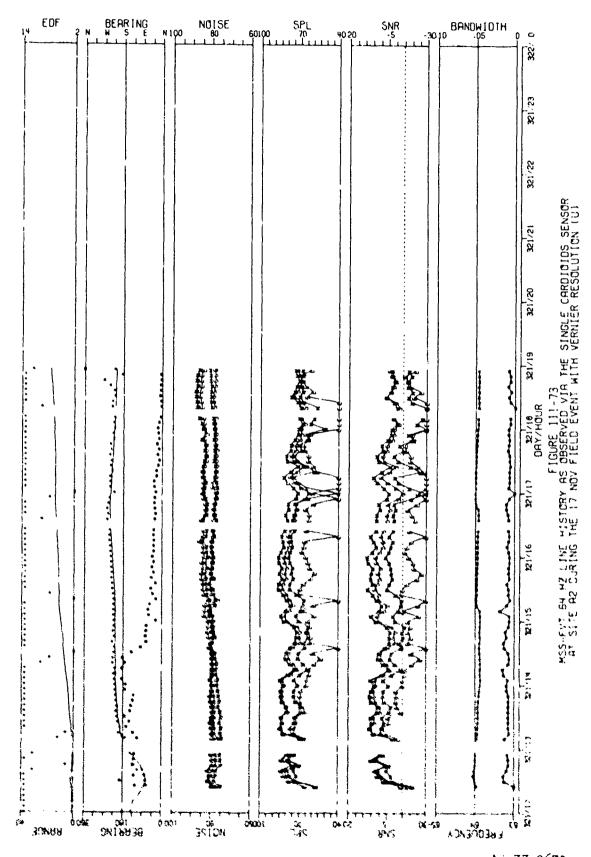
AS-77-2670



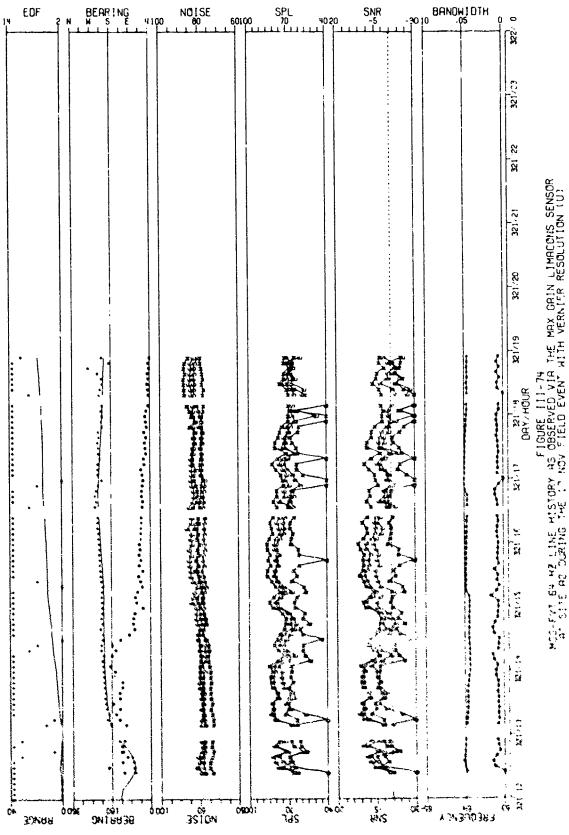
AS-77-2671

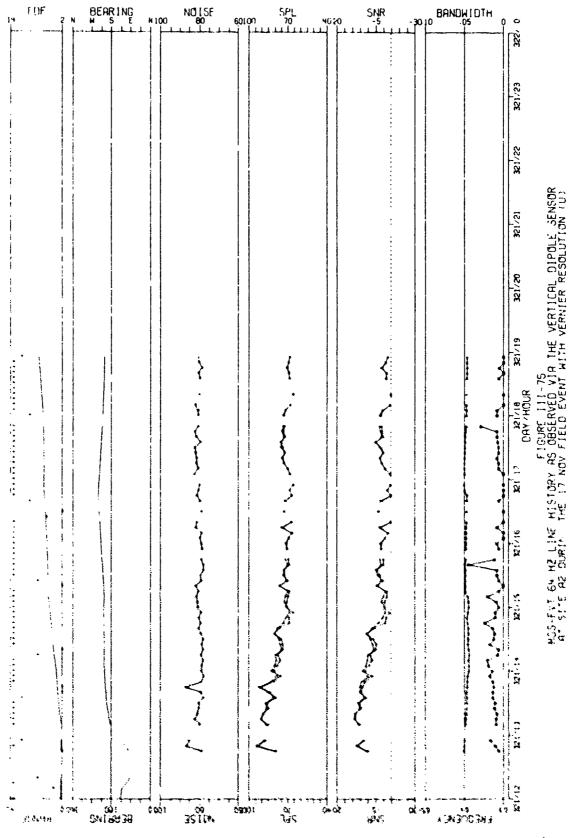


and the second second second second second

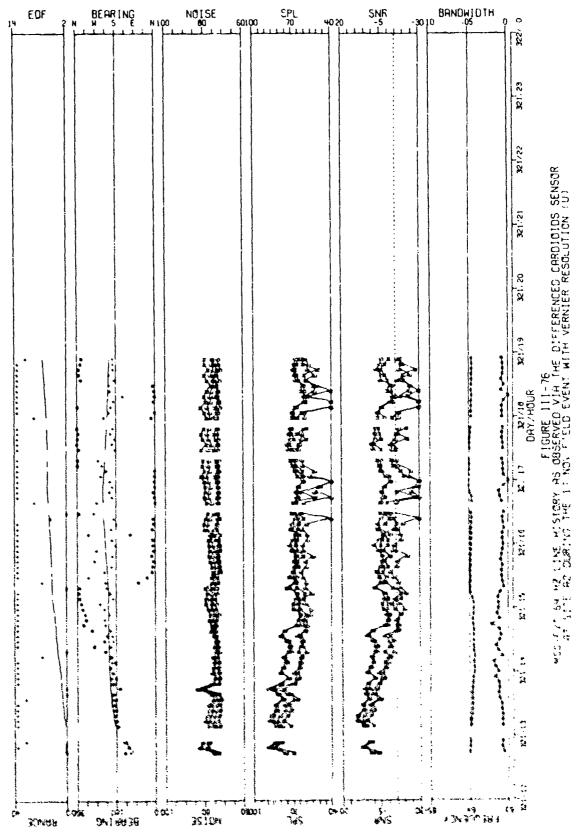


AS-77-2673





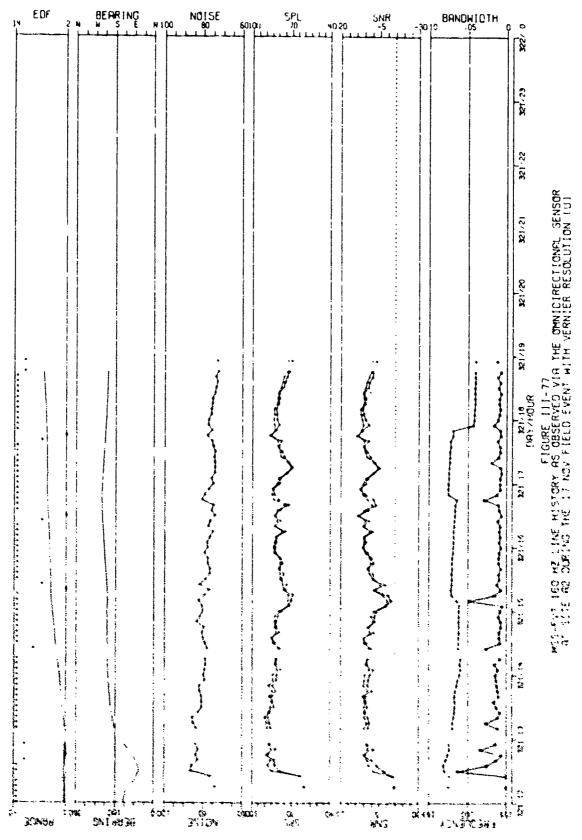
AS-77-2675



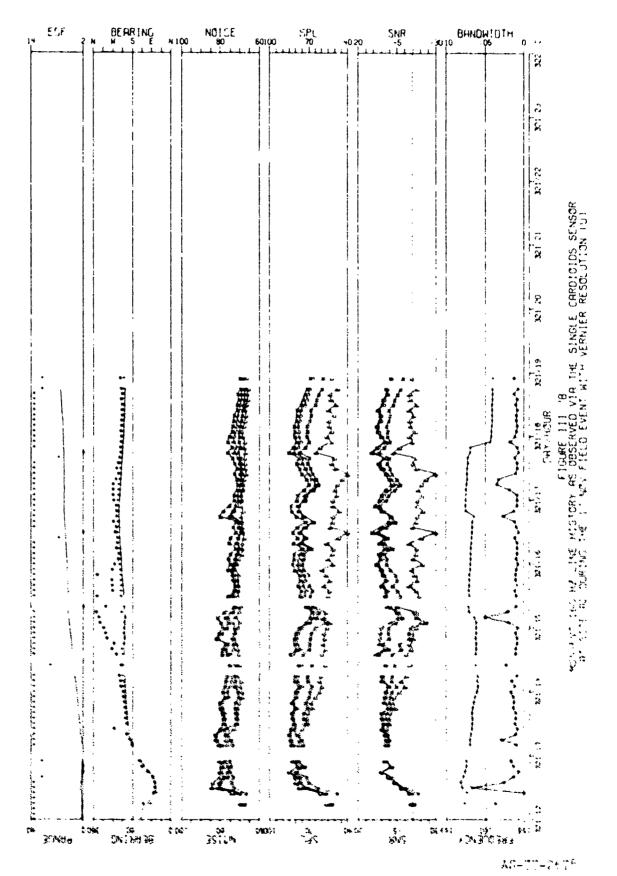
AS-77-2676

CONFIDENTIAL

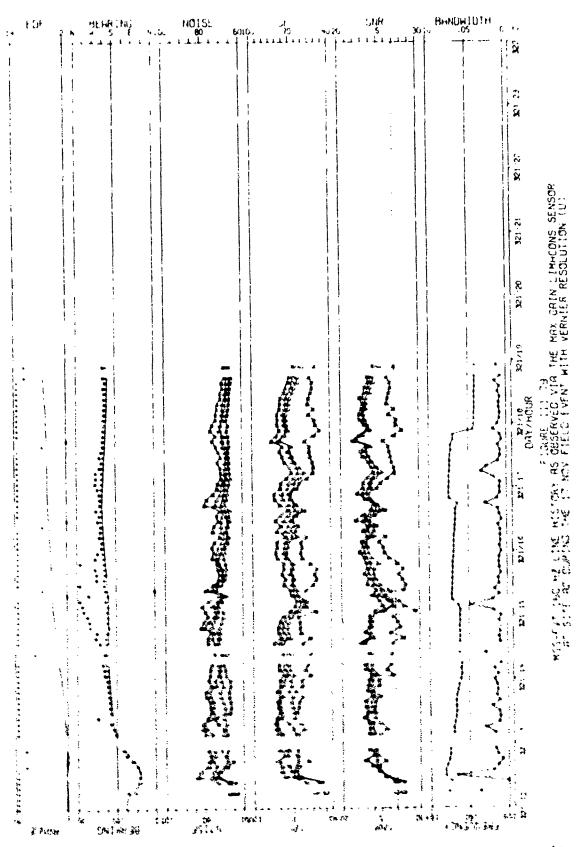
and the second of the second o



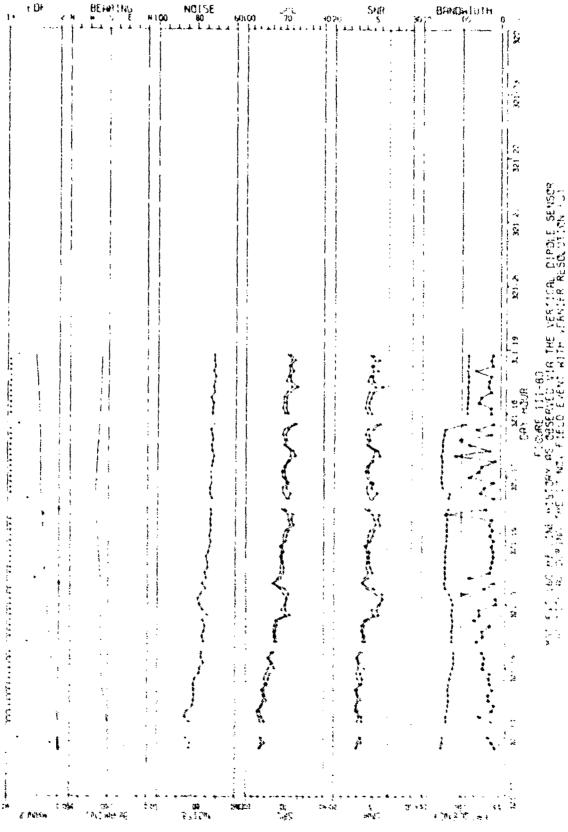
AS-77-2677



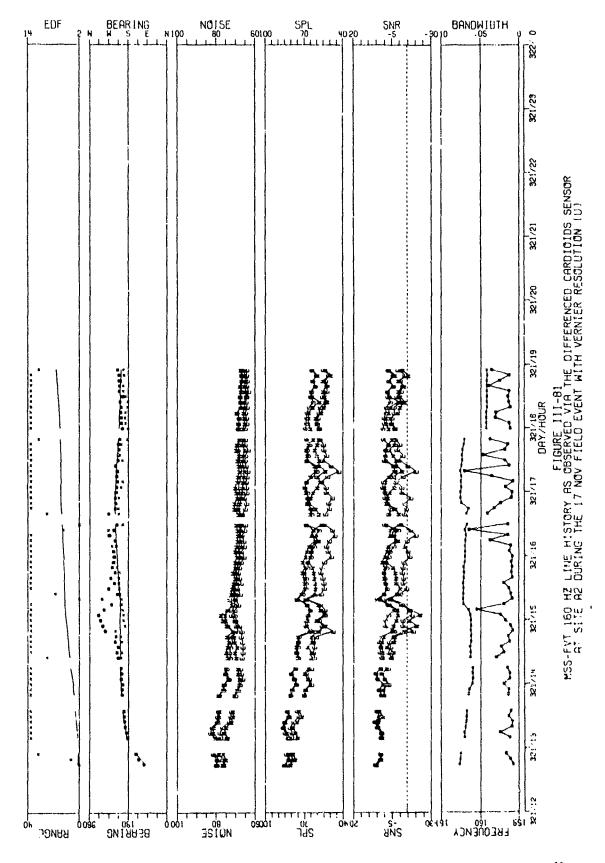
107



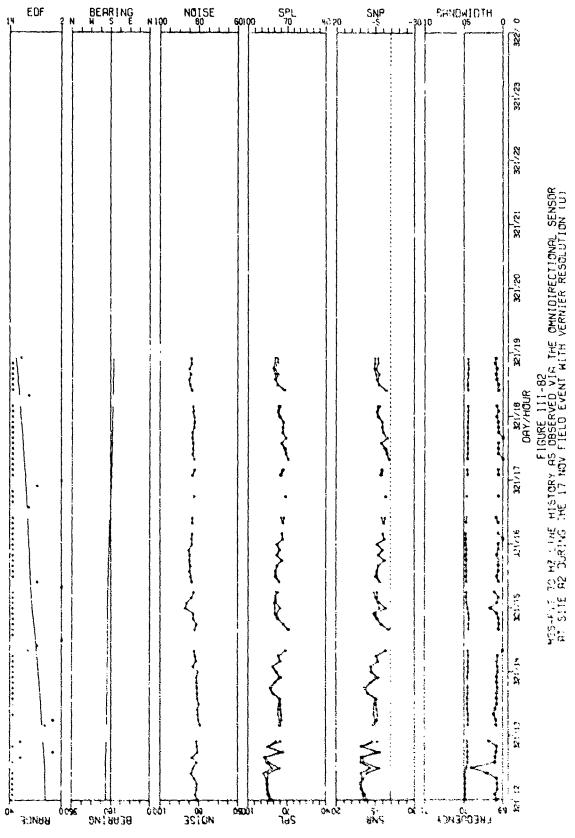
AS-77-2679



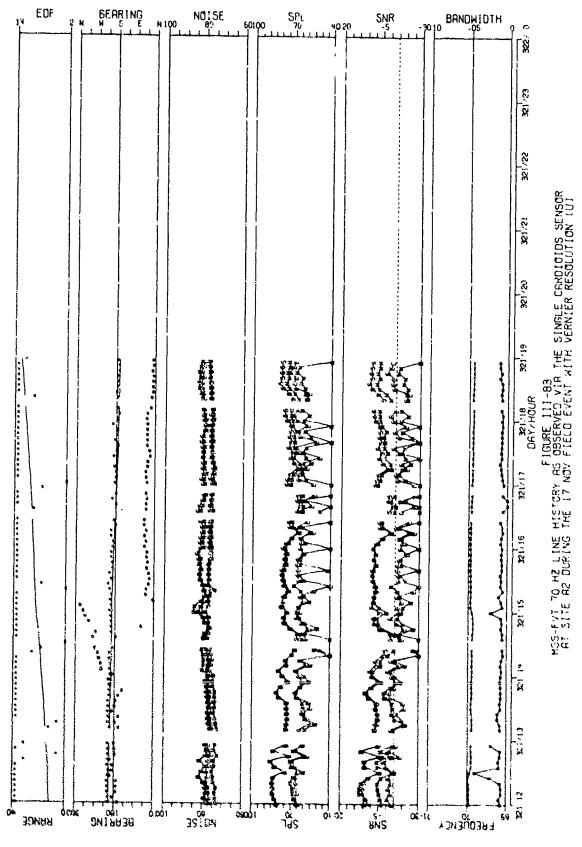
AS-77-2680



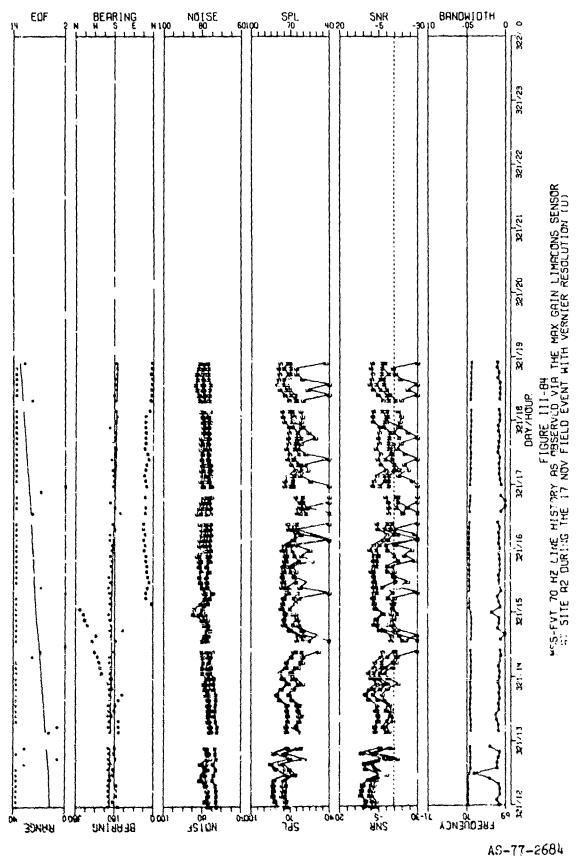
AS-77-2681



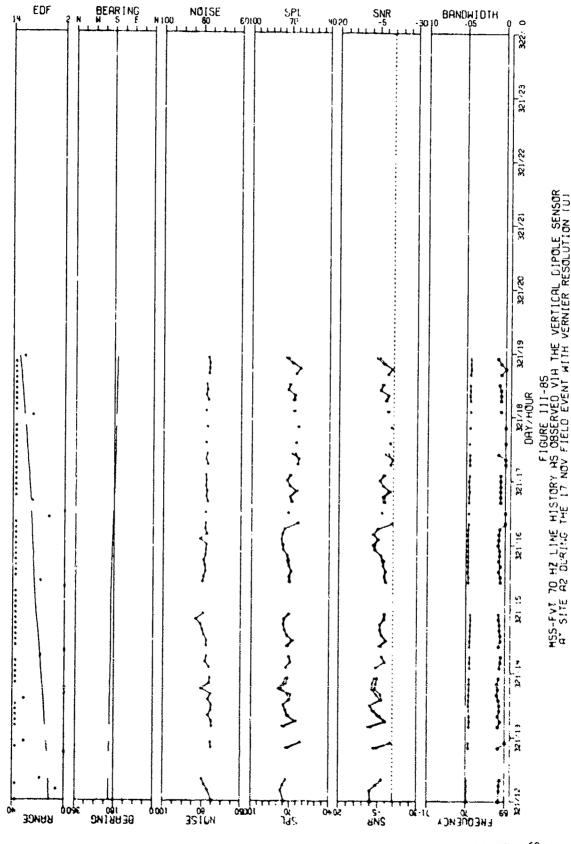
AS-77-2682



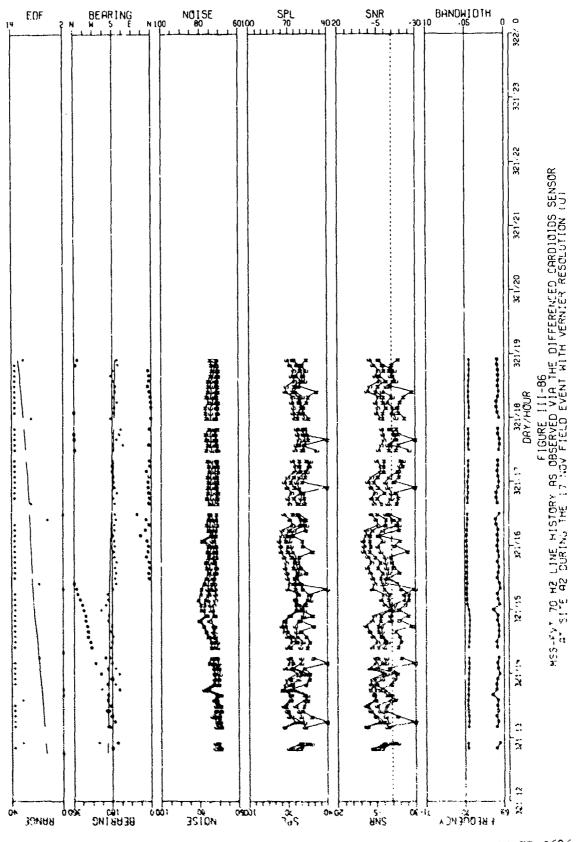
AS-77-2683



7407 [;

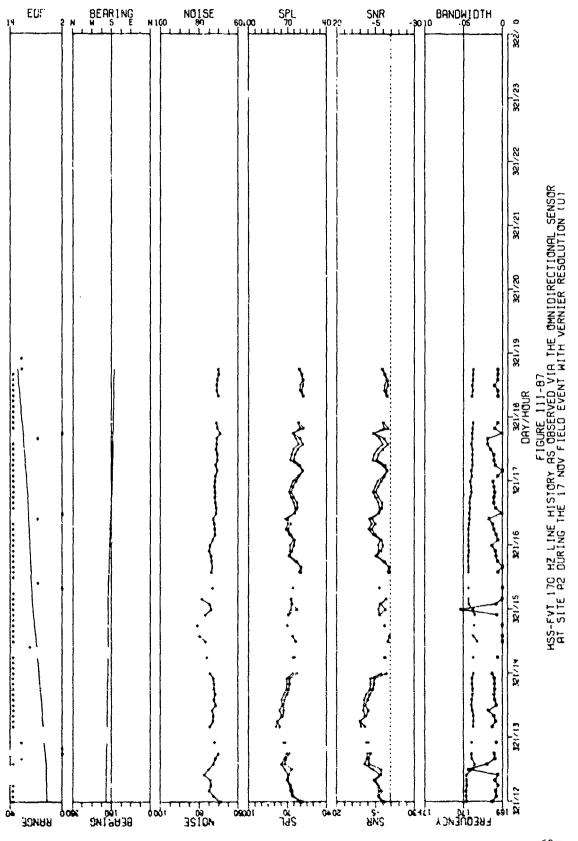


AS-77-2685

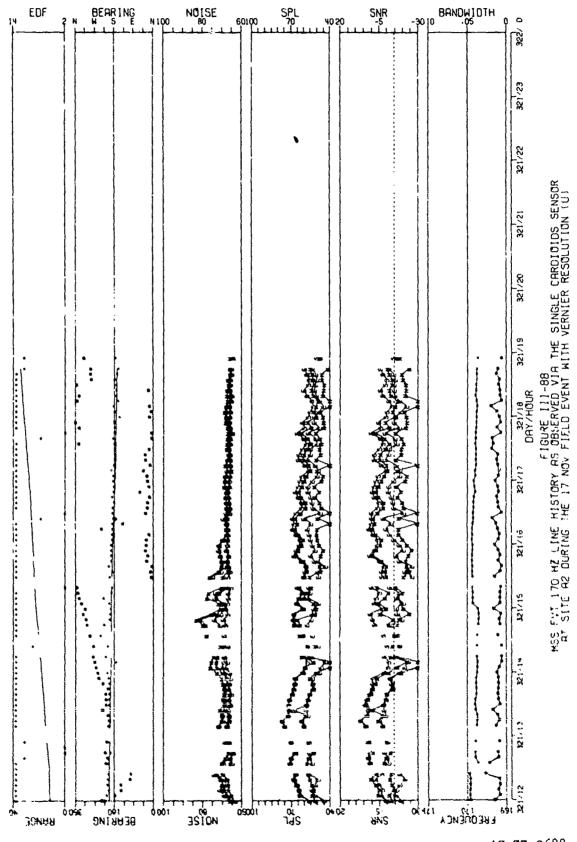


and the state of the state of the state of the state of the state of the state of the state of the state of the

AS-77-2686

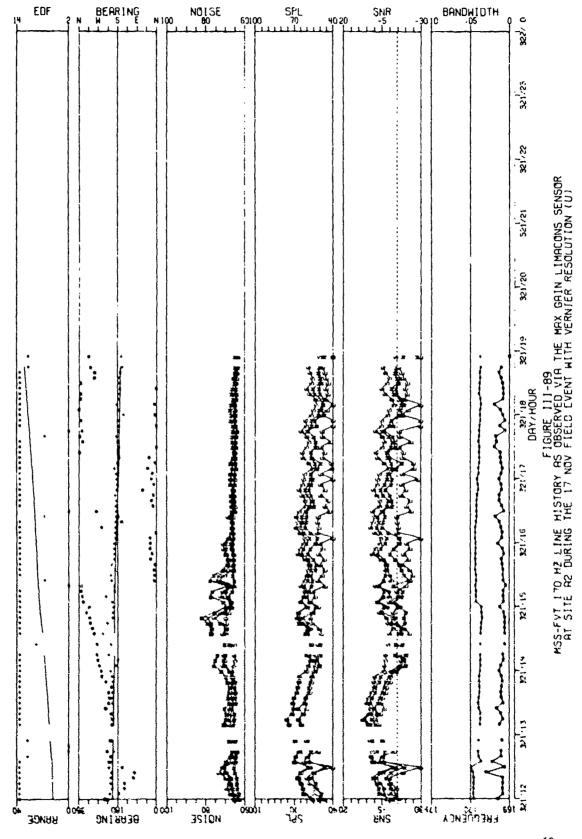


AS-77-2687



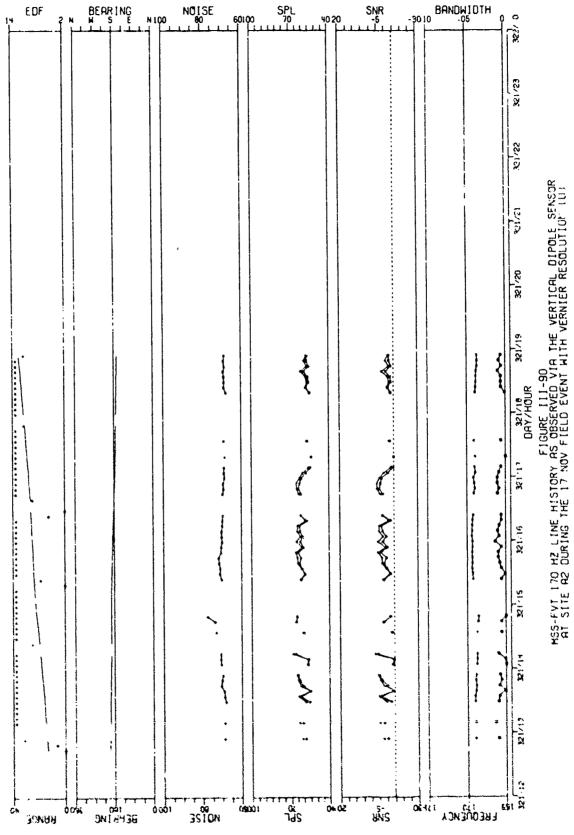
AS-77-2688

Andrew Branch



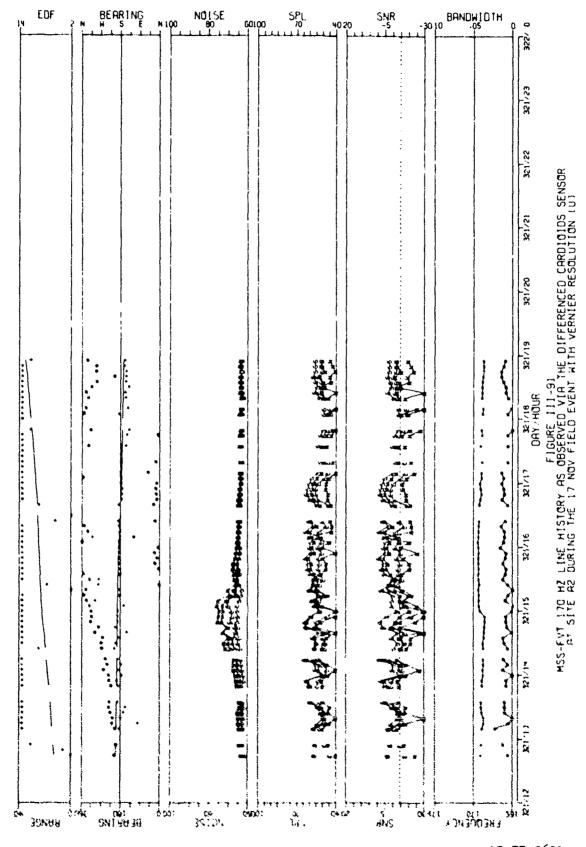
the second second second reactions are second secon

AS-77-2689

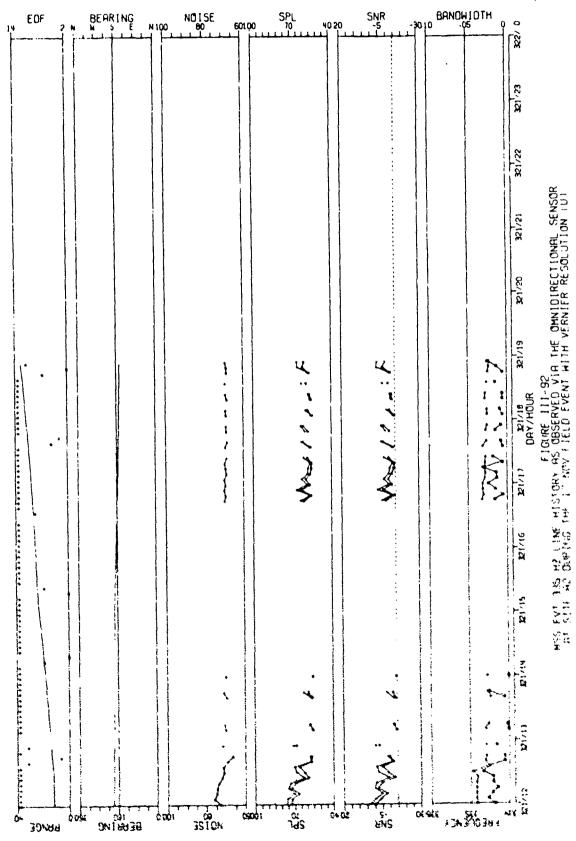


and the state of the state of the state of the state of the state of the state of the state of the state of the

AS-77-2690

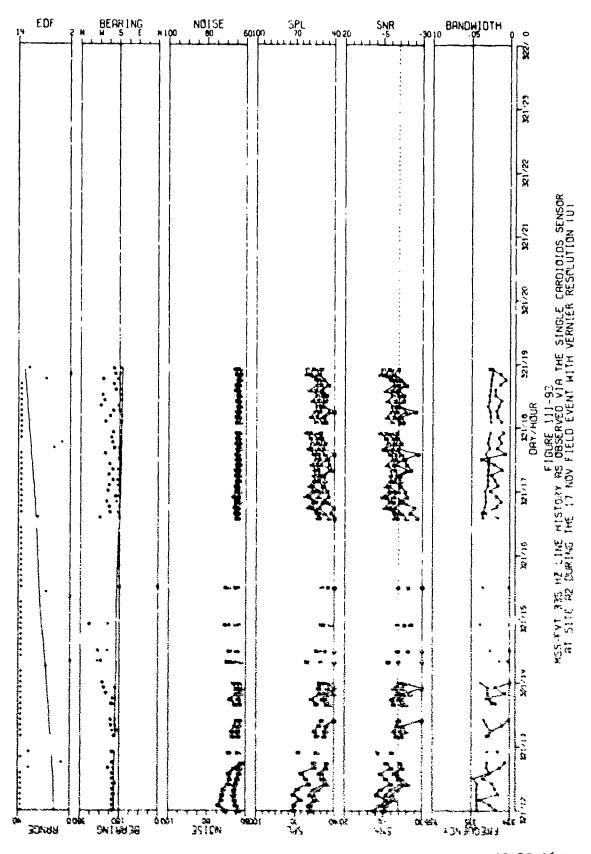


AS-77-2691

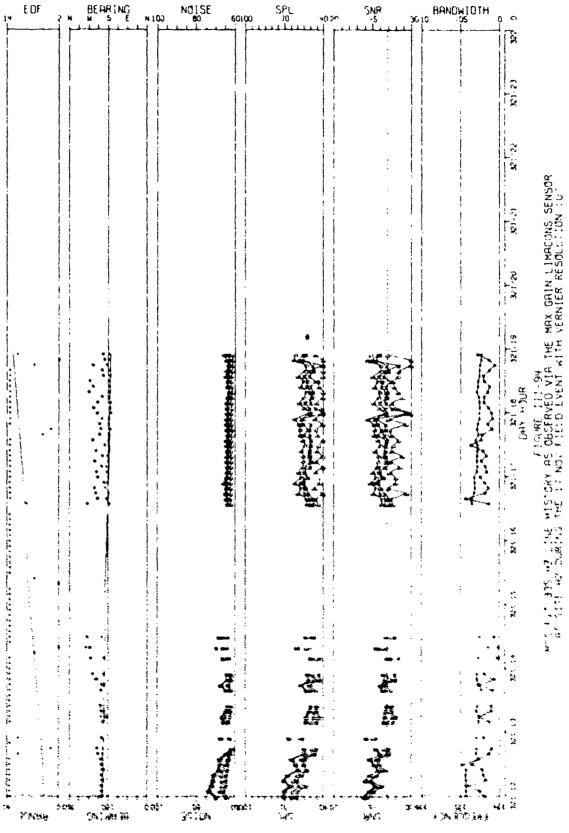


AS-77-2692

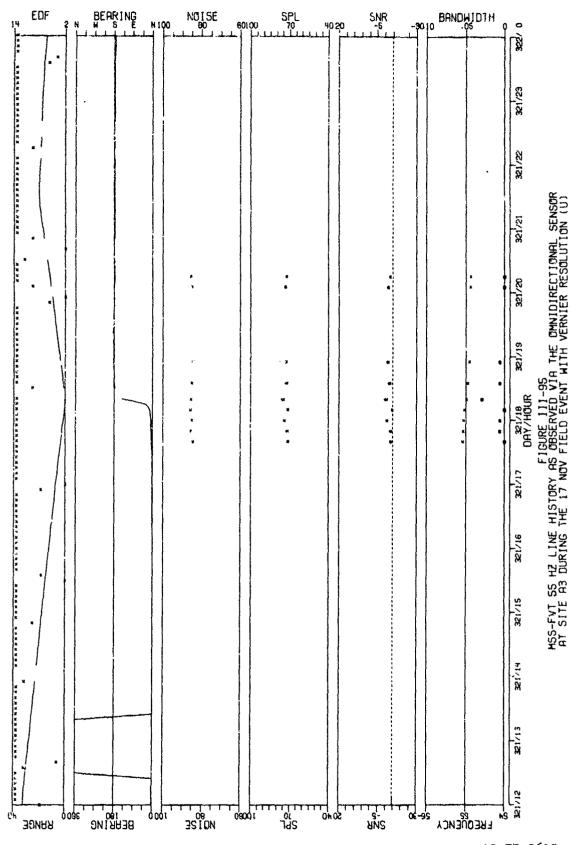
CONFIDENTIAL



AS-77-2693

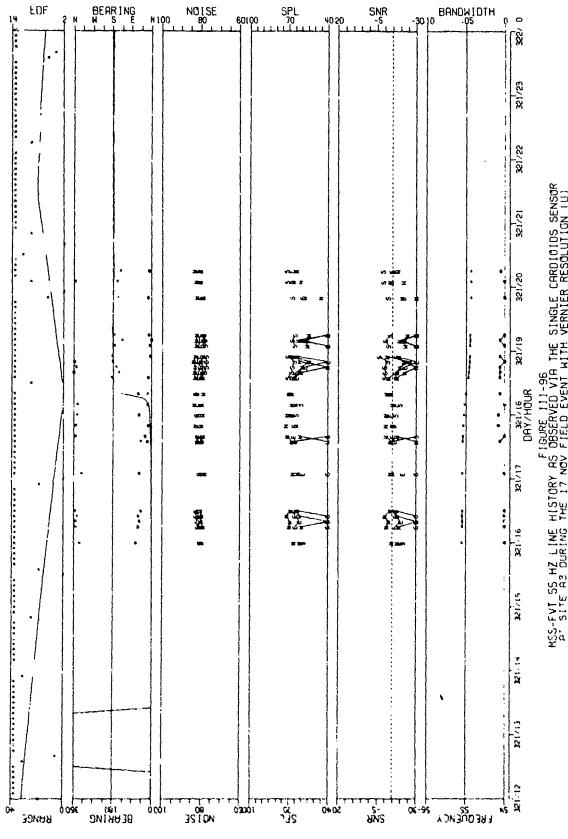


AS-77-2694

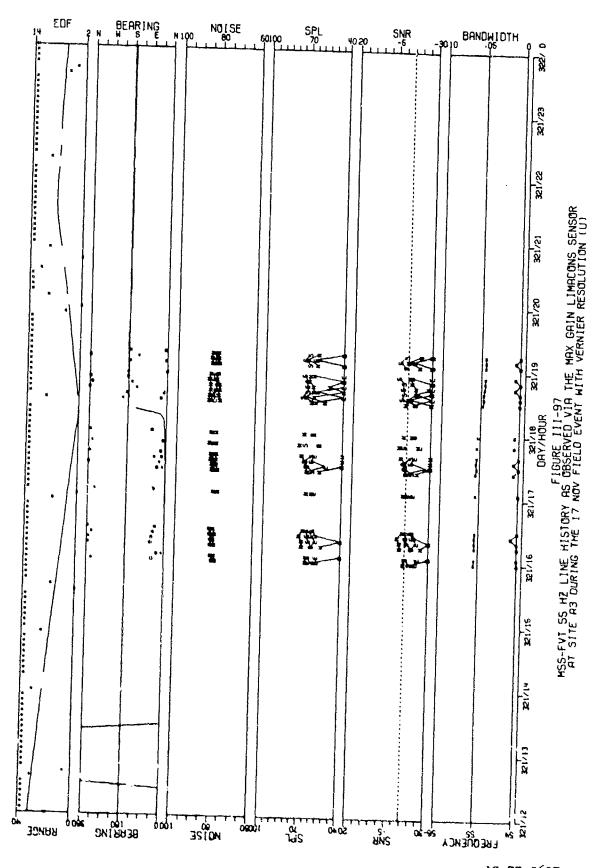


AS-77-2695

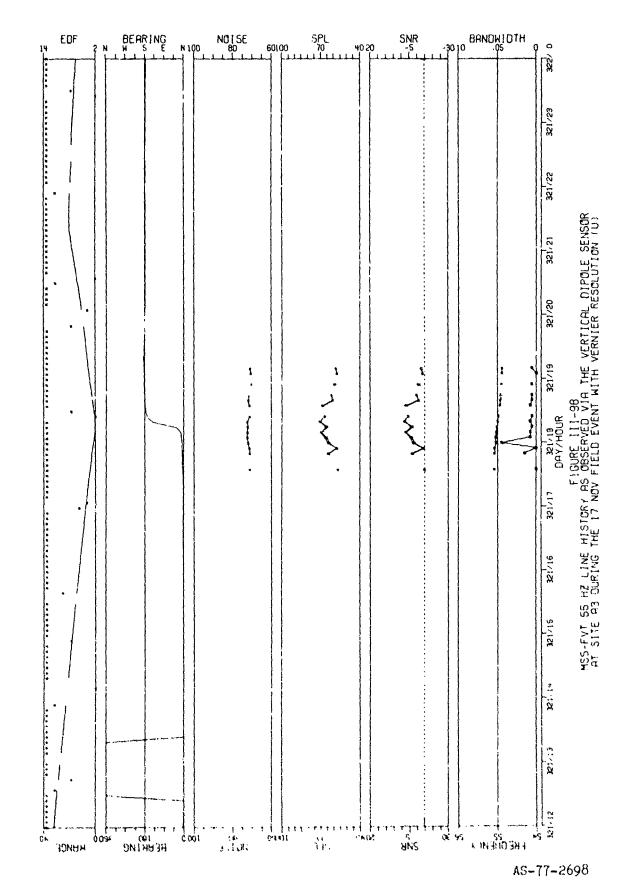
C INFIDENTIAL



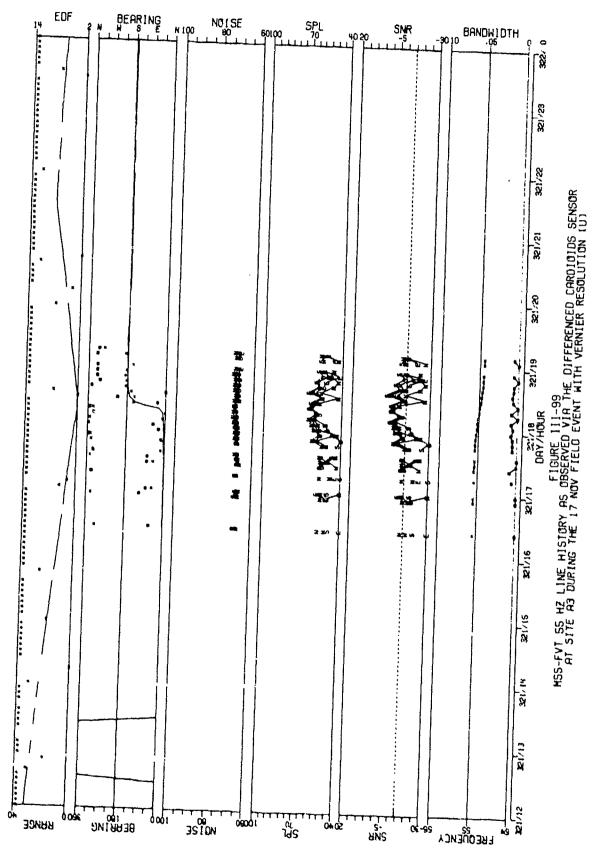
AS-77-2696



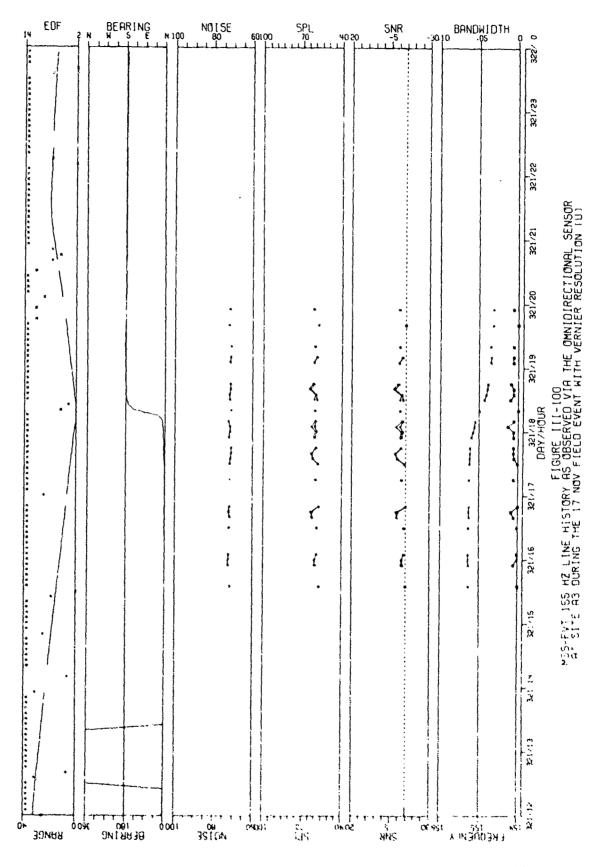
AS-77-2697



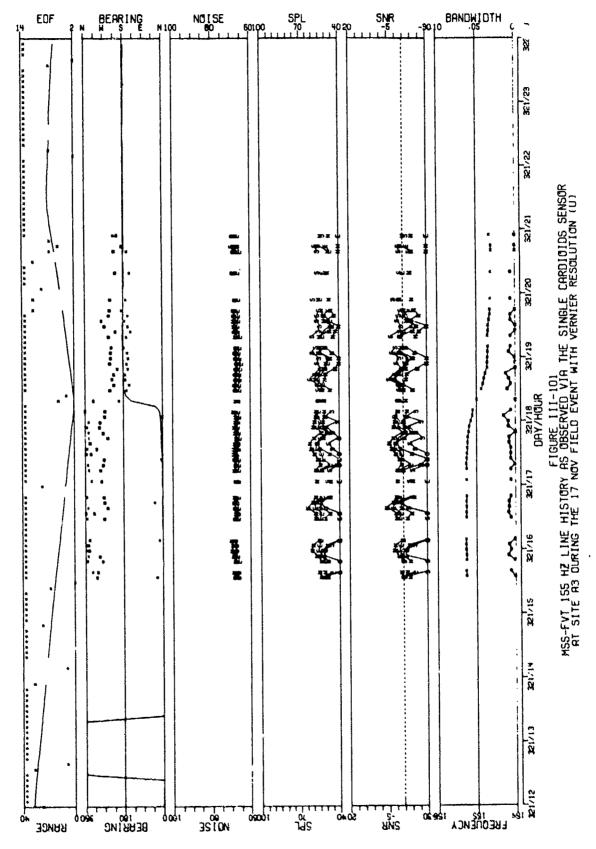
CONFIDENTIAL



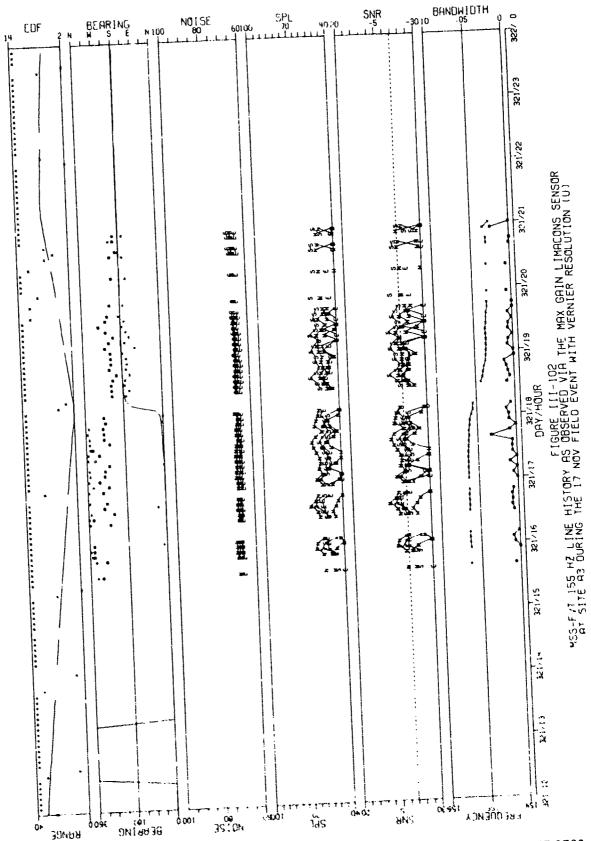
AS-77-2699



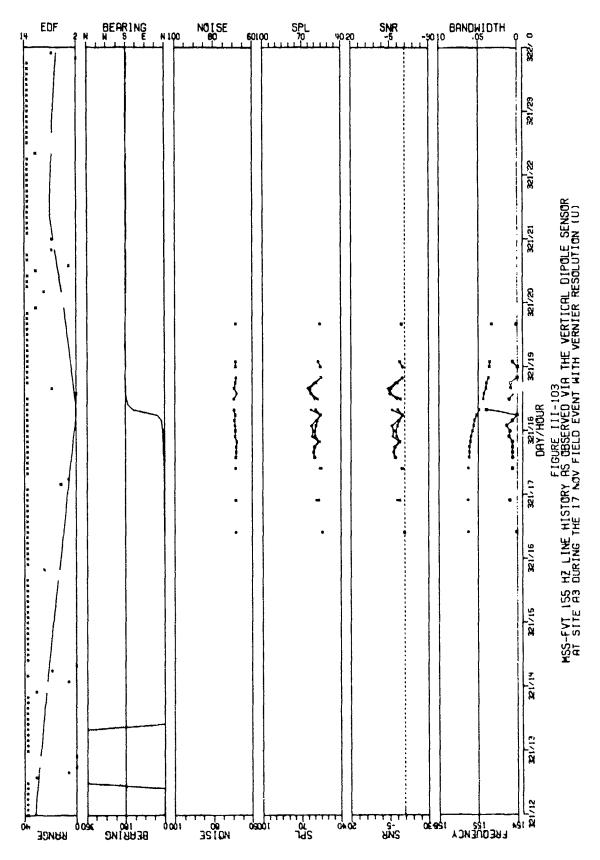
AS-77-2700



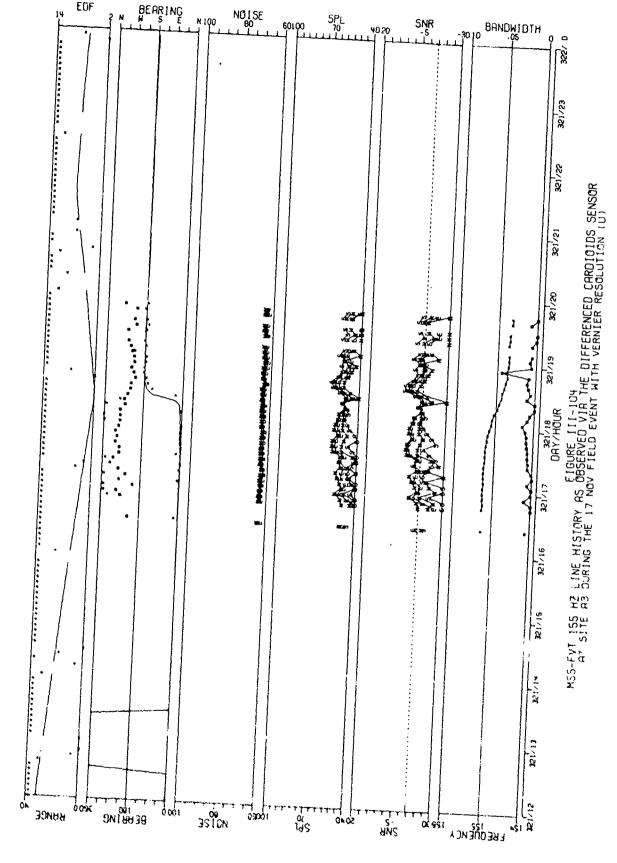
AS-77-2701



AS-77-2702

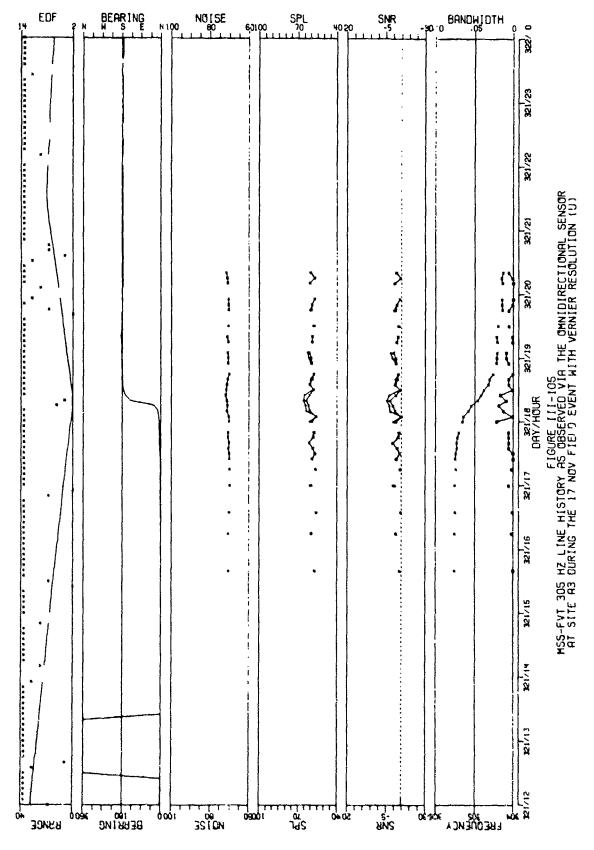


AS-77-2703

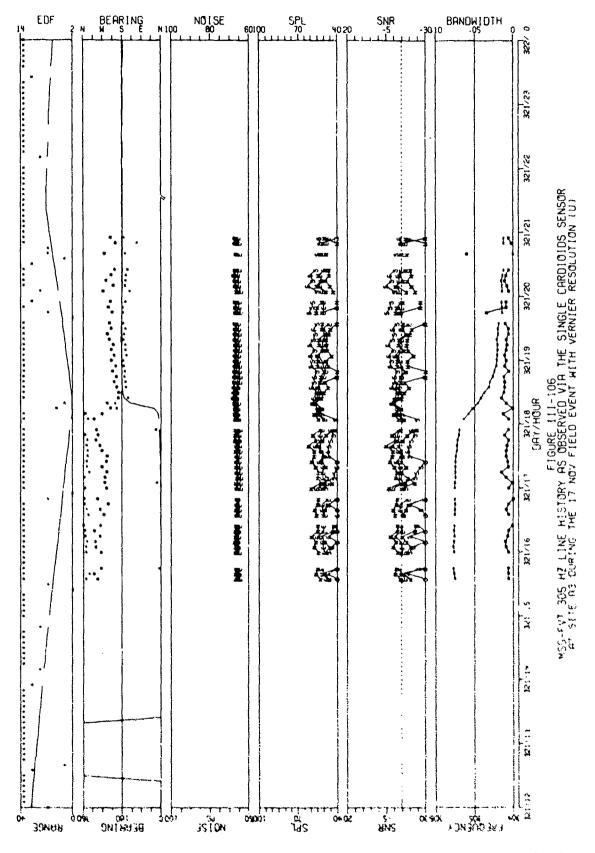


CONTRACTOR SECTIONS OF THE SECTION

AS-77-2704

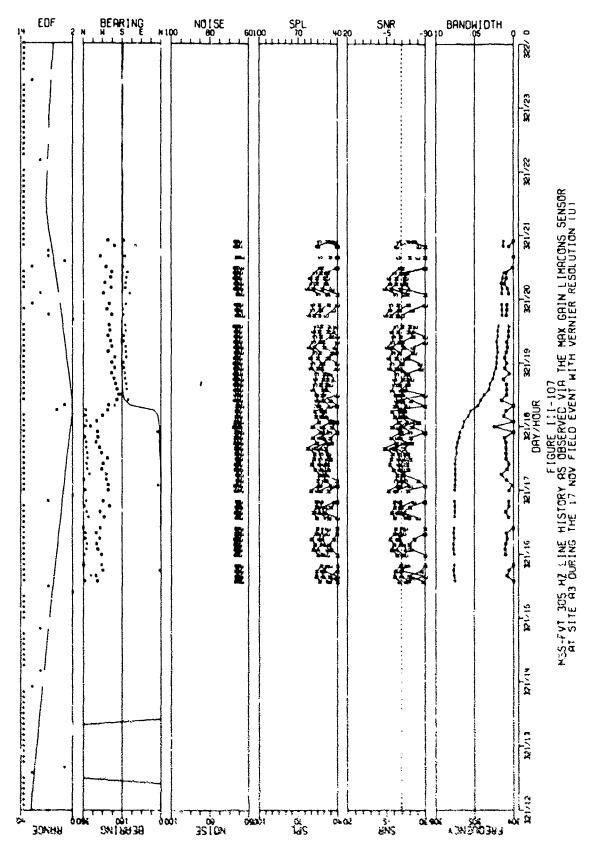


AS-77-2705

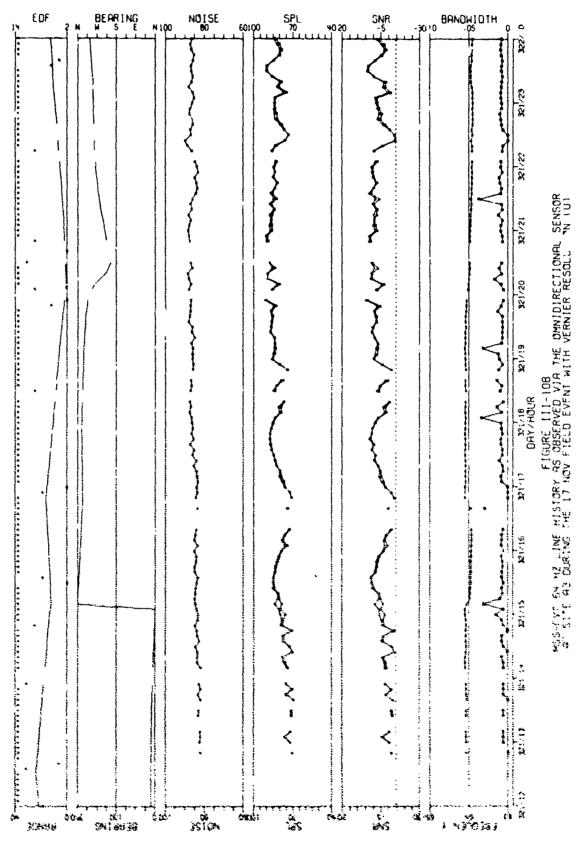


the first the state of the stat

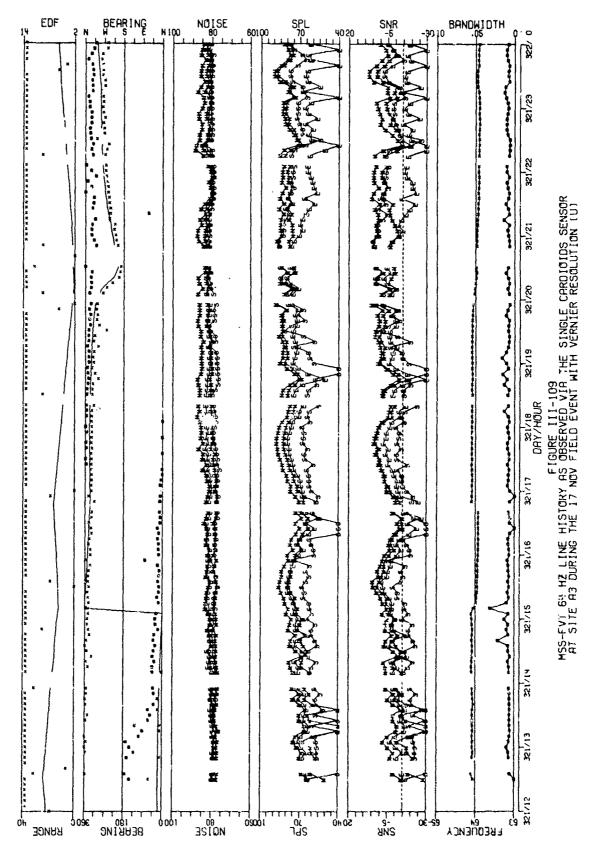
AS-77-2706



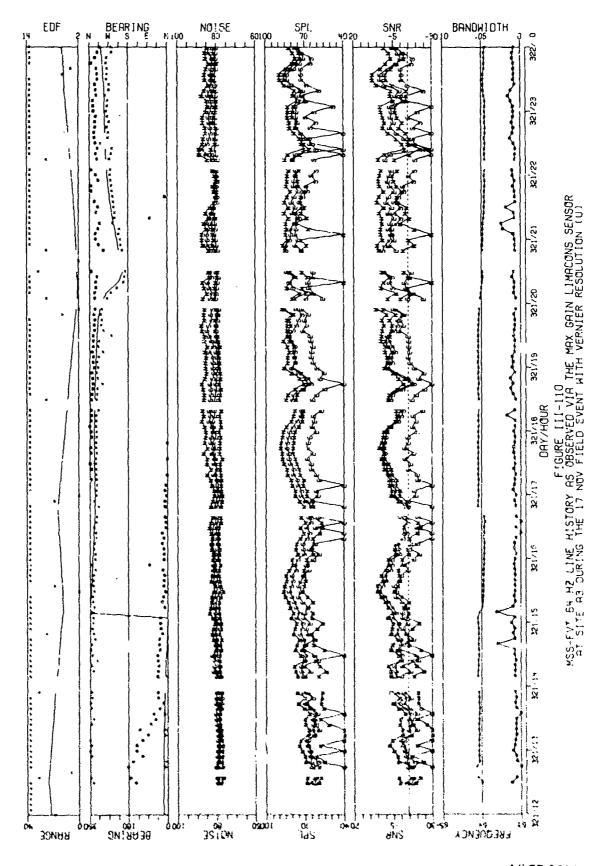
AS-77-2707



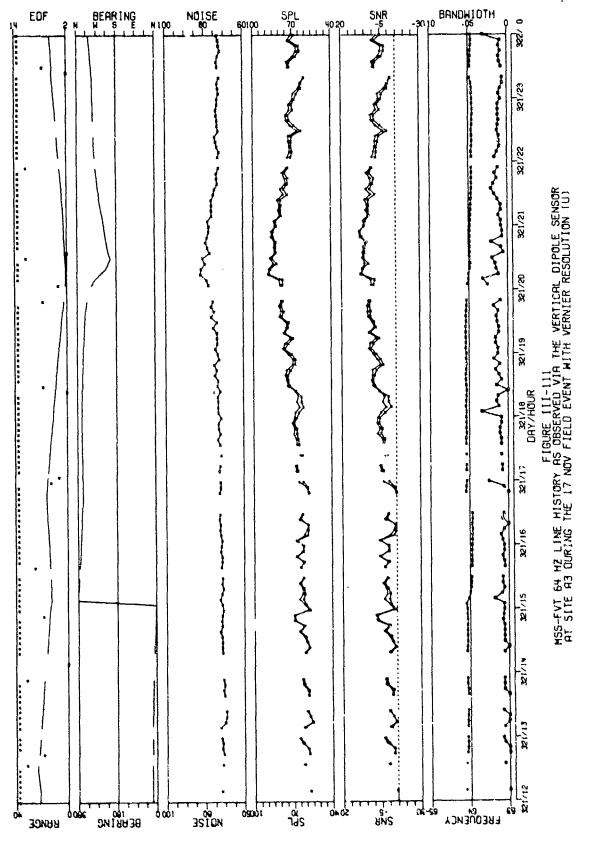
AS-77-2708



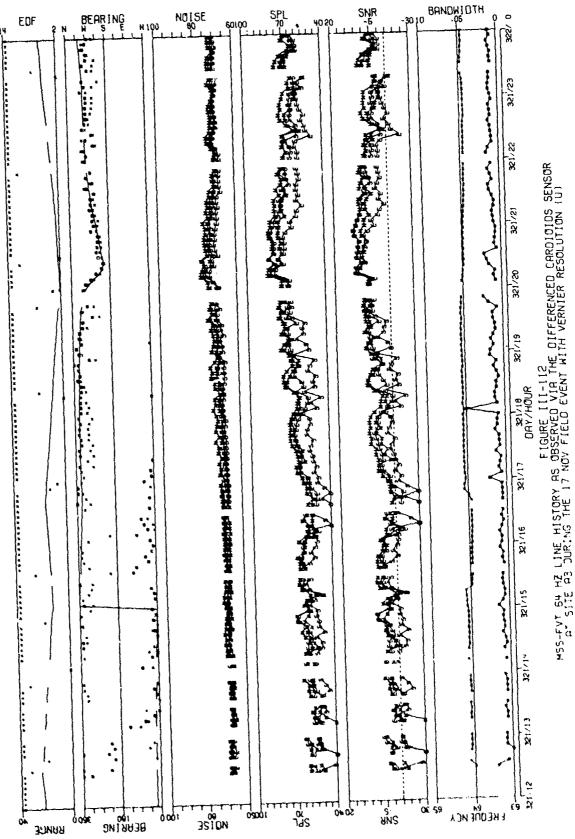
AS-77-2709



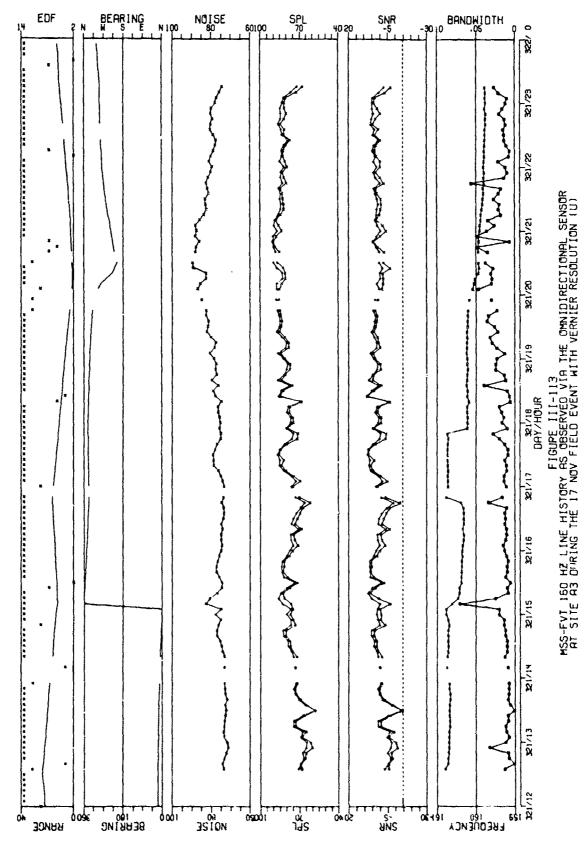
AS-77-2710



AS-77-2711



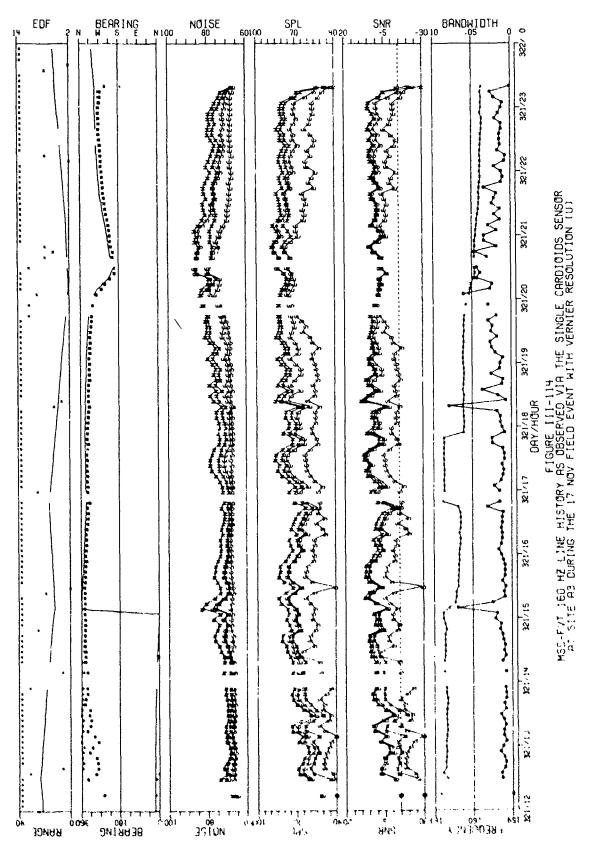
AS-77-2712



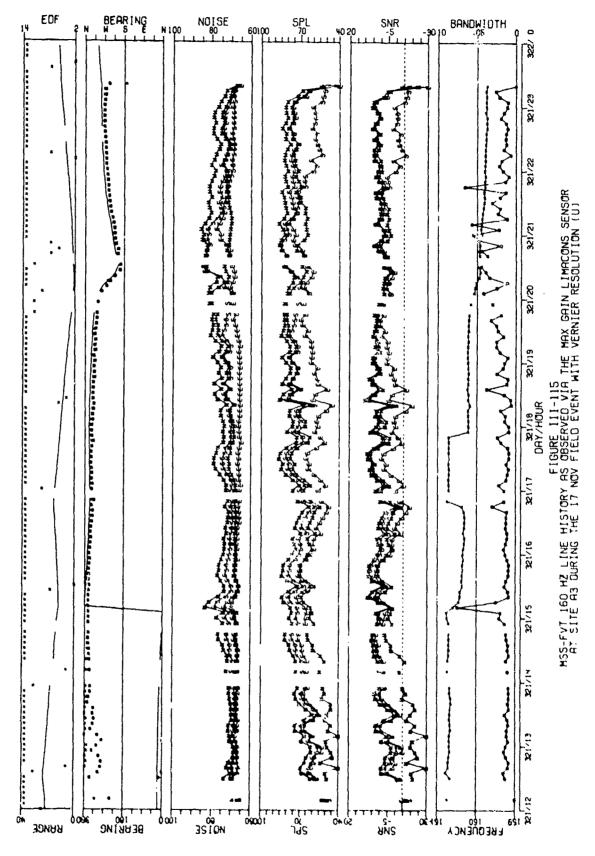
AS-77-2713

CONFIDENTIAL

The same of the sa



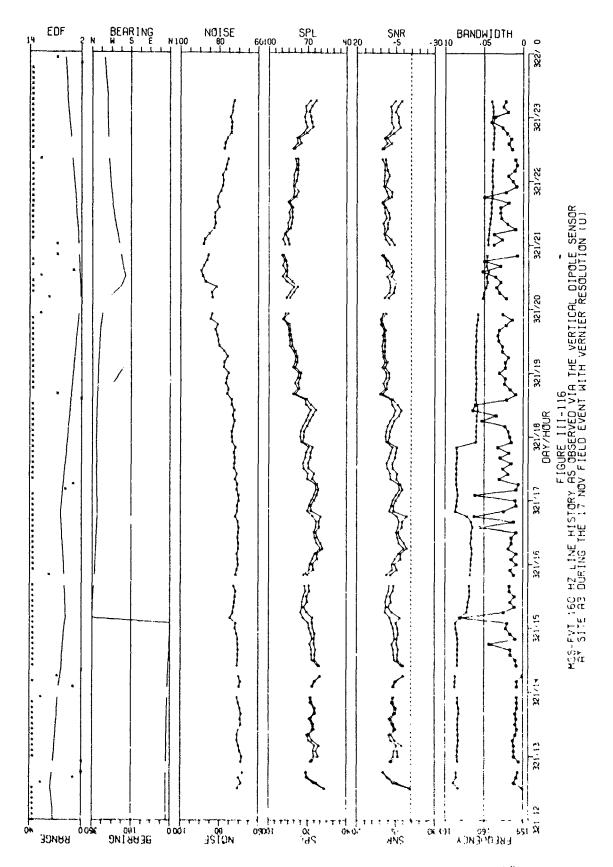
AS-77-2714



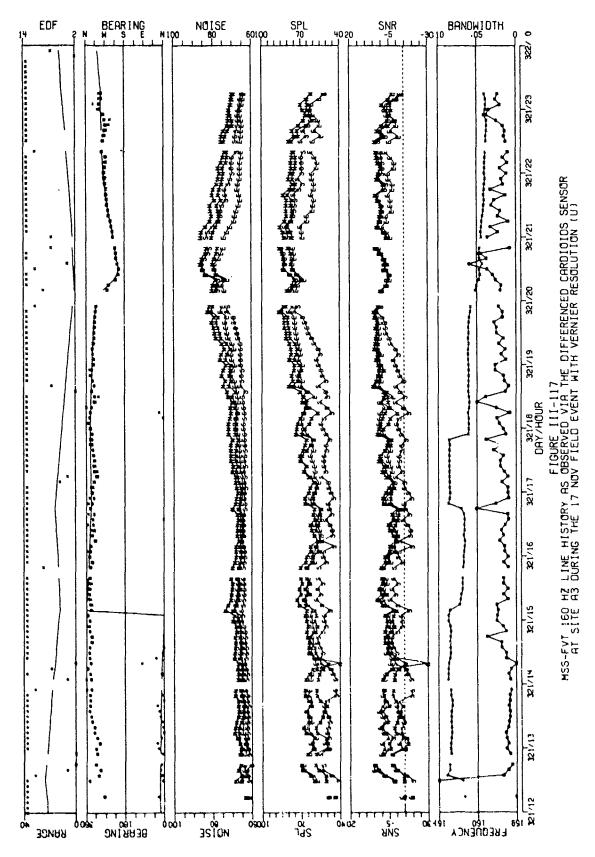
AS-77-2715

CONFIDENTIAL

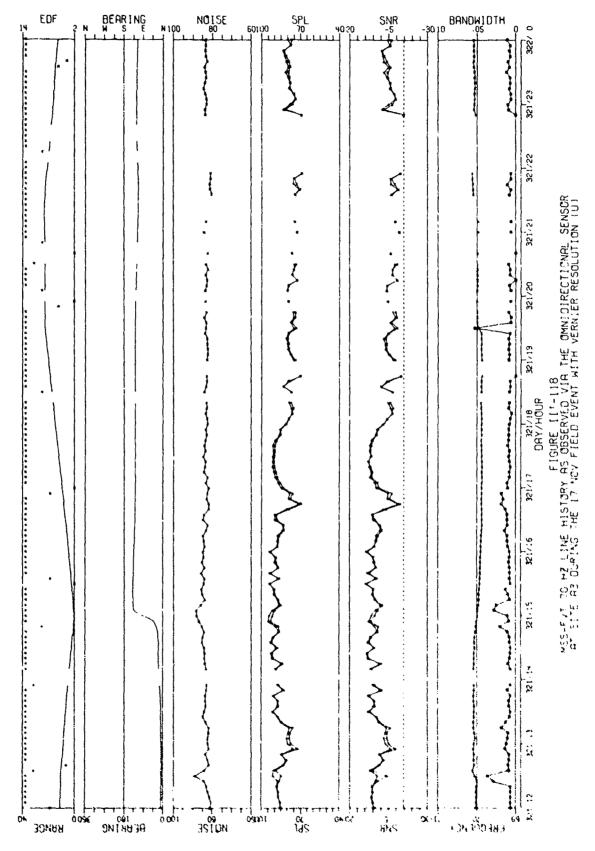
Britanes and a constant



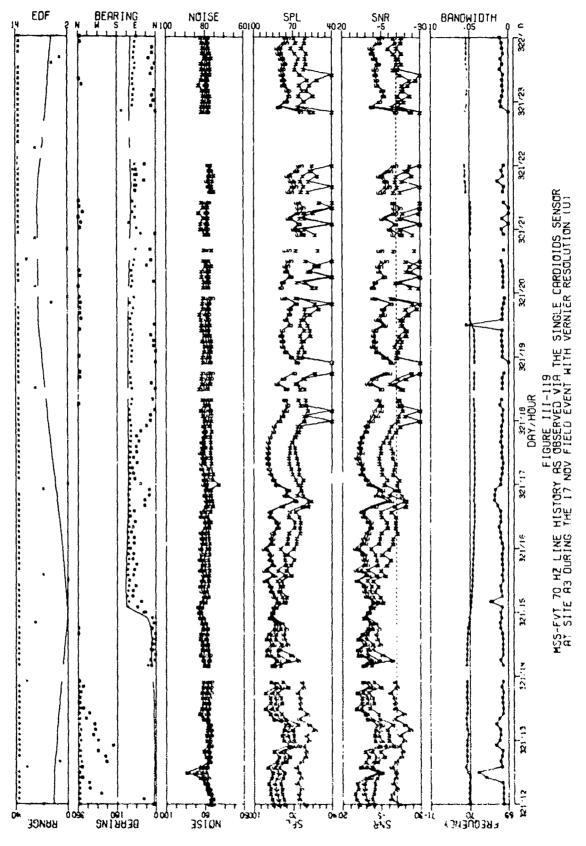
AS-77-2716



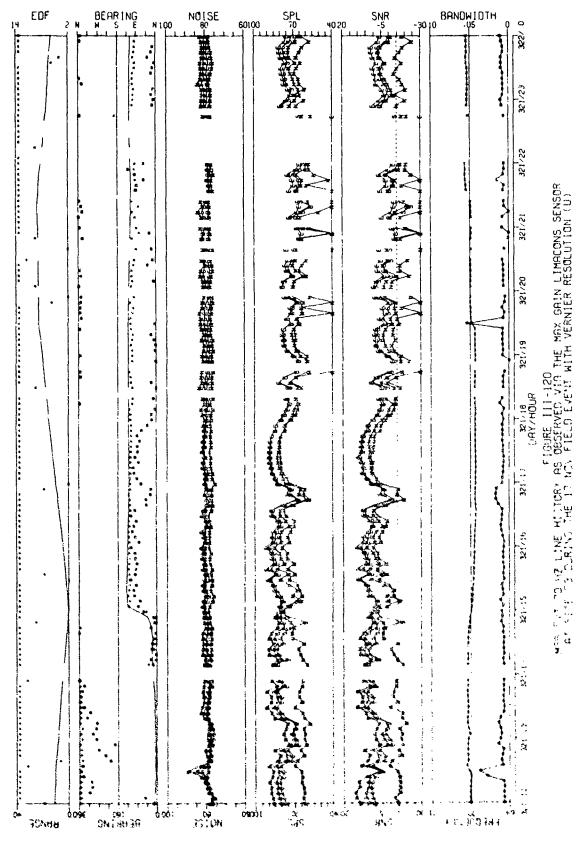
AS-77-2717



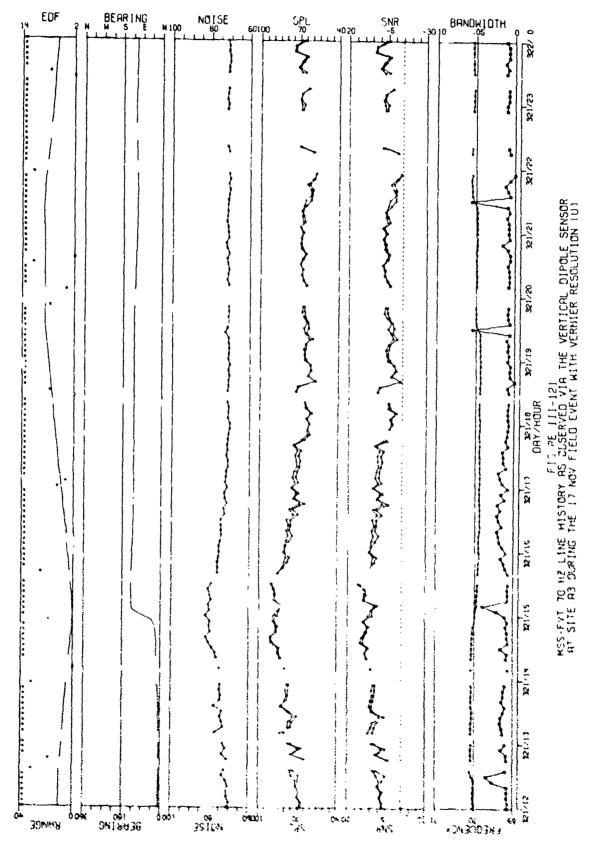
AS-77-2718



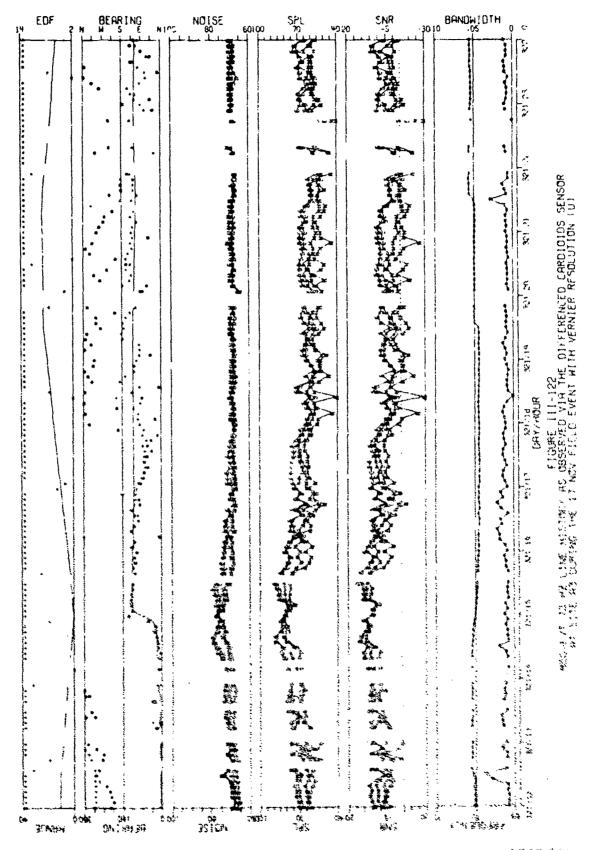
AS-77-2719



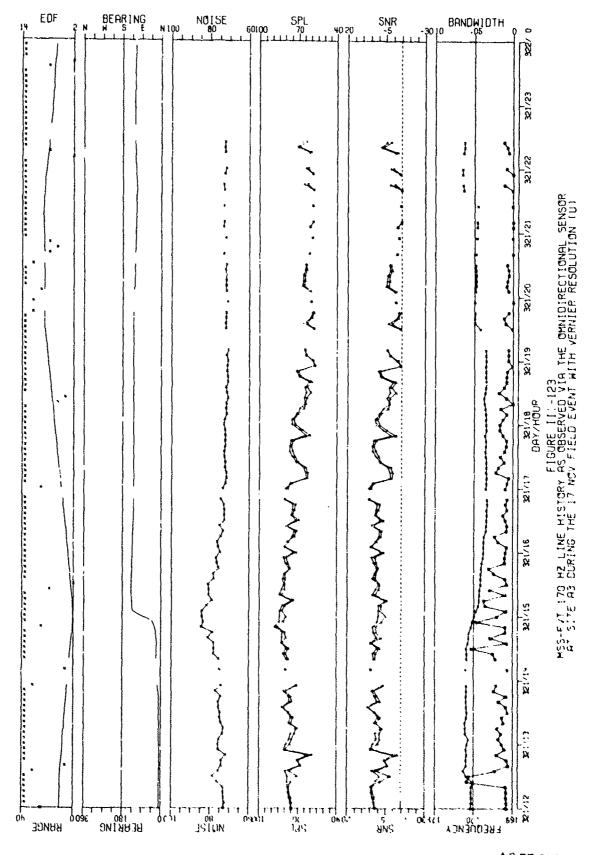
AS-77-2720



AS-77-2721

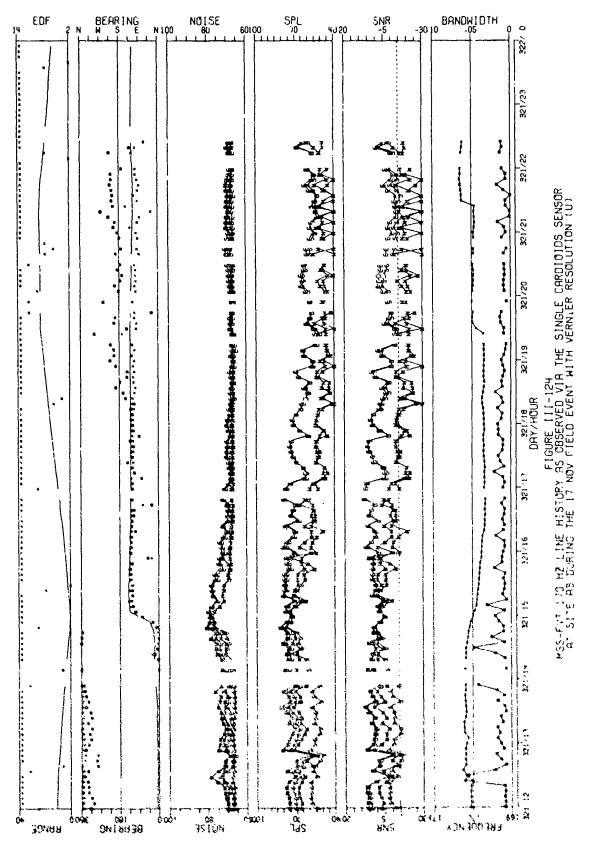


AS-77-2722

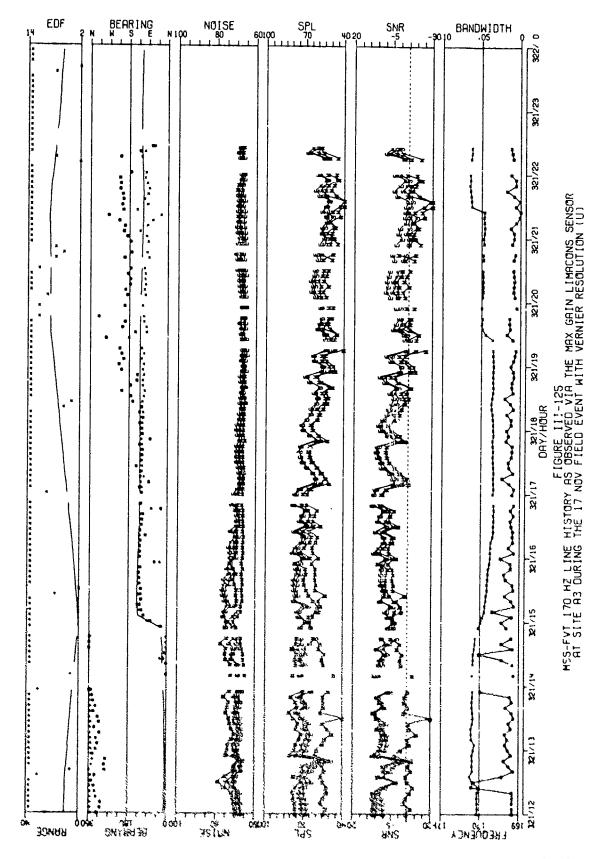


CONFIDENTIAL

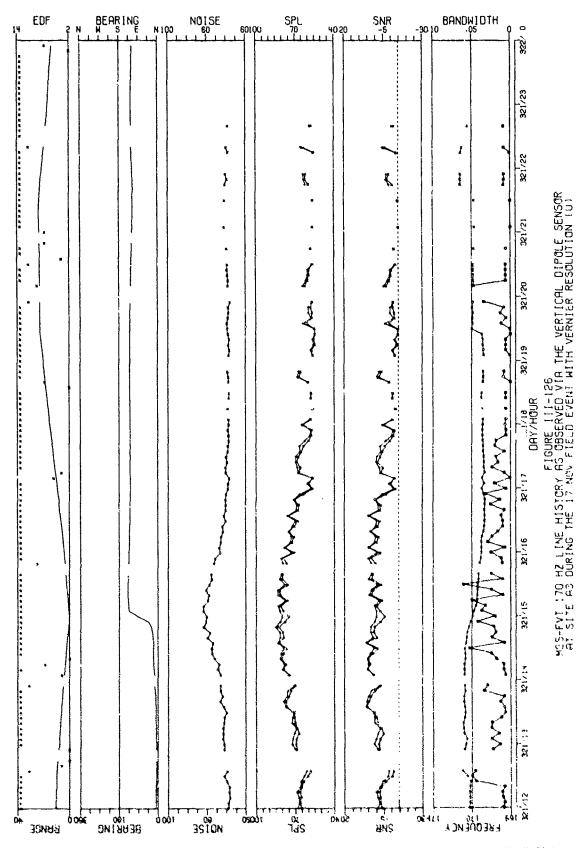
AS-77-2723



AS-77-2724

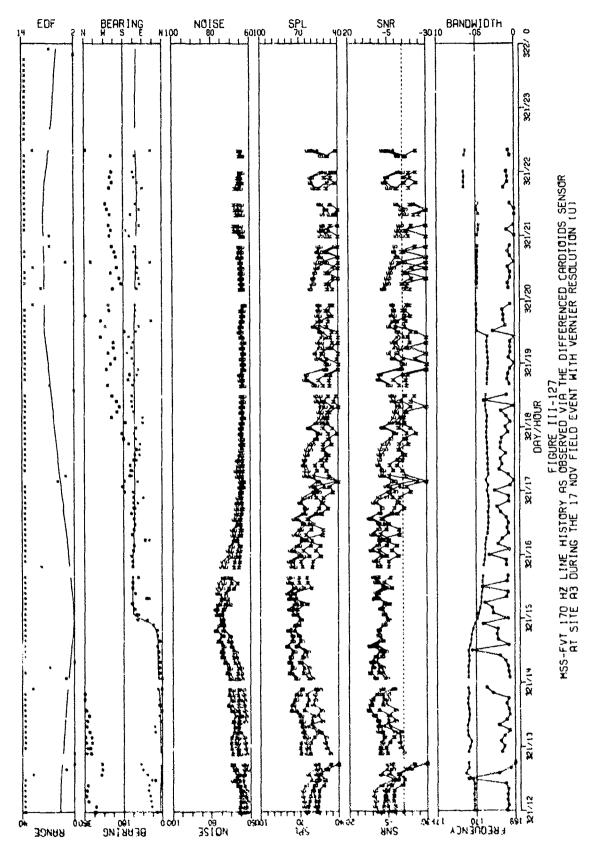


AS-77-2725



AS-77-2726

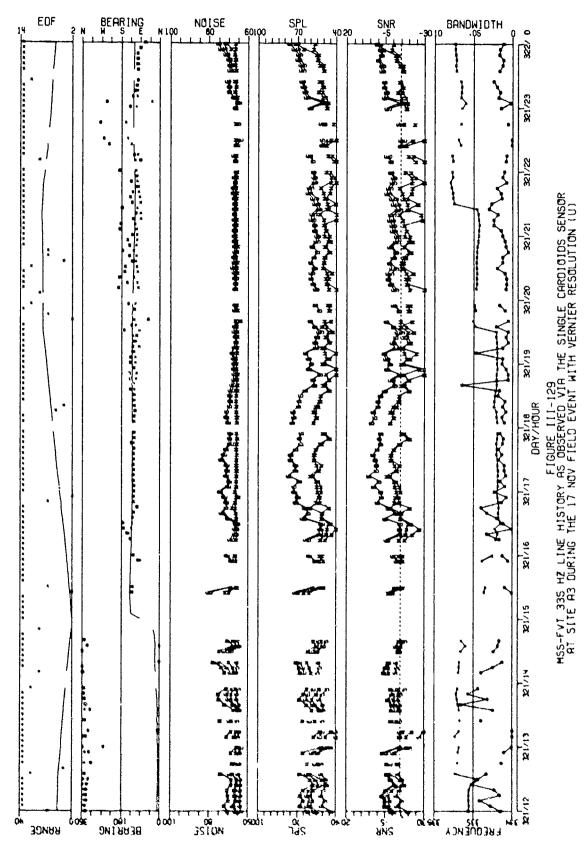
CONFIDENTIAL



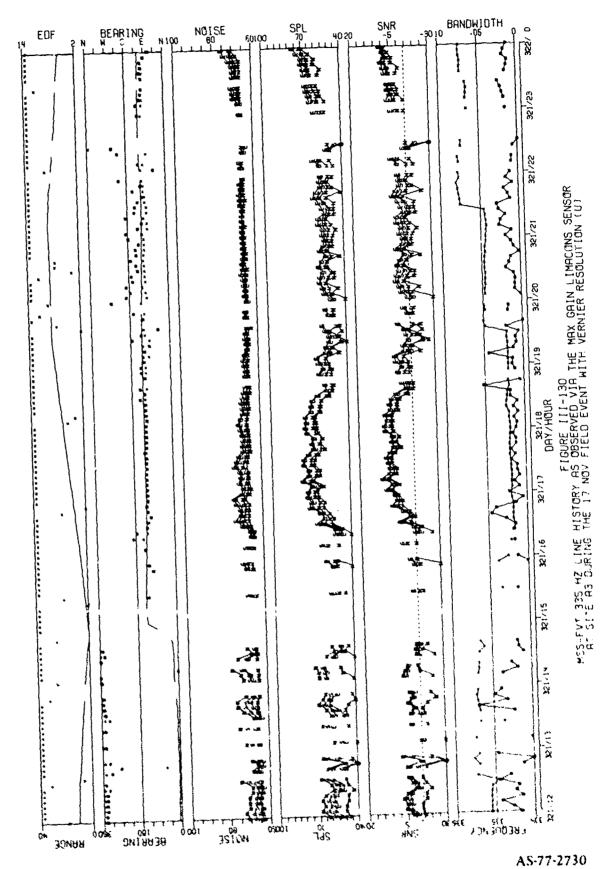
AS-77-2727

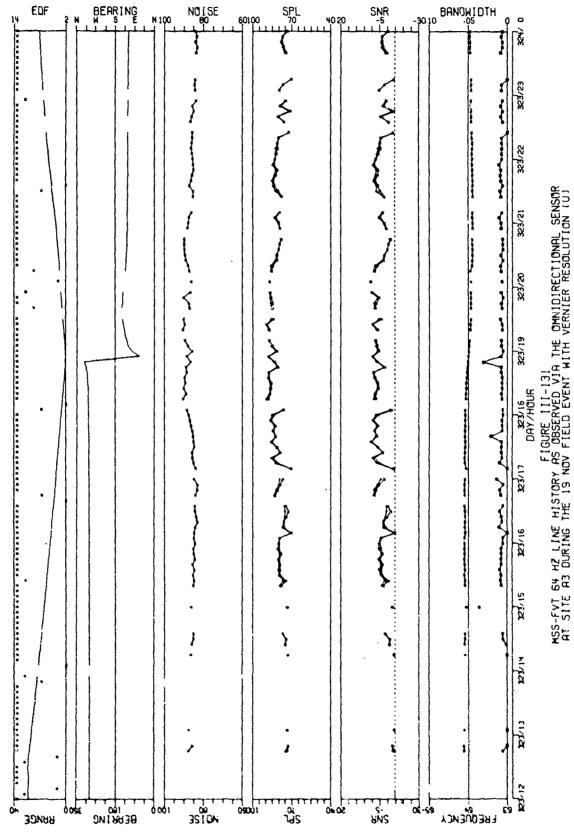


AS-77-2728



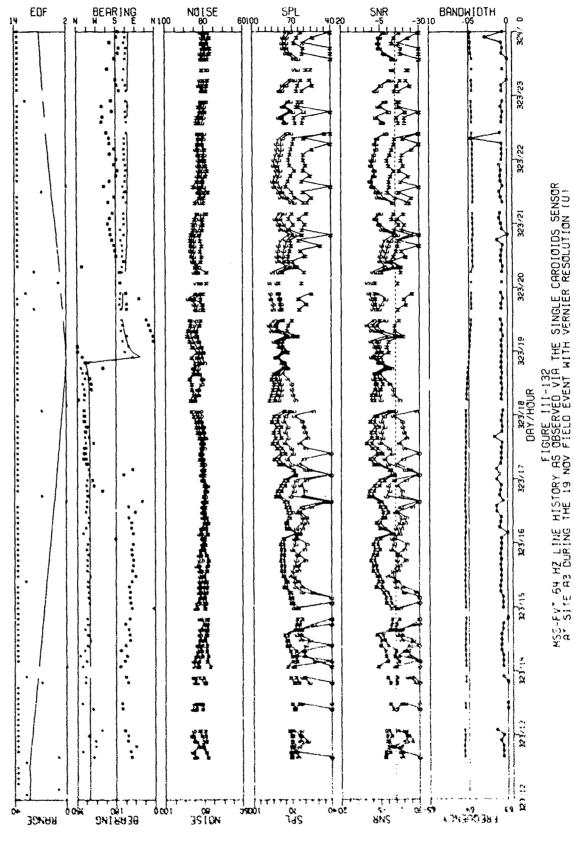
AS-77-2729



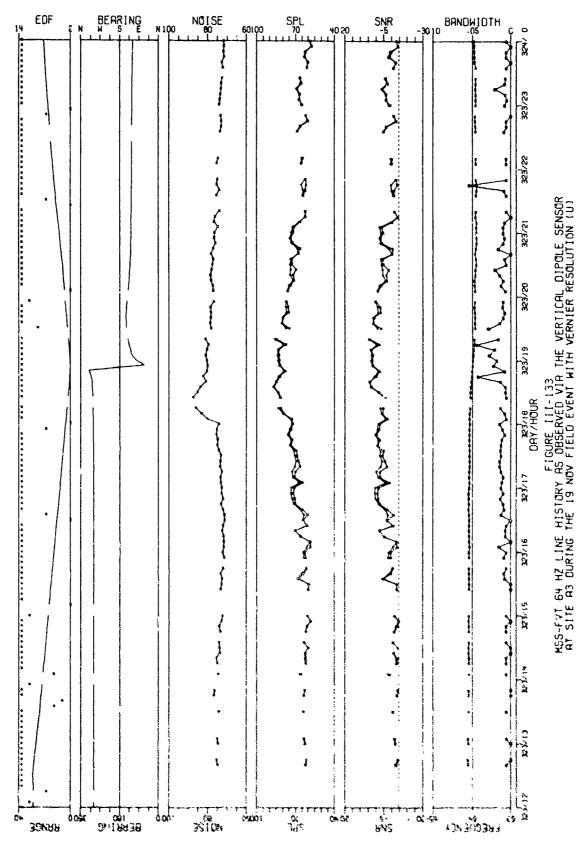


AS-77-2731

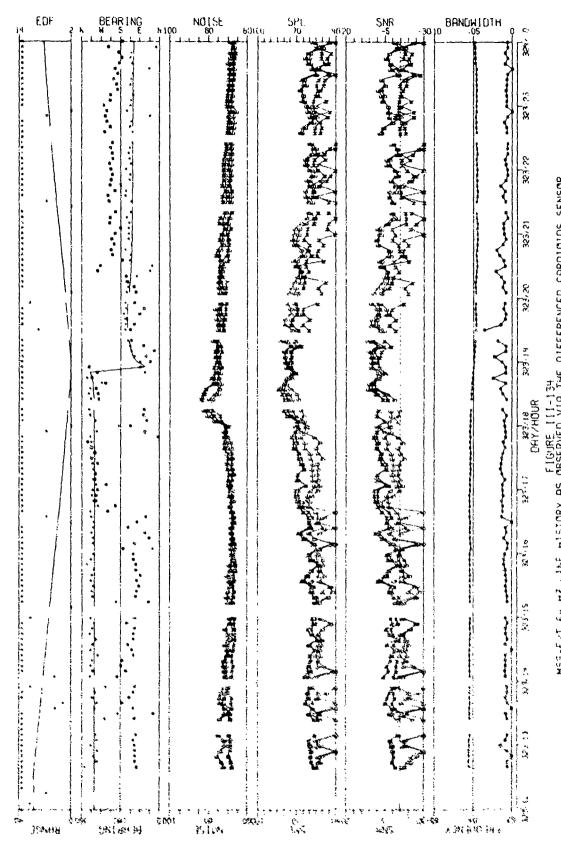
\$ 16.30 \$ The St.



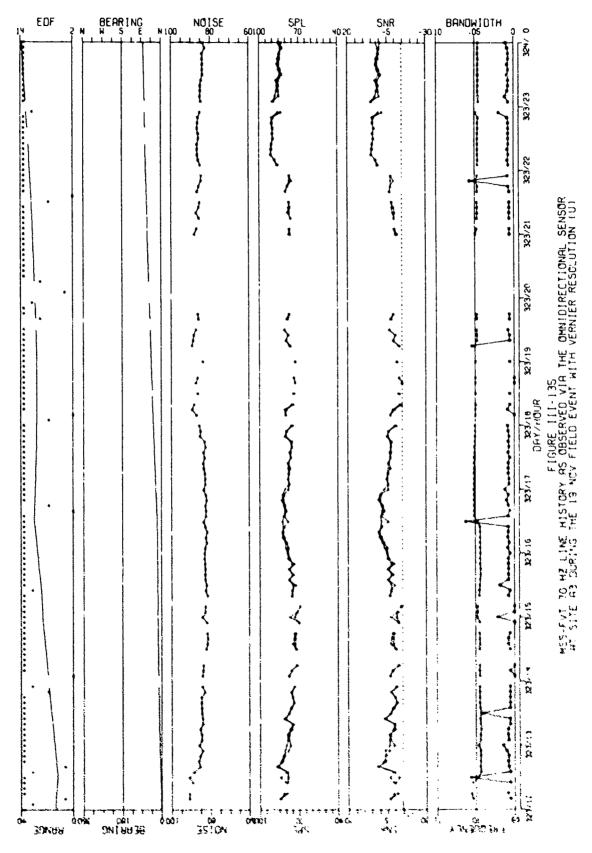
AS-77-2732



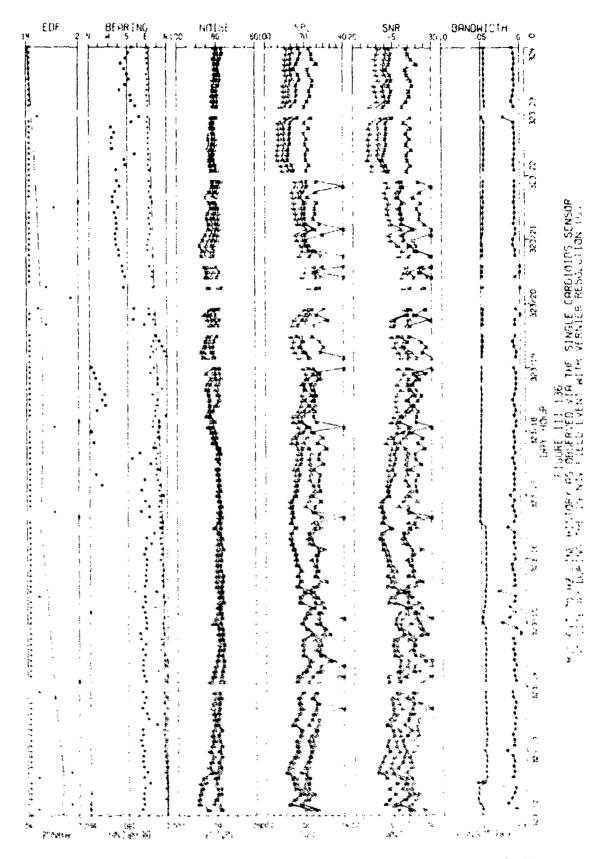
AS-77-2733



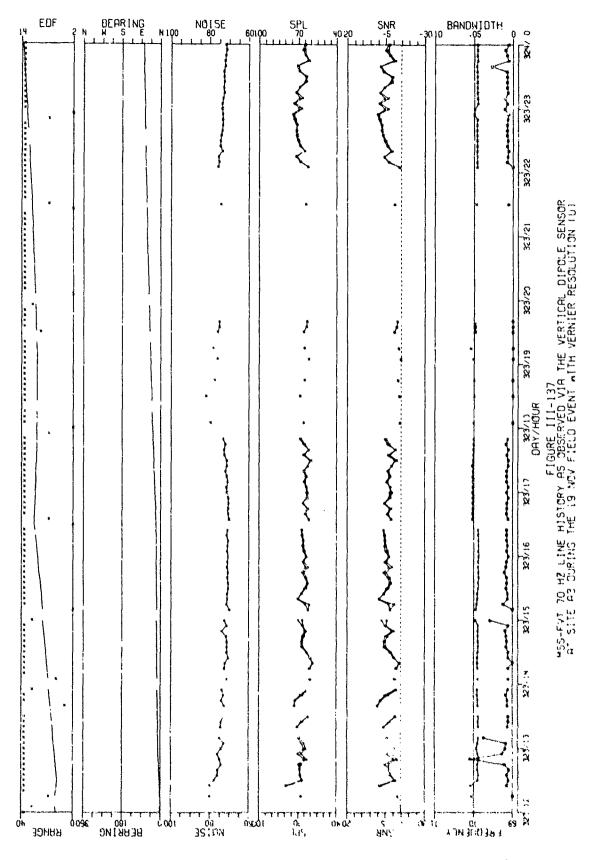
AS-77-2734



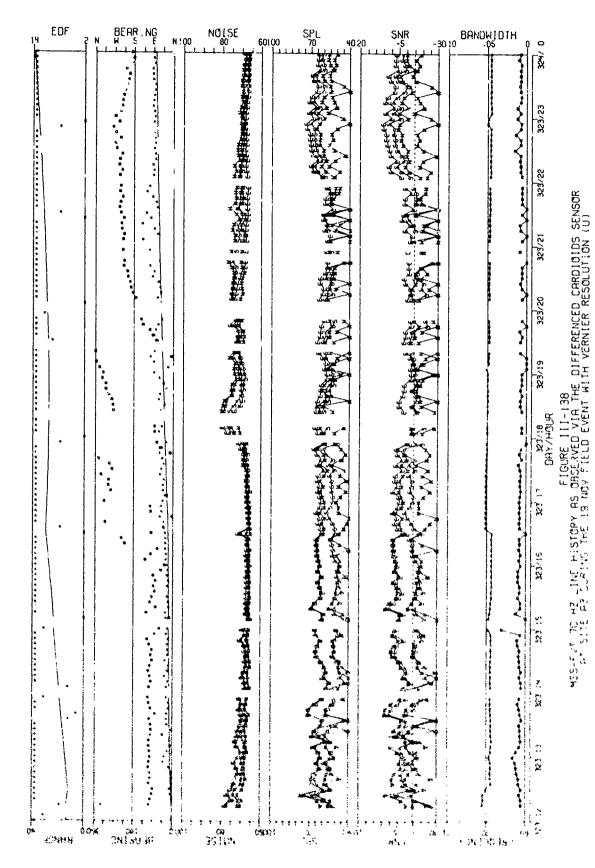
15-77-2735



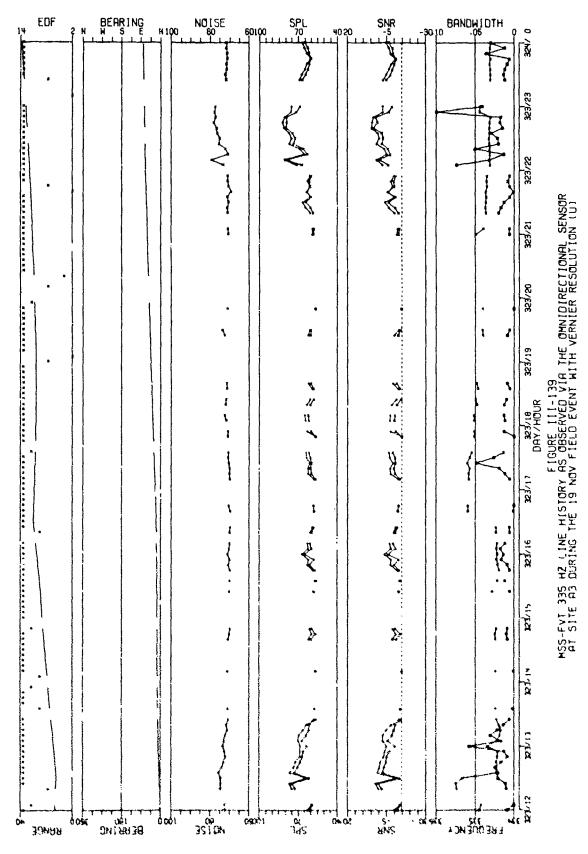
AS-77-2736



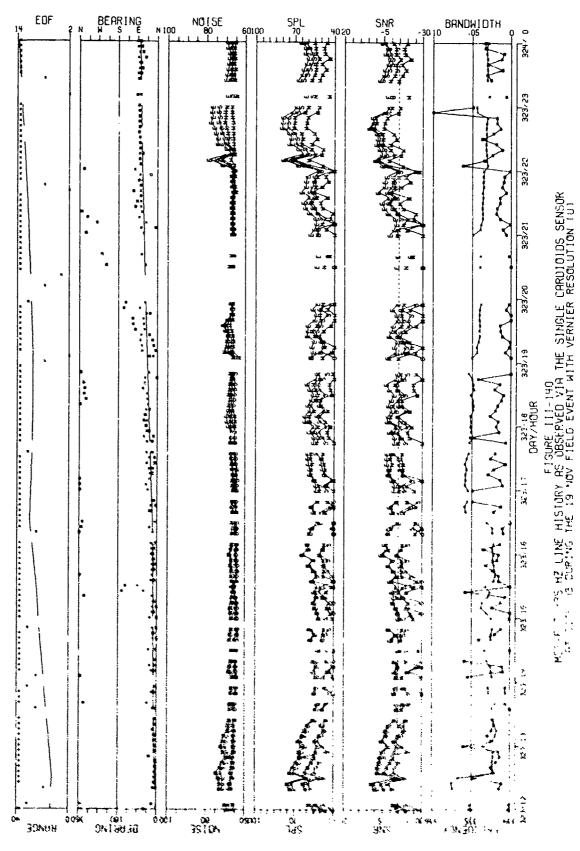
AS-77-2737



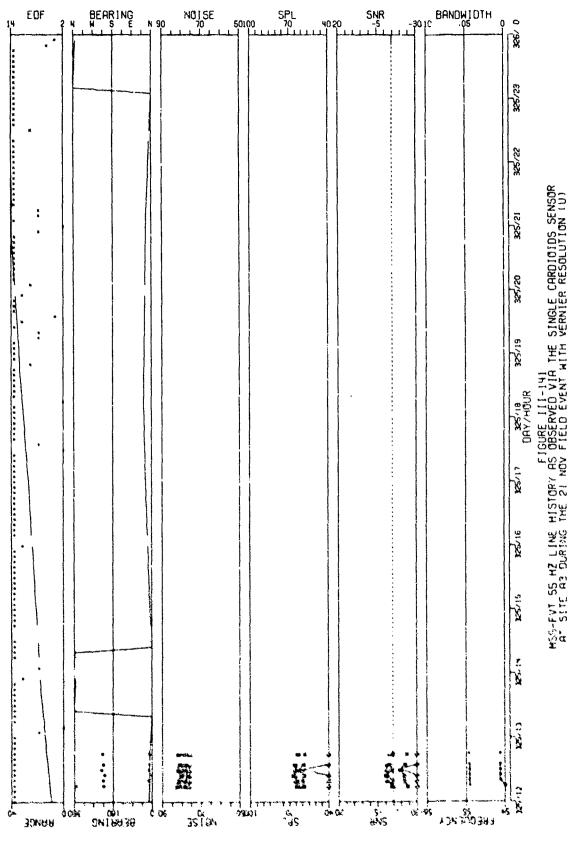
AS-77-2738



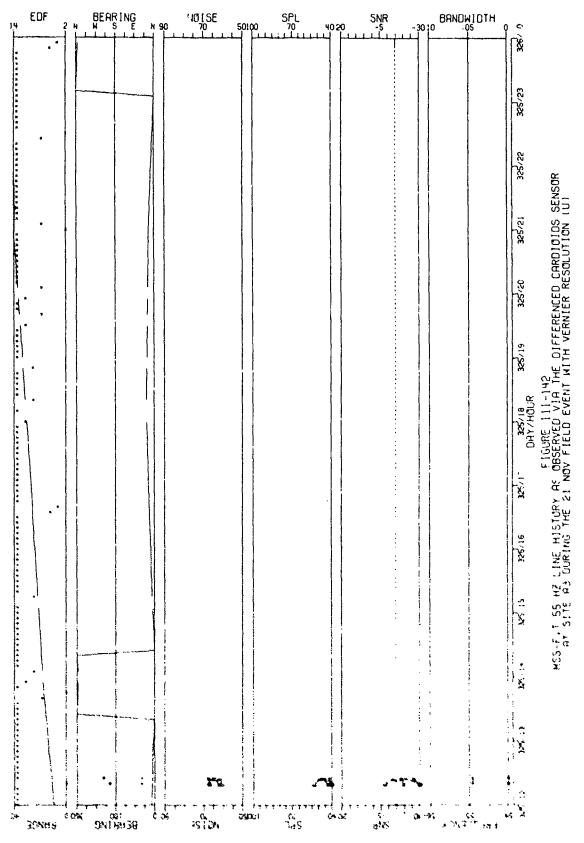
AS-77-2739



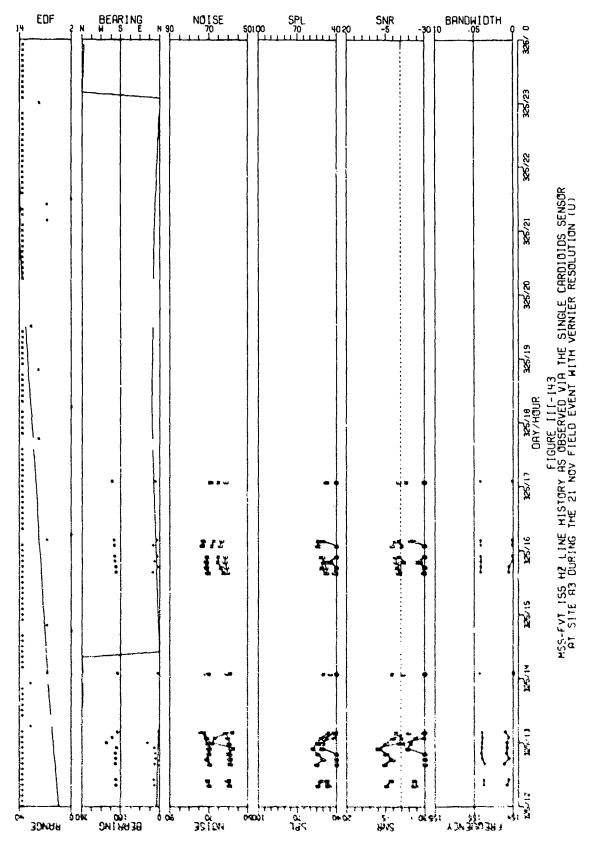
AS-77-2740



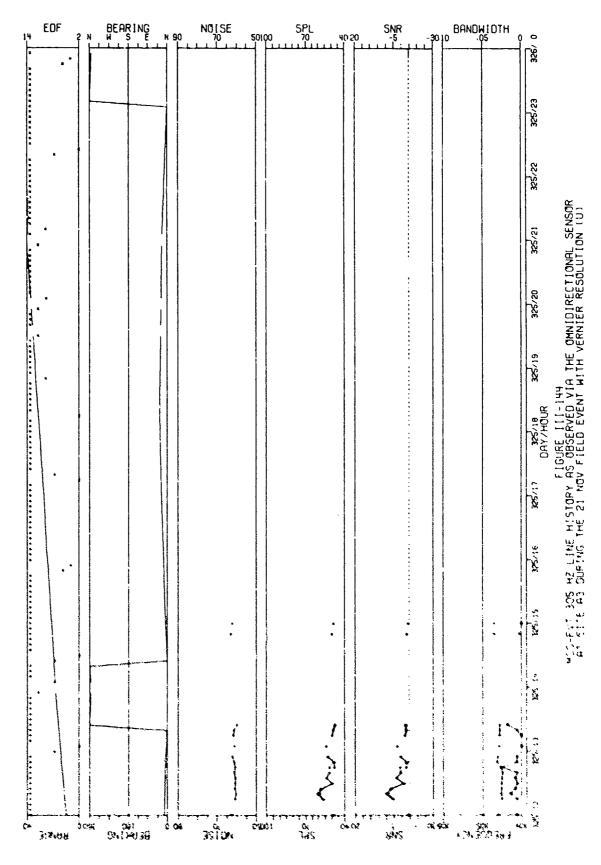
AS-77-2741



AS-77-2742

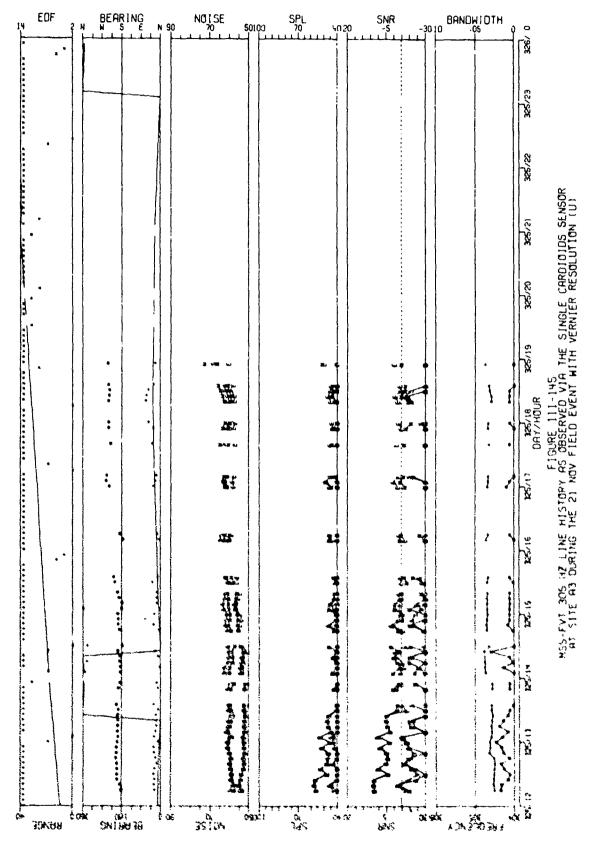


AS-77-2743

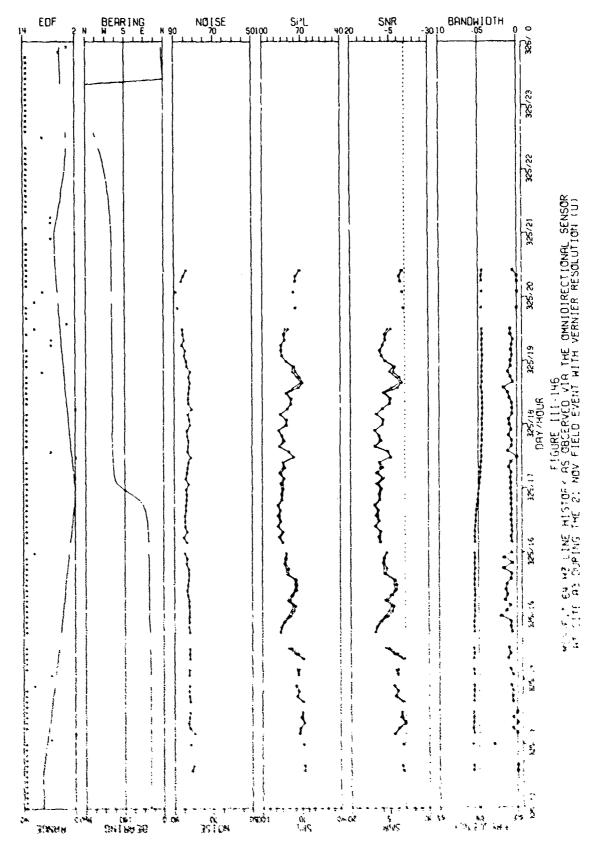


CONFIDENTIAL

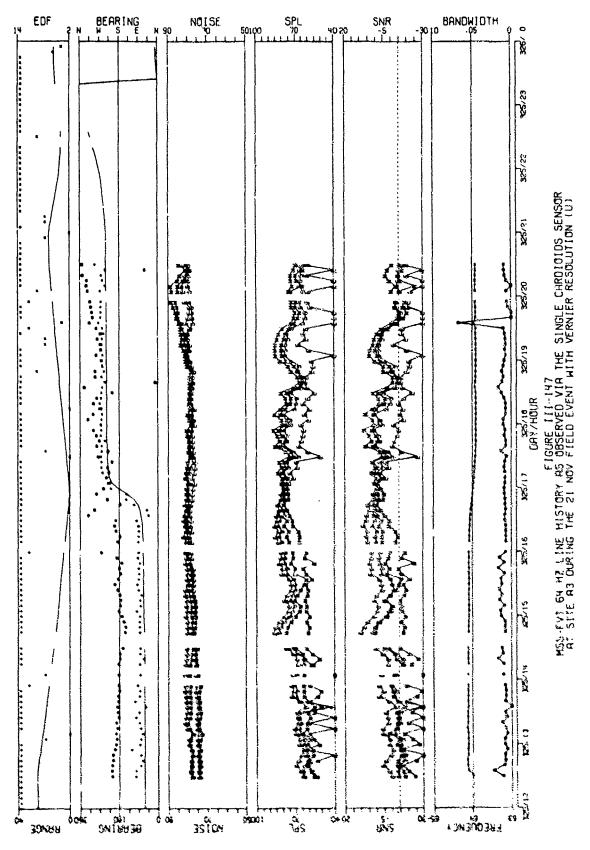
AS-77-2744



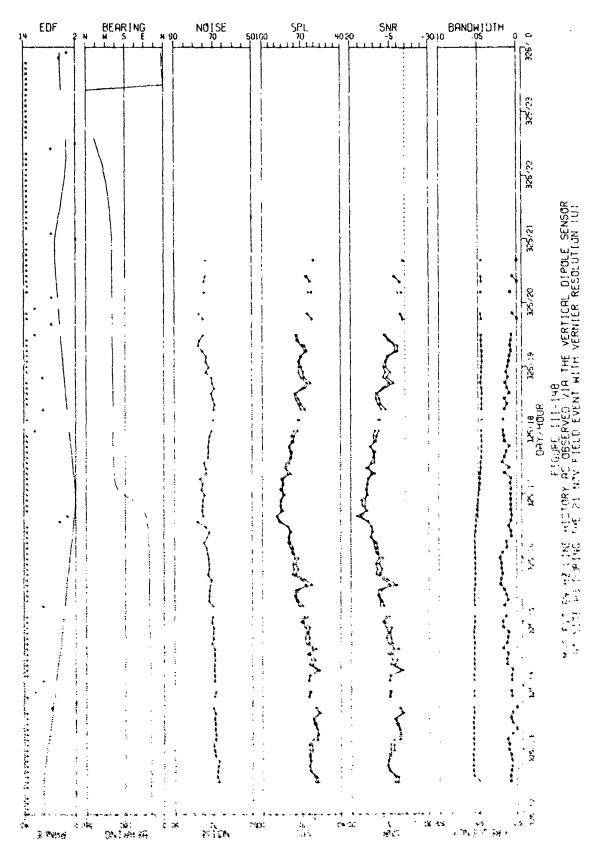
AS-77-2745



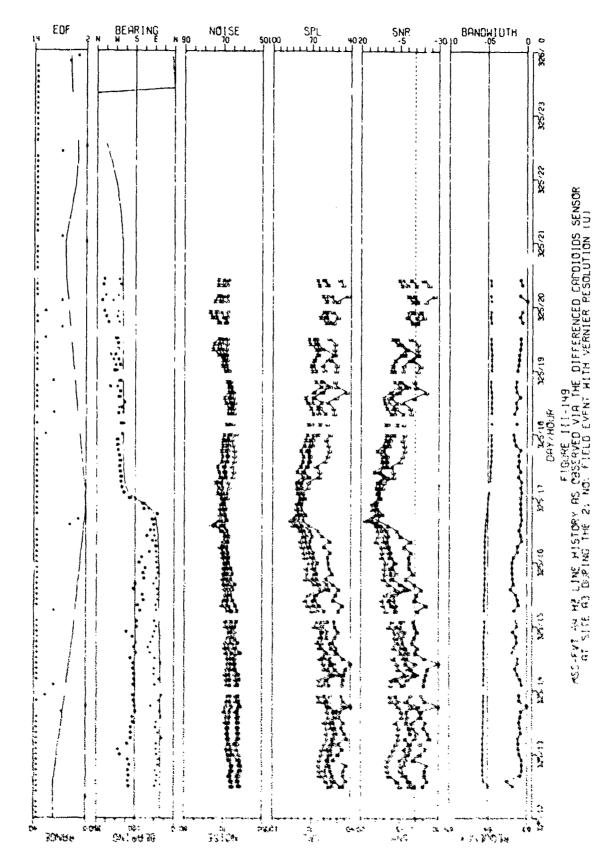
AS-77-2746



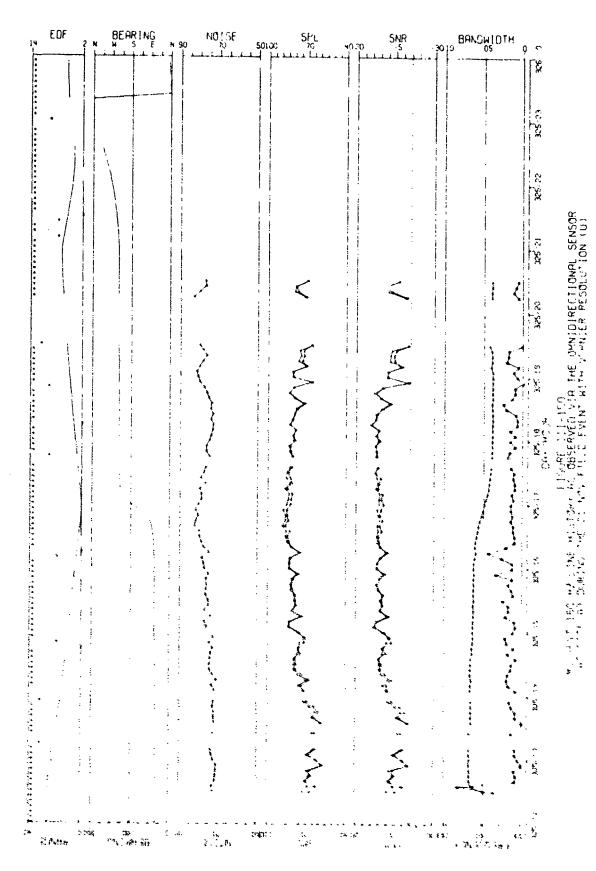
A5-77-2747



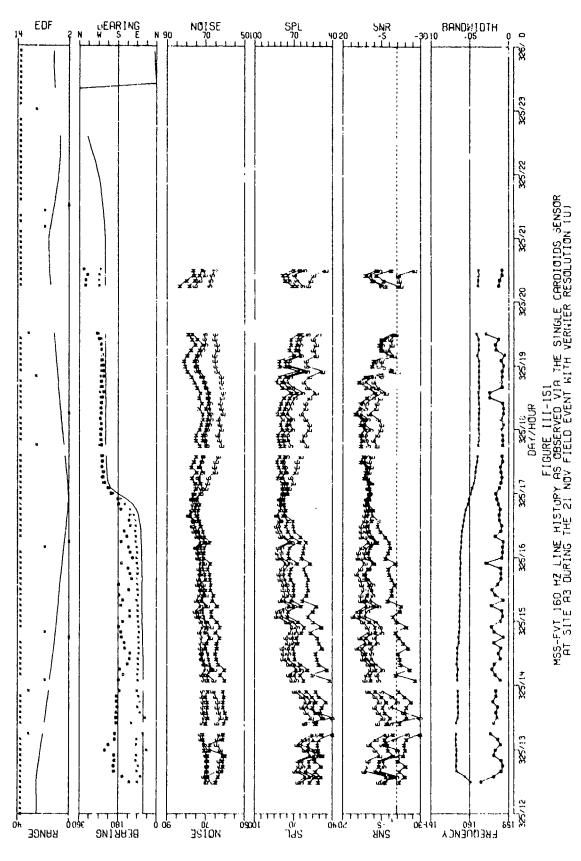
AS-77-2748



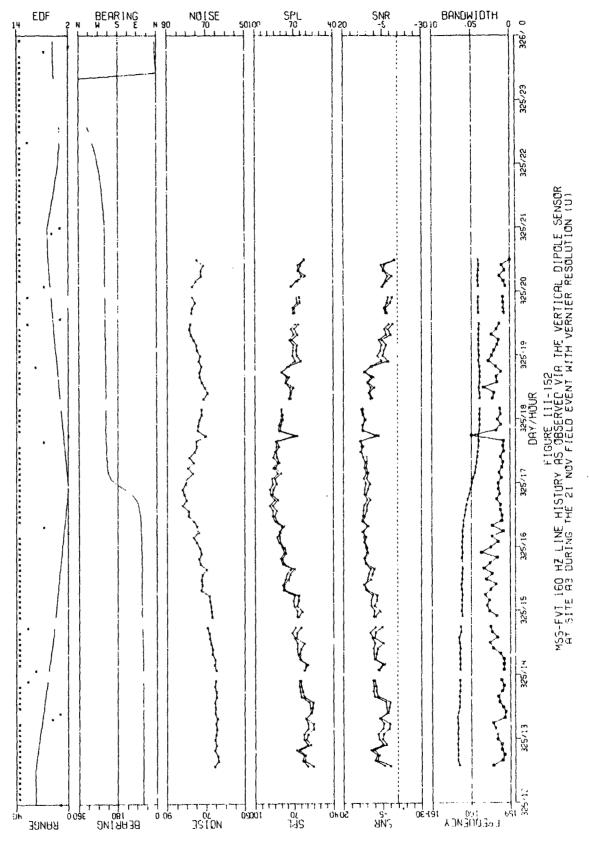
AS-77-2749



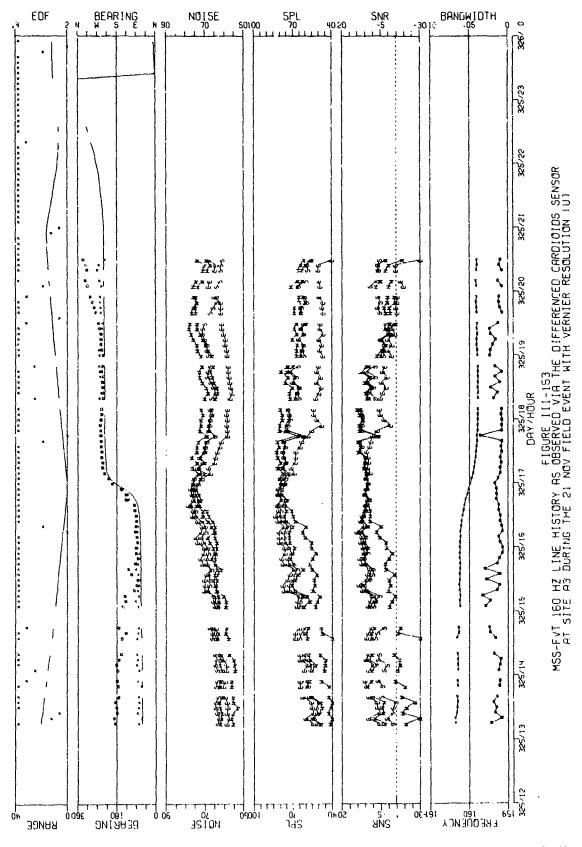
AS:77-2750



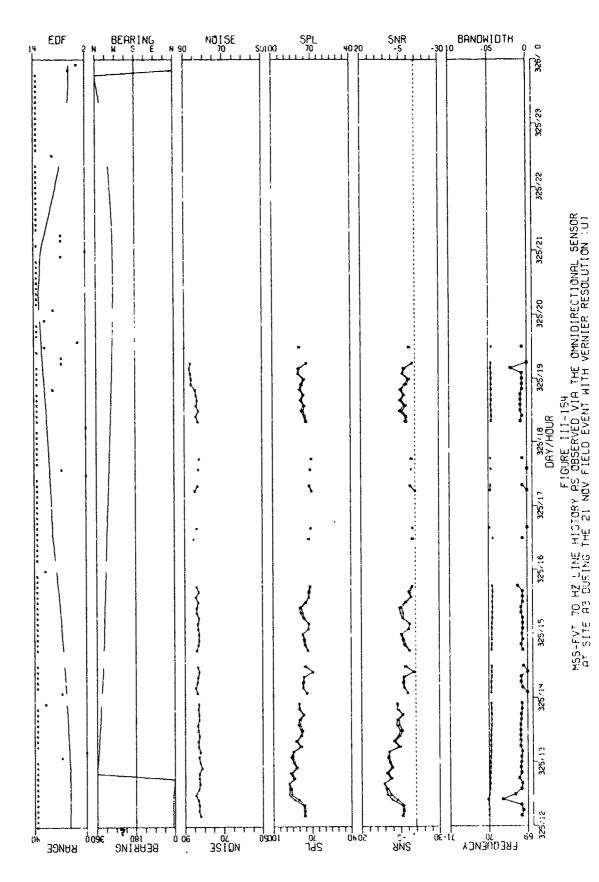
AS-77-2751

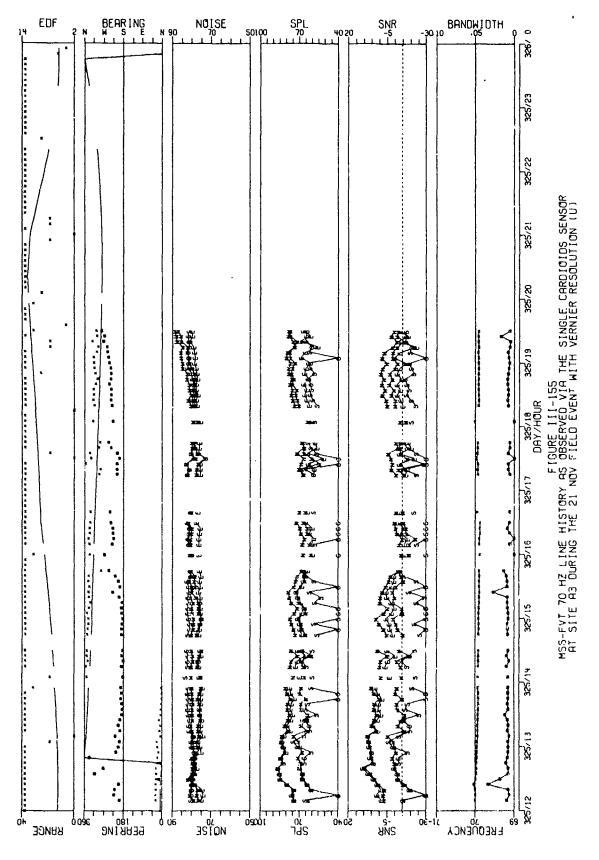


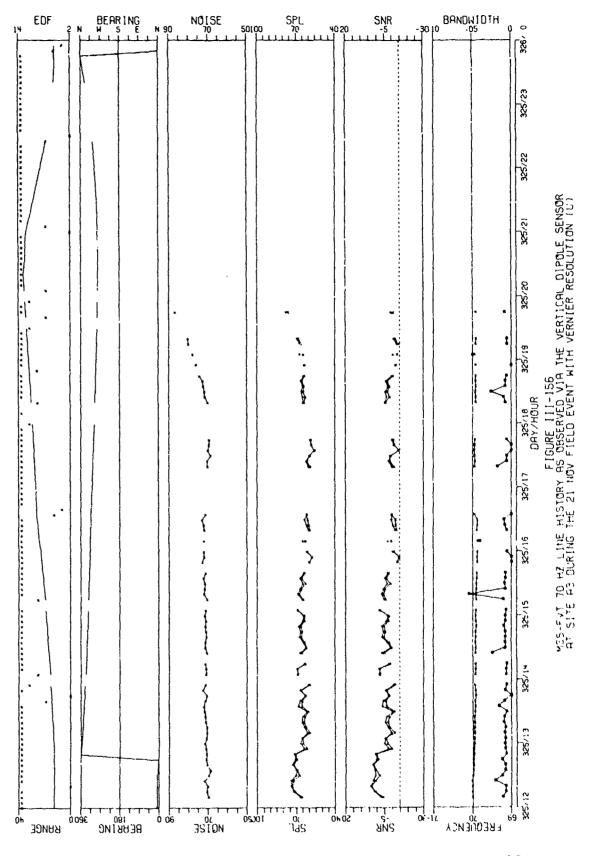
AS-77-2752



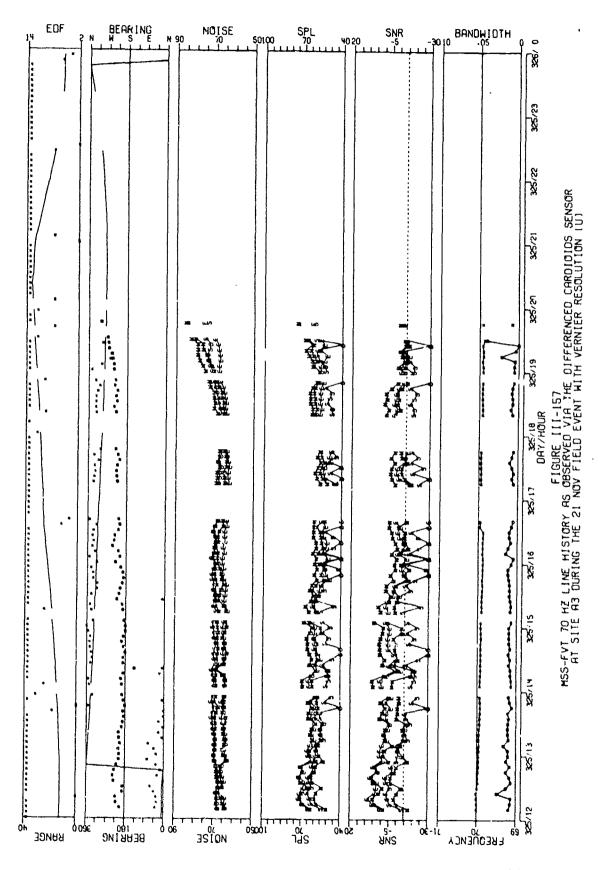
AS-77-2753



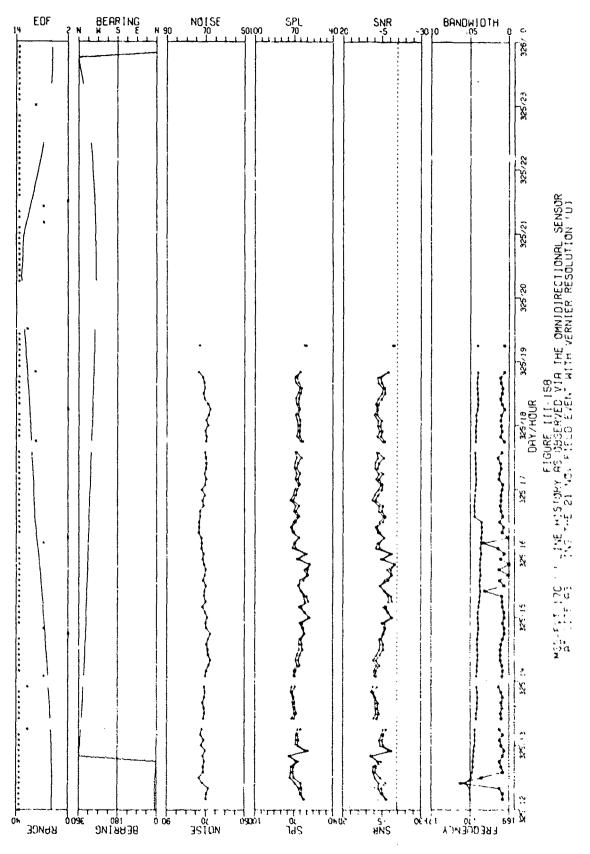


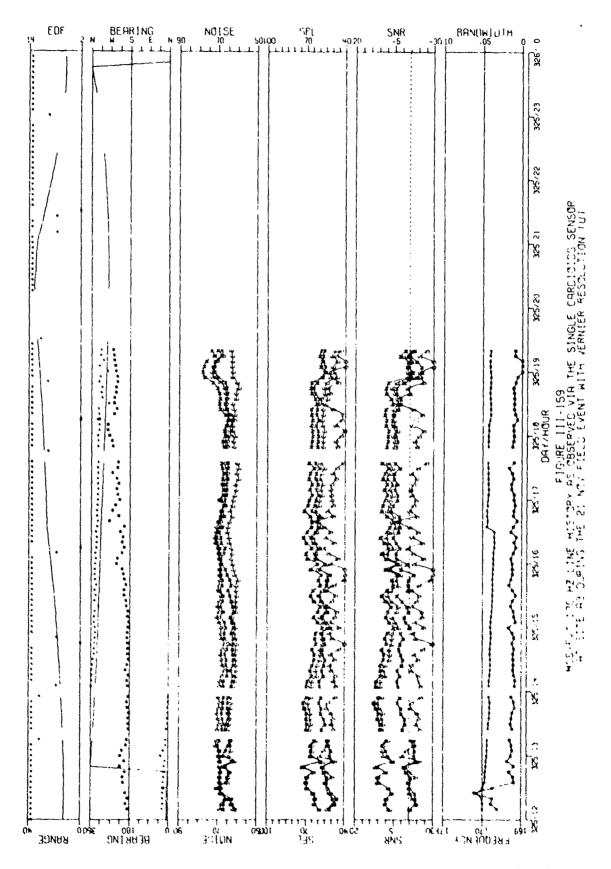


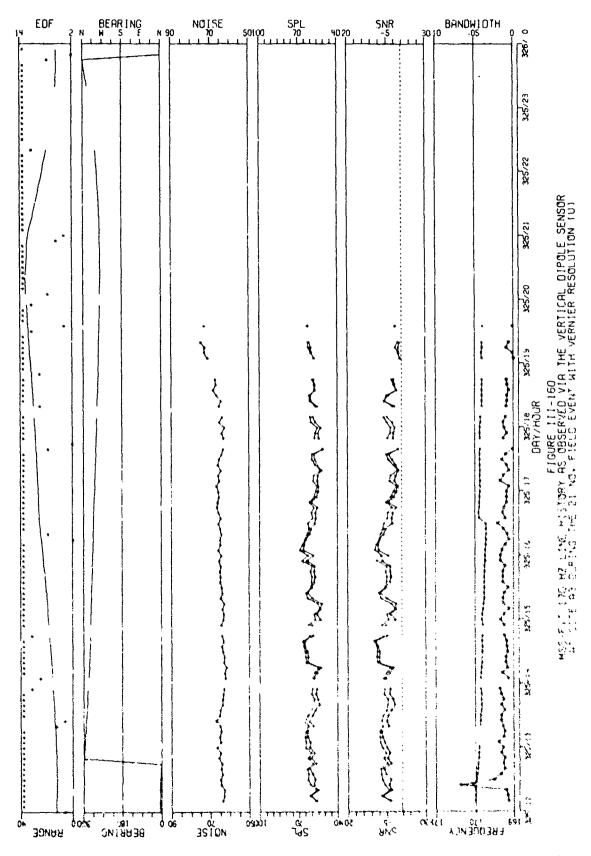
AS-77-2756

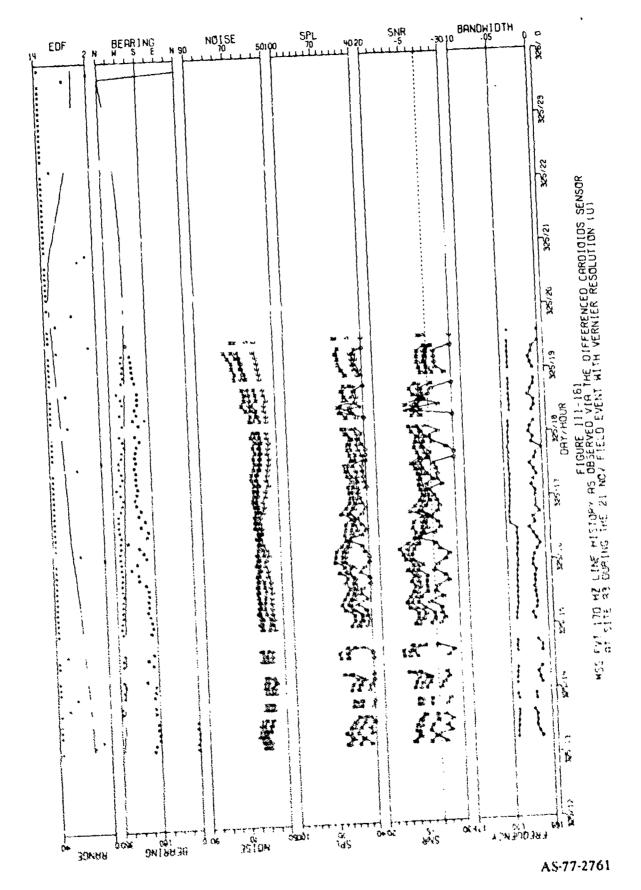


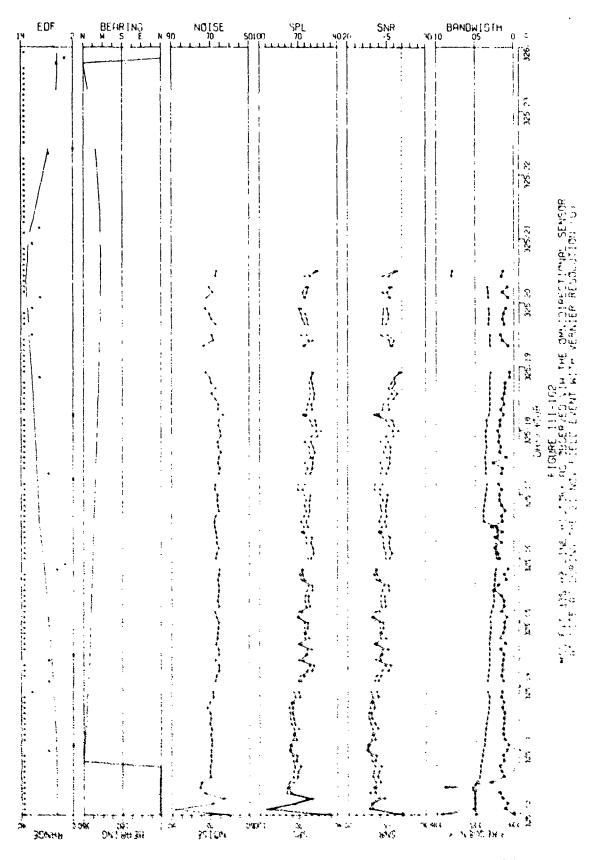
AS-77-2757

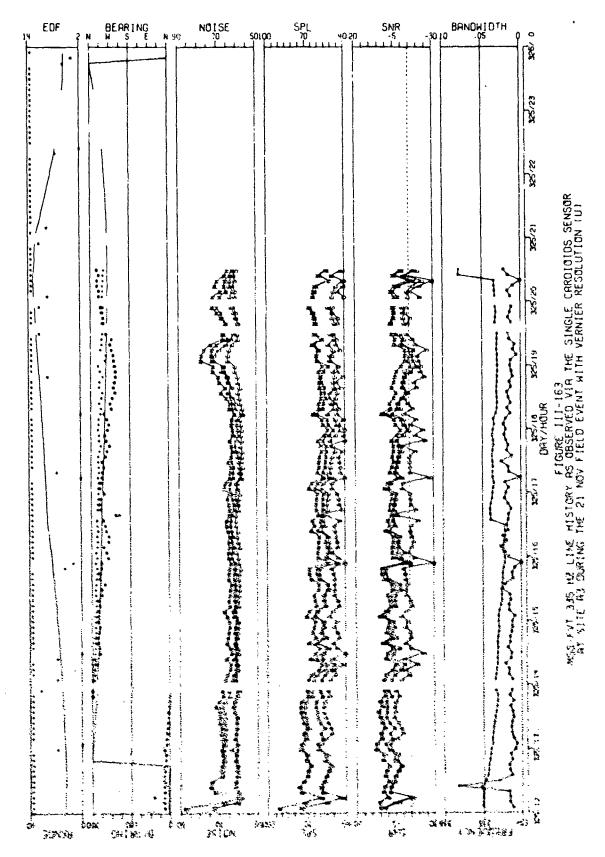












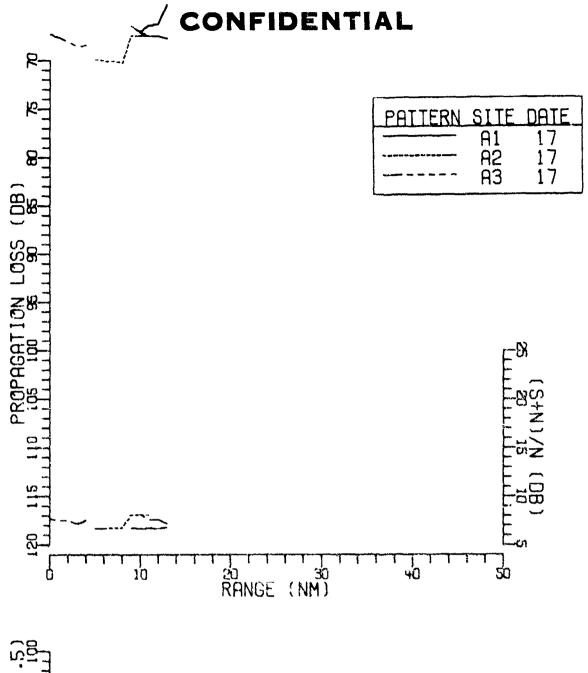
AS-77-2763

UNCLASSIFIED

APPENDIX C

PROPAGATION LOSS versus RANGE CURVES (U)

(FIGURES III-164 - III-171)



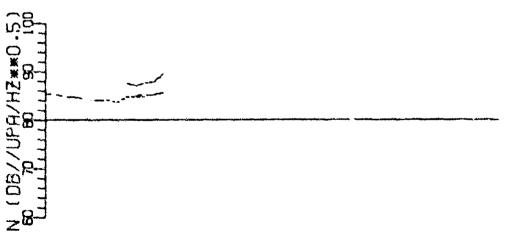
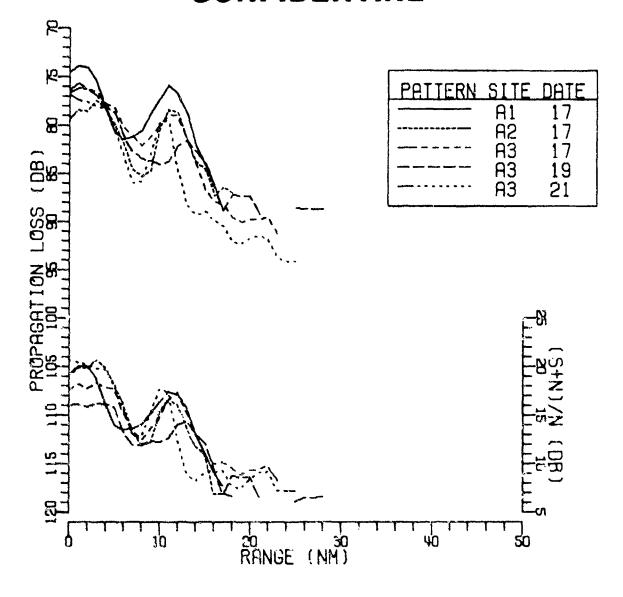


FIGURE III-164
MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR
PROPAGATION LOSS RESULTS FOR 55HZ AT 141DB (U)
195
CONFIDENTIAL



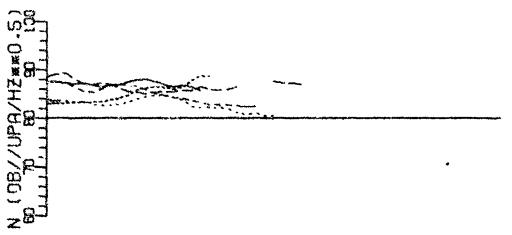
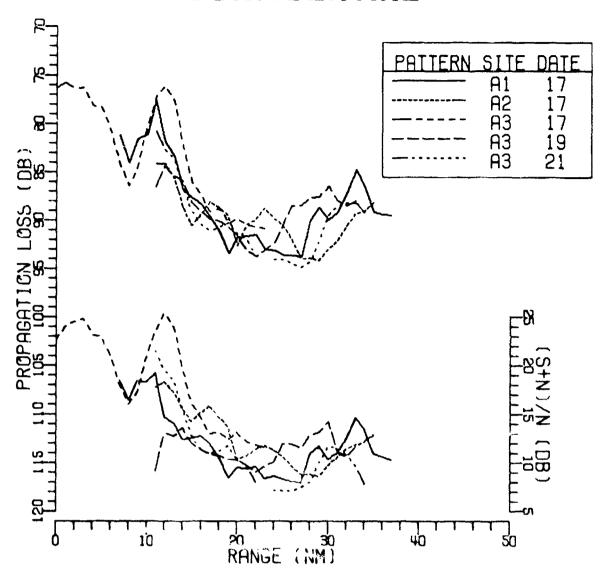


FIGURE III-165
MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR
PROPAGATION LOSS RESULTS FOR 64HZ AT 162DB (U)

96

CONFIDENTIAL



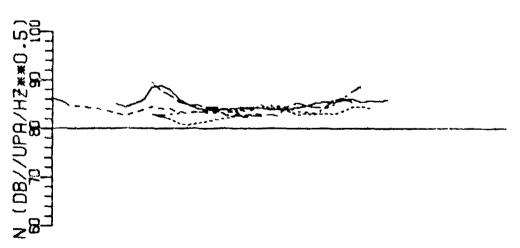


FIGURE III-166 MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR PROPAGA:ION LOSS RESULTS FOR 70HZ AT 166DB (U)

CONFIDENTIAL

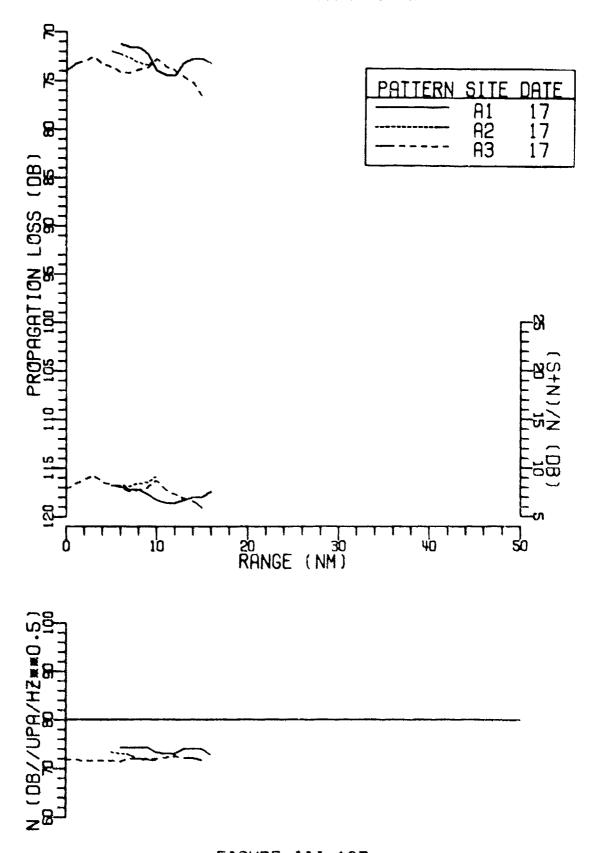
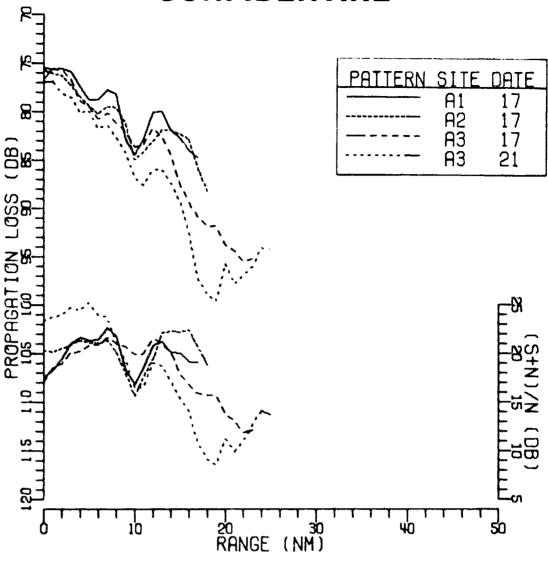


FIGURE III-167 MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR PROPAGATION LOSS RESULTS FOR 155HZ AT 134DB (U)

CONFIDENTIAL



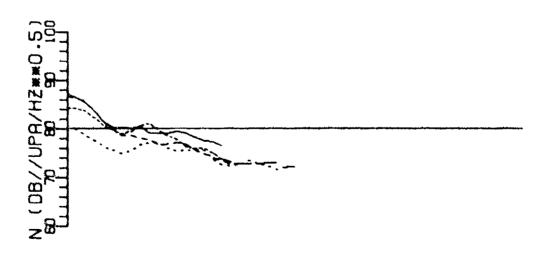
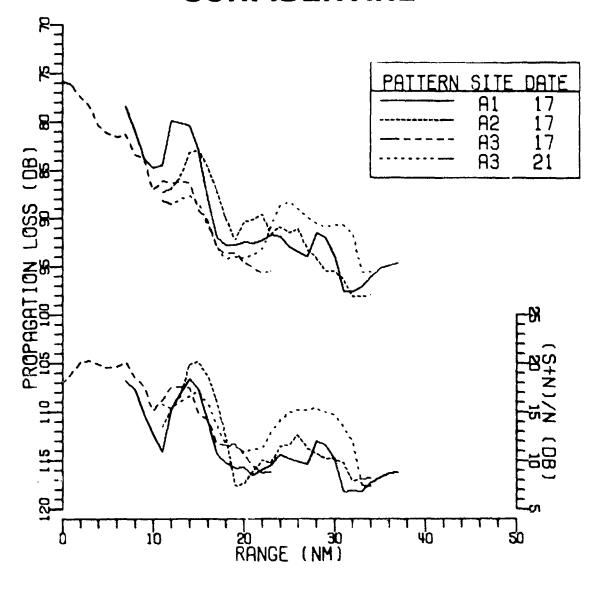


FIGURE III-168
MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR
PROPAGATION LOSS RESULTS FOR 160HZ AT 161DB (U)

AS-77-2768



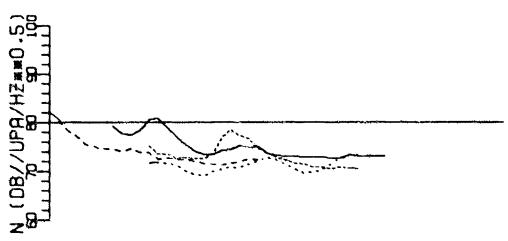


FIGURE III-169
MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR
PROPAGATION LOSS RESULTS FOR 170HZ AT 156DB (U)

CONFIDENTIAL

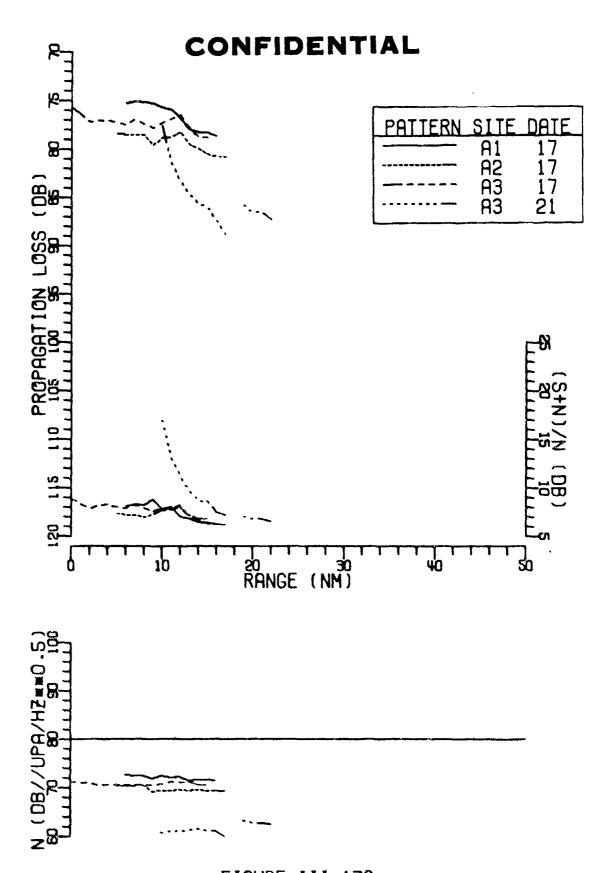
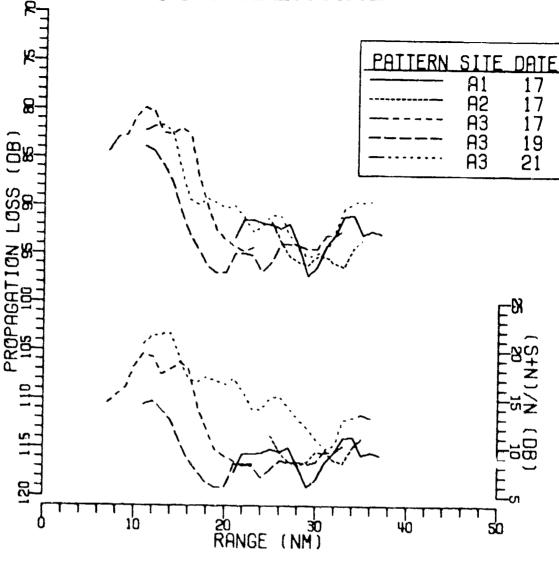


FIGURE III-170
MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR
PROPAGATION LOSS RESULTS FOR 305HZ AT 136DB (U)



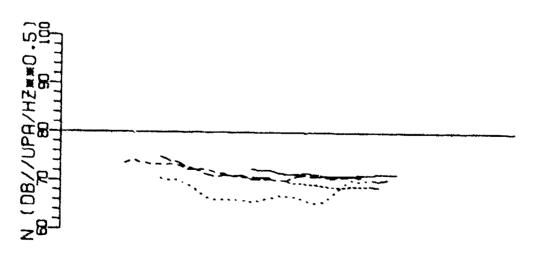


FIGURE III-171 MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR PROPAGATION LOSS RESULTS FOR 335HZ AT 154DB (U)

202

AS-77-2771

UNCLASSIFIED

APPENDIX D

ARRAY GAIN versus RANGE CURVES (U)

(FIGURES III-172 - III-199)

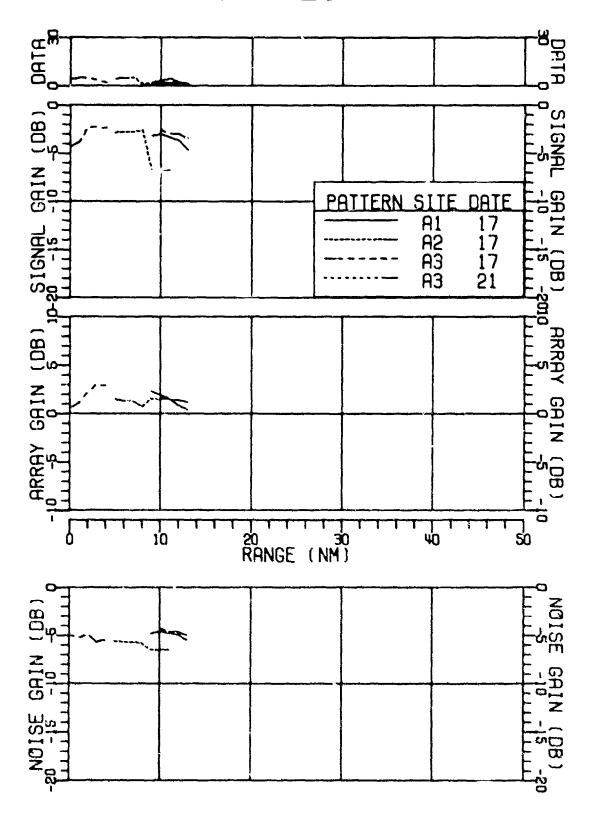


FIGURE III-172
MSS-FVT NEAR BOTTOM SINGLE CARDIDIDS SENSOR
ARRAY GAIN RESULTS FOR 55HZ AT 141DB (U)

AS-77-2772

The second secon

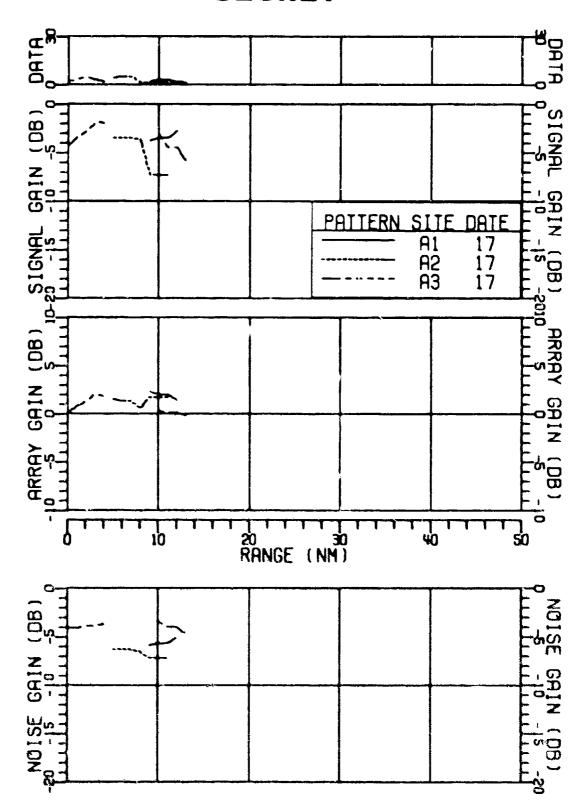


FIGURE III-173
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
ARRAY GAIN RESULTS FOR S5HZ AT 141DB (U)

AS-77-2773

SECRET

The second secon

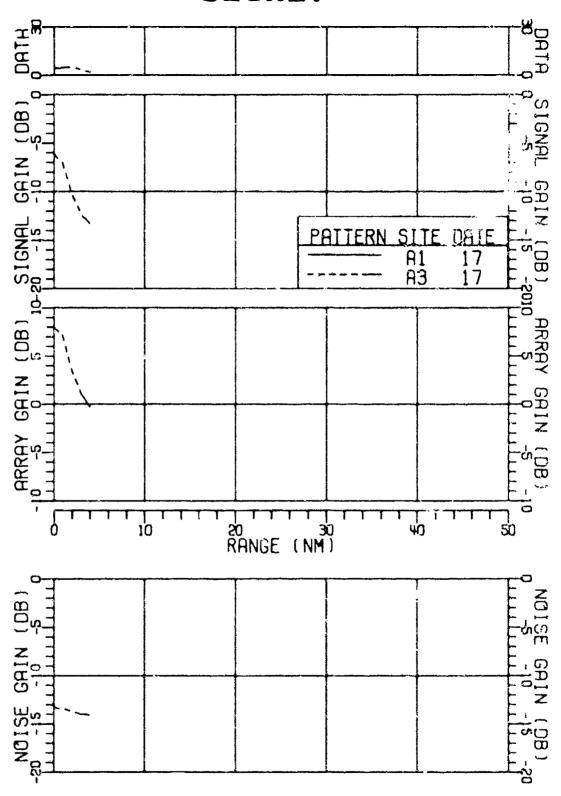


FIGURE III-174
MSS-FVT NEAR BOTTOM VERTICAL DIPOLE SENSOR
ARRAY GAIN RESULTS FOR 55HZ AT 141DB (U)

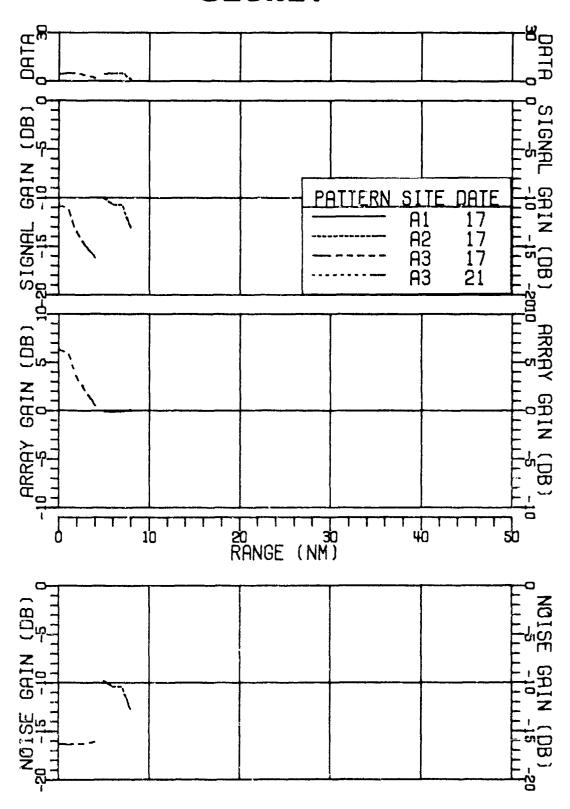


FIGURE III-175
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
ARRAY GAIN RESULTS FOR 55HZ AT 141DB (U)

AS-77-2775

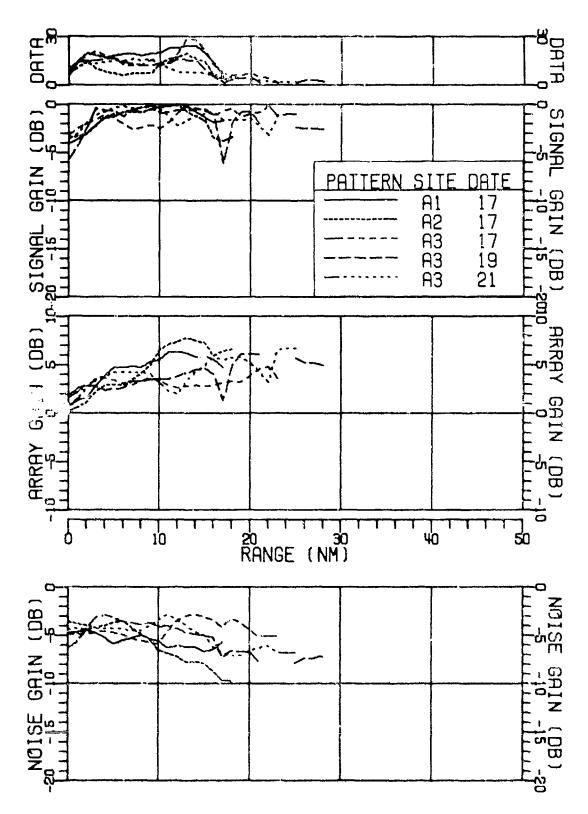


FIGURE III-176
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
ARRAY GAIN RESULTS FOR 64HZ AT 162DB (U)

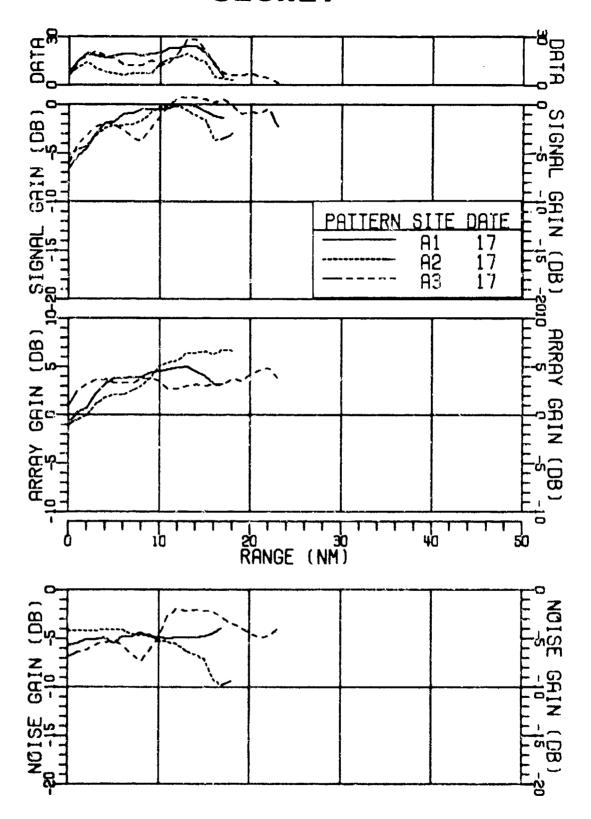


FIGURE III-177
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
ARRAY GAIN RESULTS FOR 64HZ AT 162DB (U)

AS-77-2777

SECRET

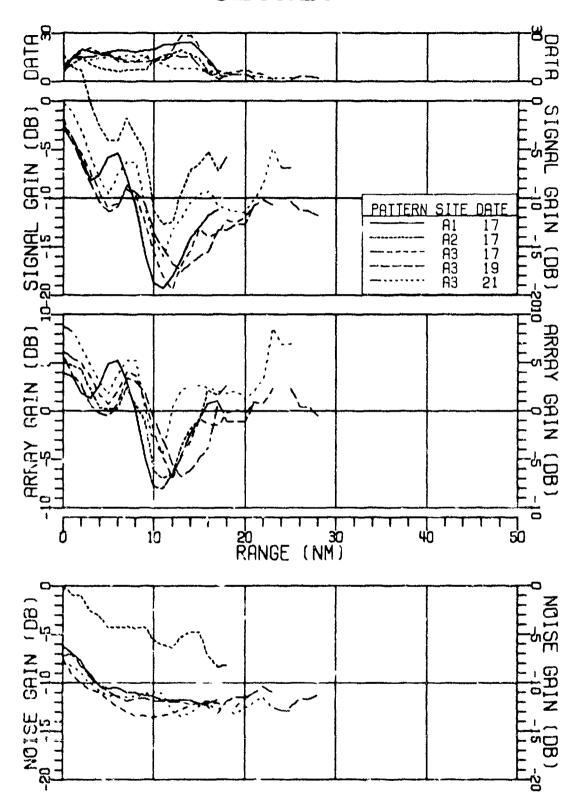


FIGURE 111-178
MSS-FVT NEAR BOTTOM VERTICAL DIPOLE SENSOR
ARRAY GAIN RESULTS FOR 64HZ AT 162DB (U)

AS-77-2778

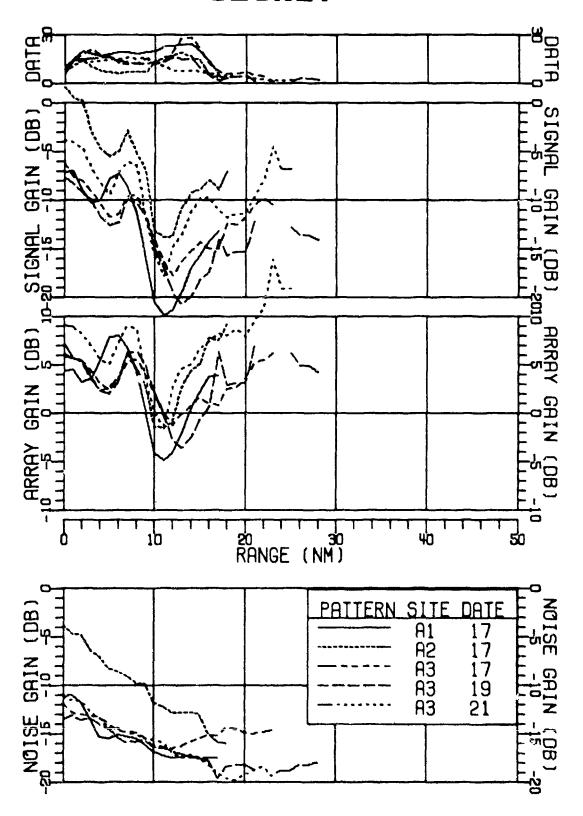


FIGURE III-179
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
ARRAY GAIN RESULTS FOR 64HZ AT 162DB (U)

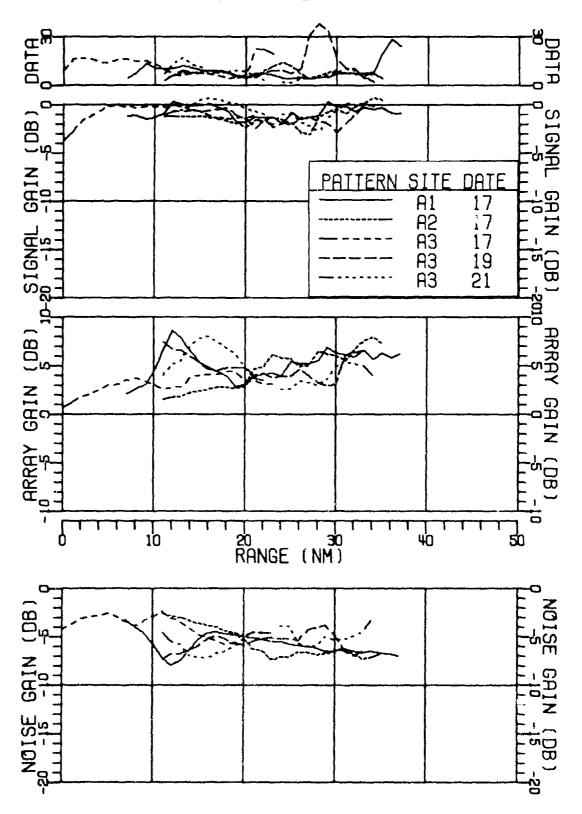


FIGURE III-180
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
ARRAY GAIN RESULTS FOR 70HZ AT 166DB (U)

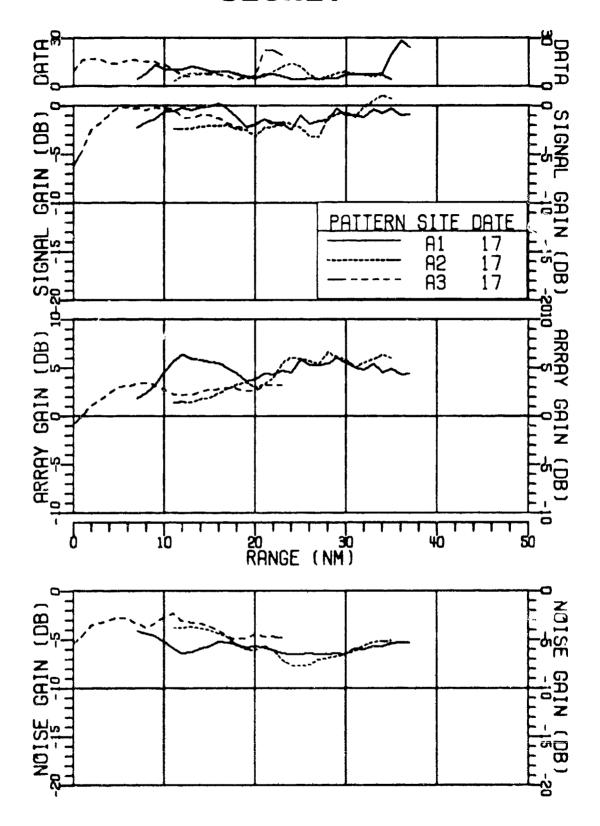


FIGURE III-181
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
ARRAY GAIN RESULTS FOR 70HZ AT 166DB (U)

AS-77-2781

214

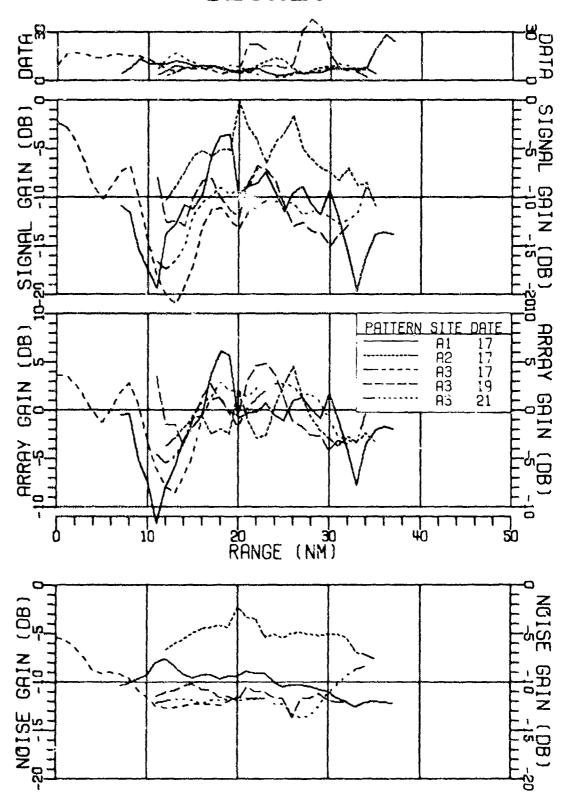


FIGURE III-182
MSS-FVT NEAR BOTTOM VERTICAL DIPOLE SENSOR
ARRAY GAIN RESULTS FOR 70HZ AT 166DB (U)

AS-77-2782

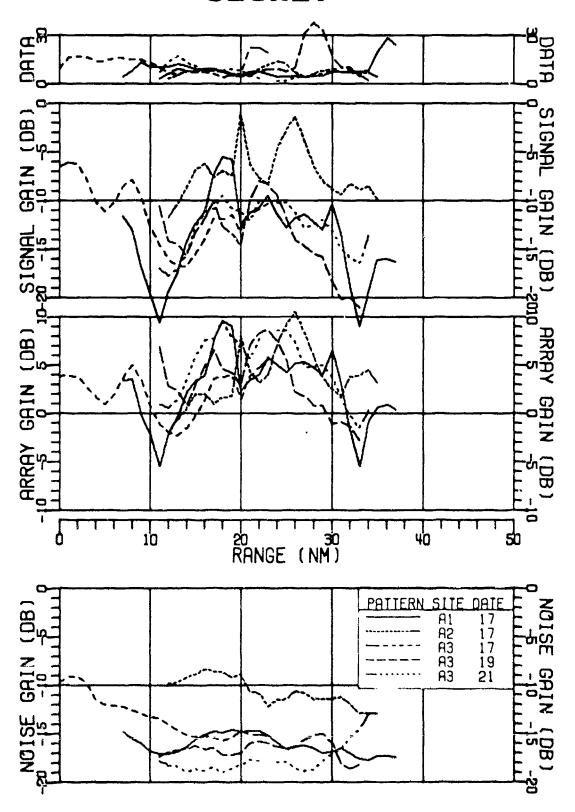


FIGURE III-183
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
ARRAY GAIN RESULTS FOR 70HZ AT 166DB (U)

AS-77-2783

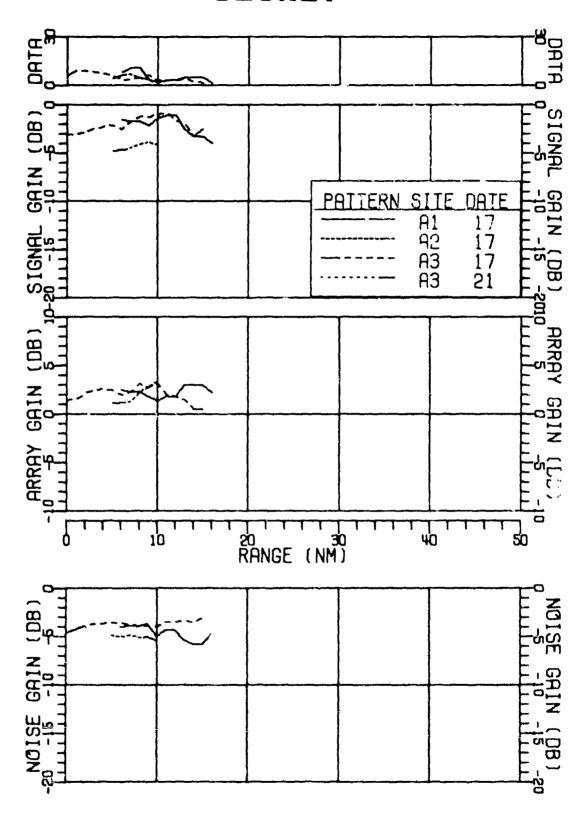


FIGURE III-184
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
ARRAY GAIN RESULTS FOR 155HZ AT 134DB (U)

AS 77-2784

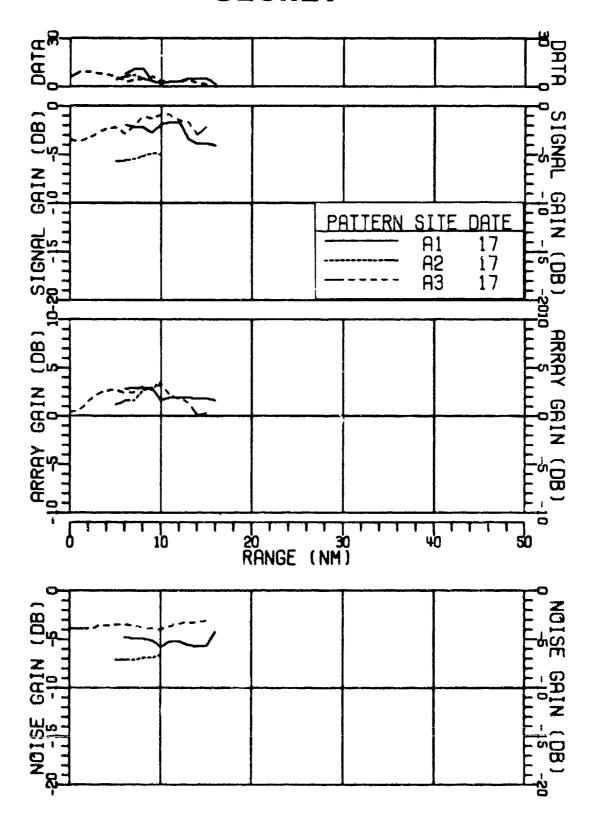


FIGURE III-185
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
ARRAY GAIN RESULTS FOR 155HZ AT 134DB (U)

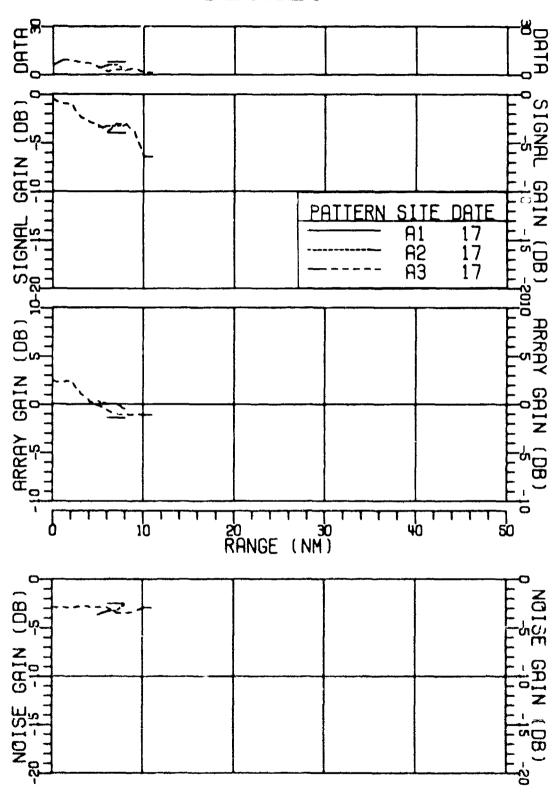


FIGURE III-186
MSS-FVT NEAR BOTTOM VERTICAL DIPOLE SENSOR
ARRAY GAIN RESULTS FOR 155HZ AT 134DB (U)

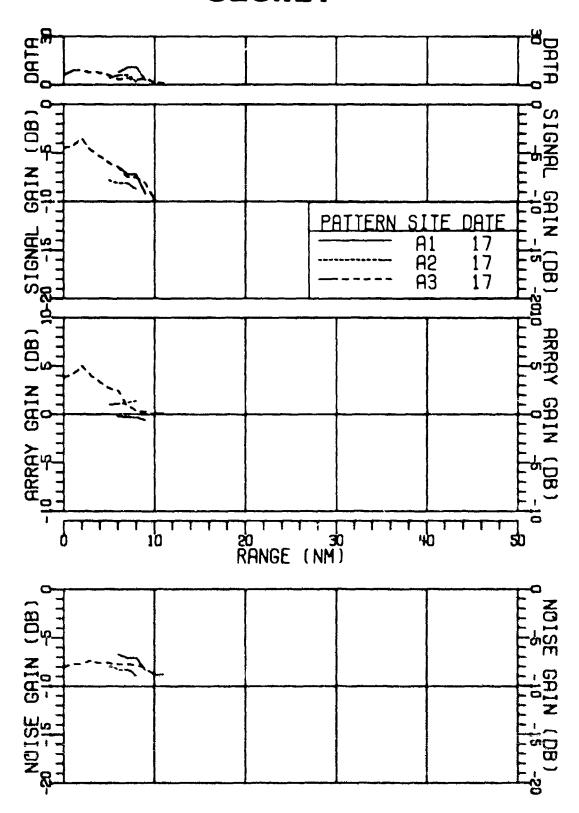


FIGURE III-187
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOF
ARRAY GAIN RESULTS FOR 155HZ AT 134DB (U)

AS-77-2787

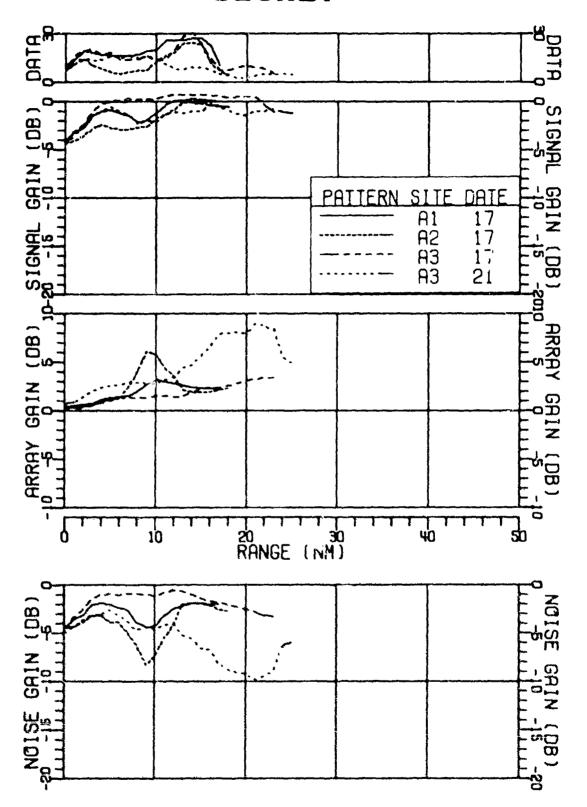


FIGURE III-188
MSS-FVT NERR BOTTOM SINGLE CARDIDIDS SENSOR
ARRAY GAIN RESULTS FOR 160HZ AT 161DB (U)

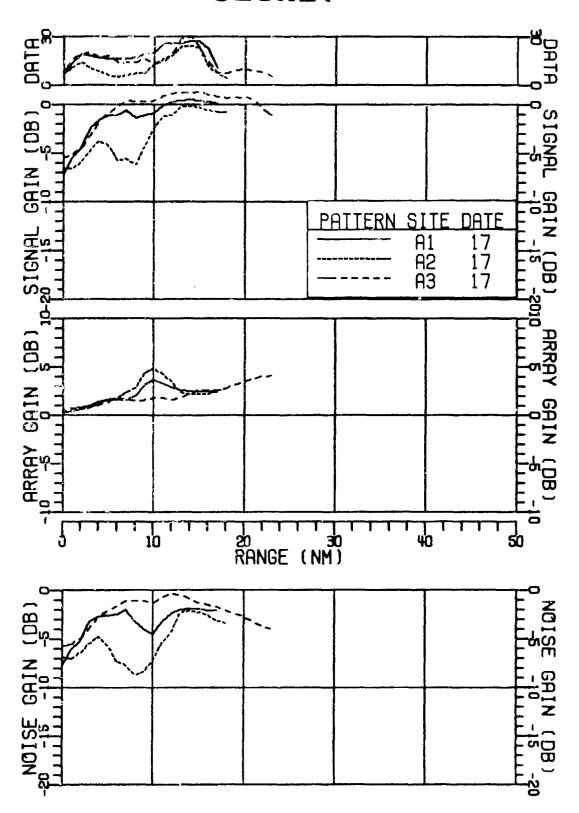


FIGURE III-189 MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR ARRAY GAIN RESULTS FOR 160HZ AT 161DB (U)

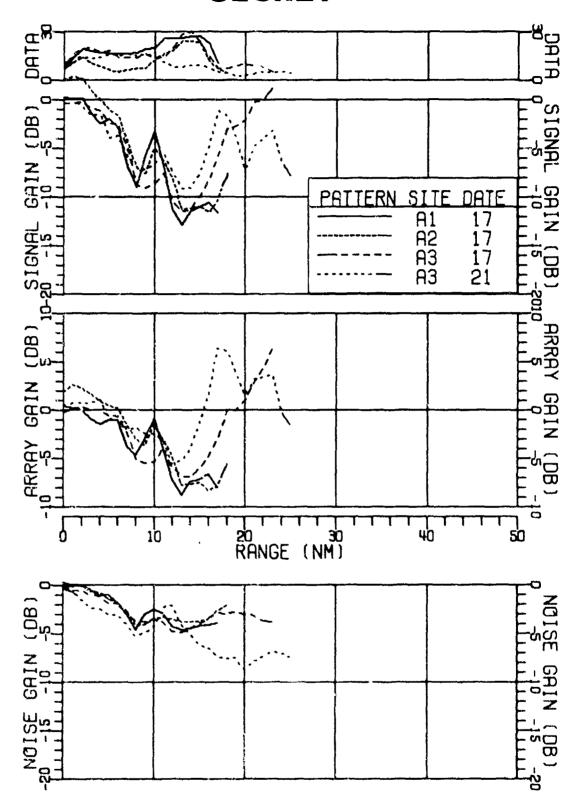


FIGURE III-190
MSS-FVT NEAR BOTTOM VERTICAL DIPOLE SENSOR
ARRAY GAIN RESULTS FOR 160HZ AT 161DB (U)

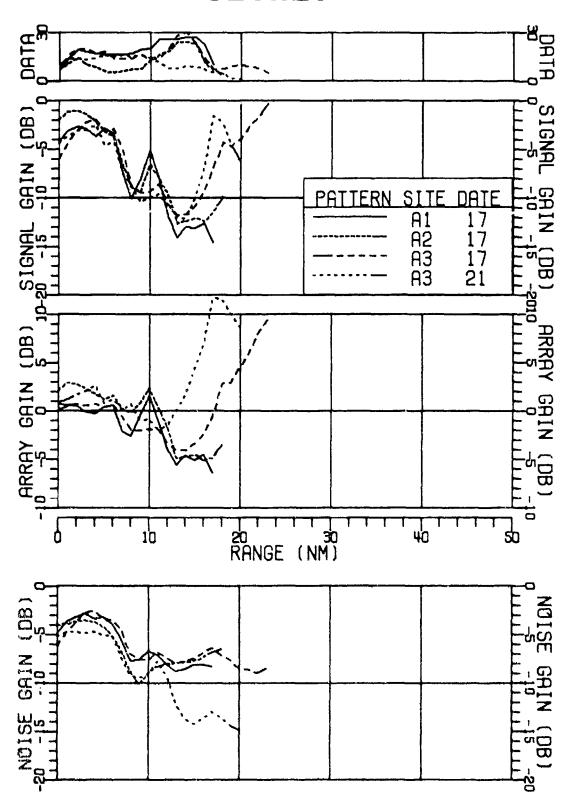


FIGURE III-191
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
ARRAY GAIN RESULTS FOR 160HZ AT 161DB (U)

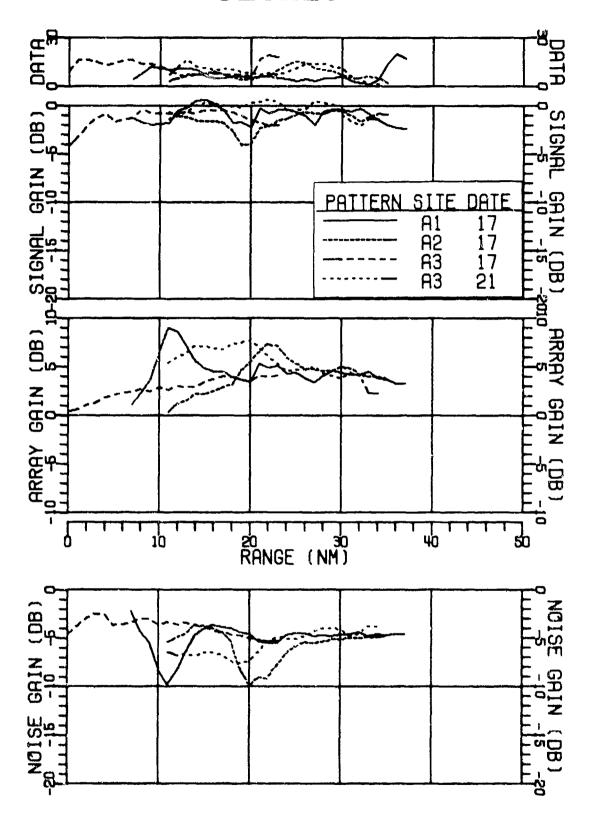


FIGURE III-192 MSS-FVT NEAR BOTTOM SINGLE CARDICIDS SENSOR ARRAY GAIN RESULTS FOR 170HZ AT 156DB (U)

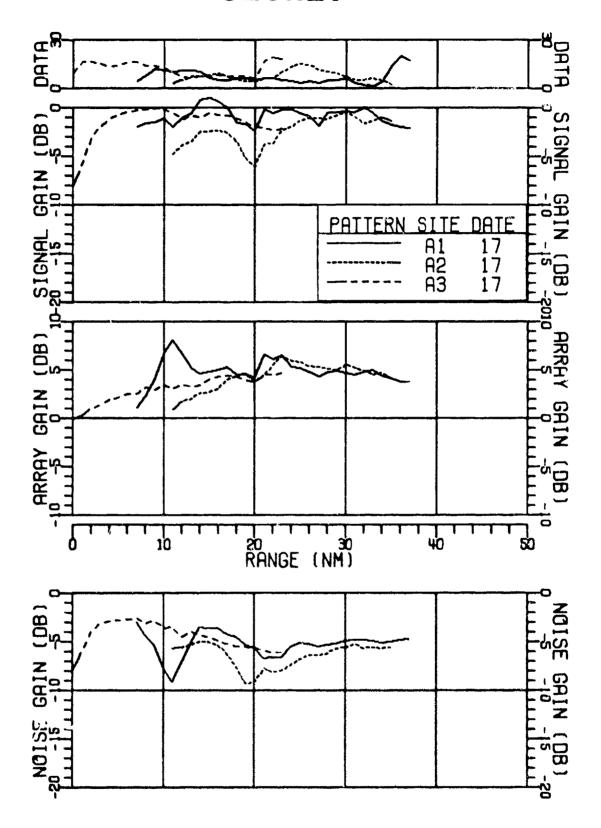


FIGURE III-193
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
ARRAY GAIN RESULTS FOR 170HZ AT 156DB (U)

AS-77-2793

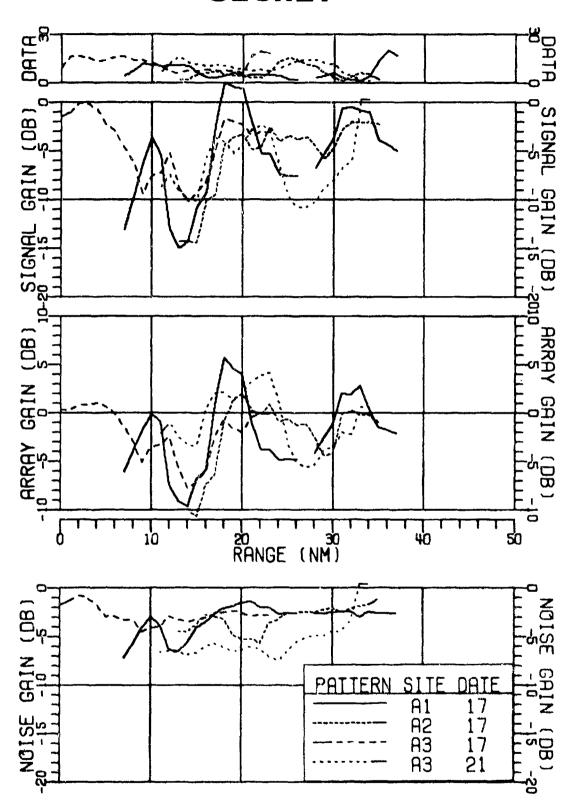


FIGURE III-194
MSS-FVT NEAR BOTTOM VERTICAL DIPOLE SENSOR
ARRAY GAIN RESULTS FOR 170HZ AT 156DB (U)

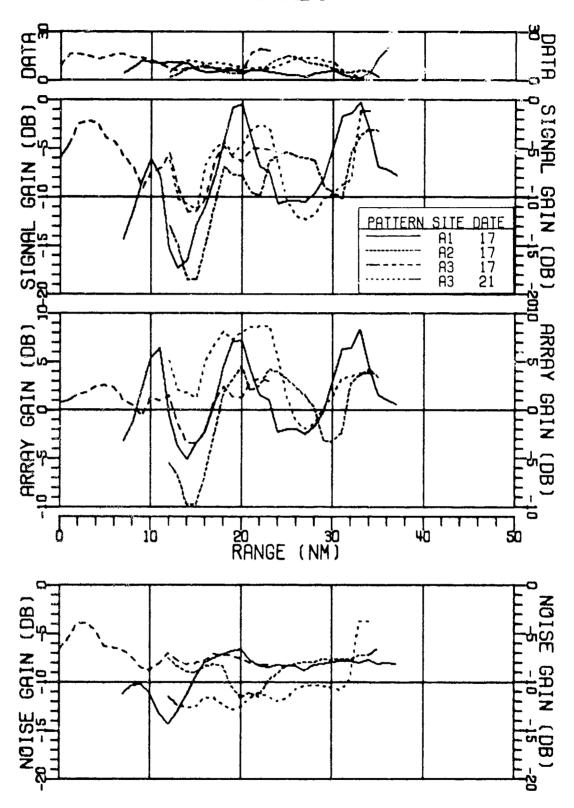


FIGURE III-195
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIDIDS SENSOR
ARRAY GAIN RESULTS FOR 170HZ AT 156DB (U)

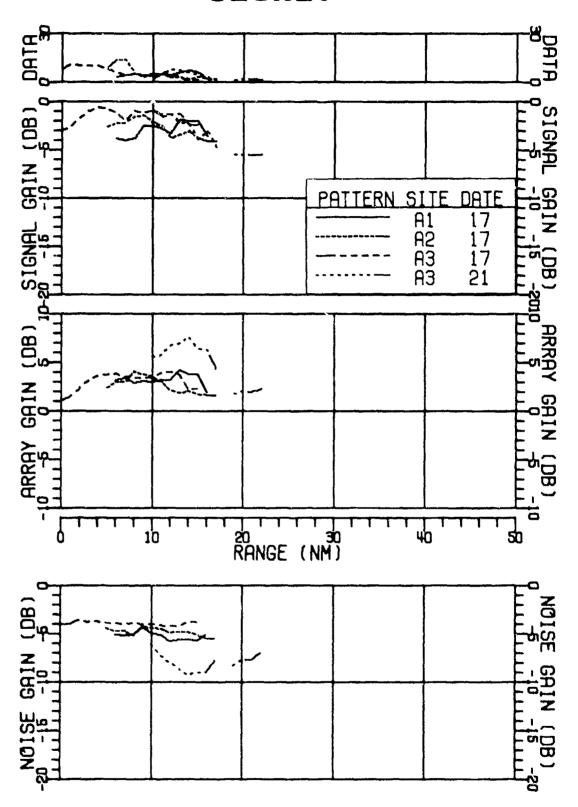


FIGURE III-196
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
ARRAY GAIN RESULTS FOR 305HZ AT 136DB (U)

AS-77-2796

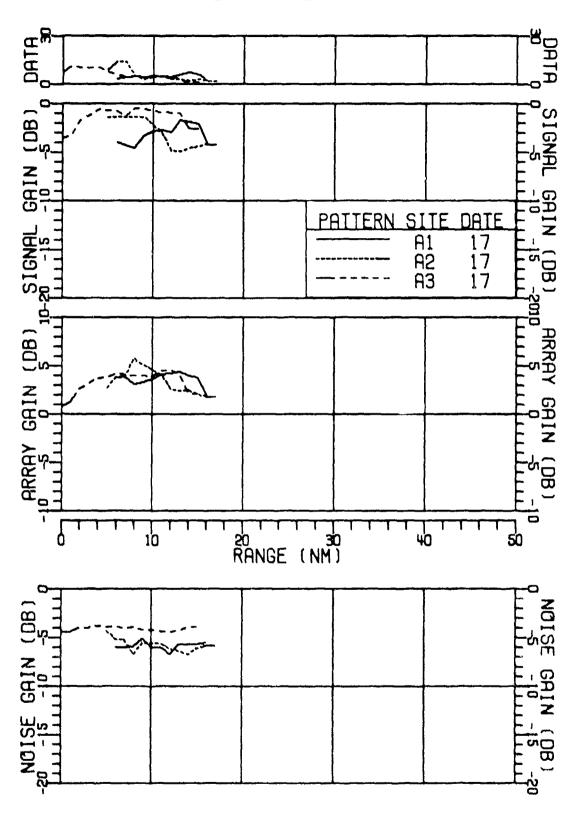


FIGURE III-197
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
ARRAY GAIN RESULTS FOR 305HZ AT 136DB (U)
AS-77-2797

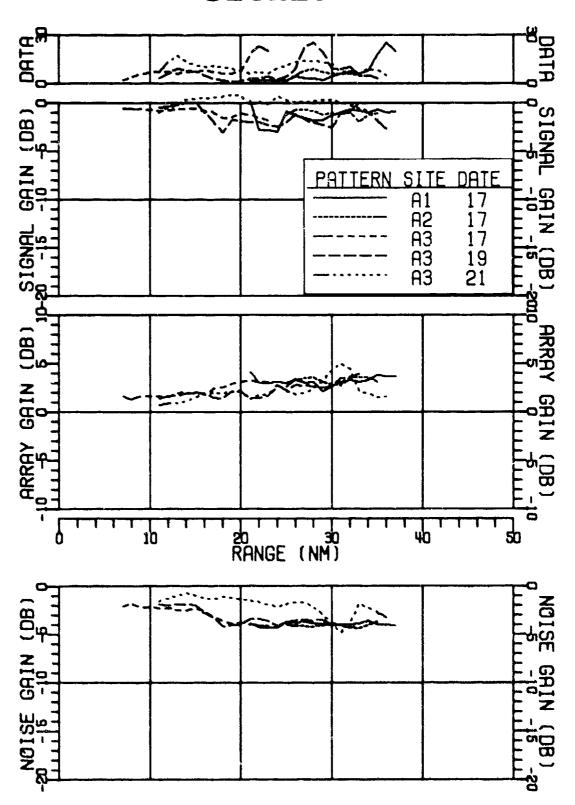


FIGURE III-198
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
ARRAY GAIN RESULTS FOR 335HZ AT 154DB (U)

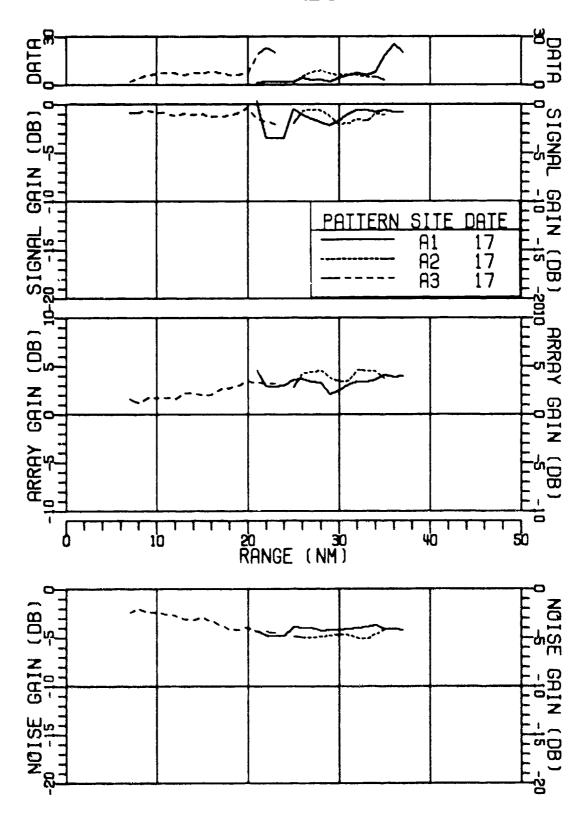


FIGURE III-199
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
ARRAY GAIN RESULTS FOR 335HZ AT 154DB (U)
AS-77-2799

UNCLASSIFIED

APPENDIX E

PERCENTAGE DETECTION versus RANGE CURVES (U)

(FIGURES III-200 - III-235)

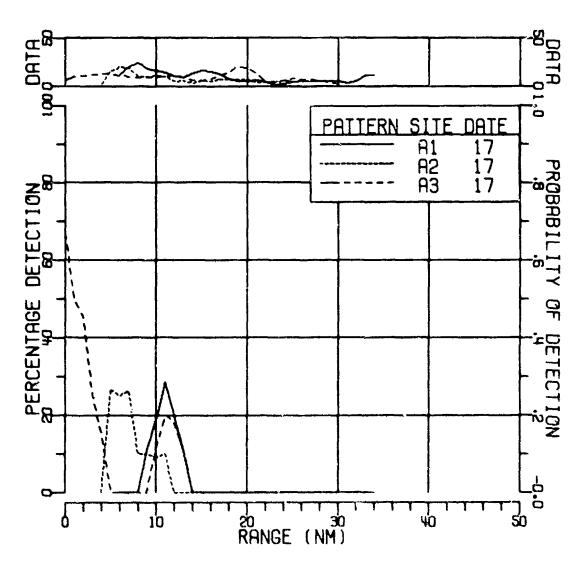


FIGURE III-200
MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR
DETECTION RESULTS FOR 55HZ AT 141DB (U)

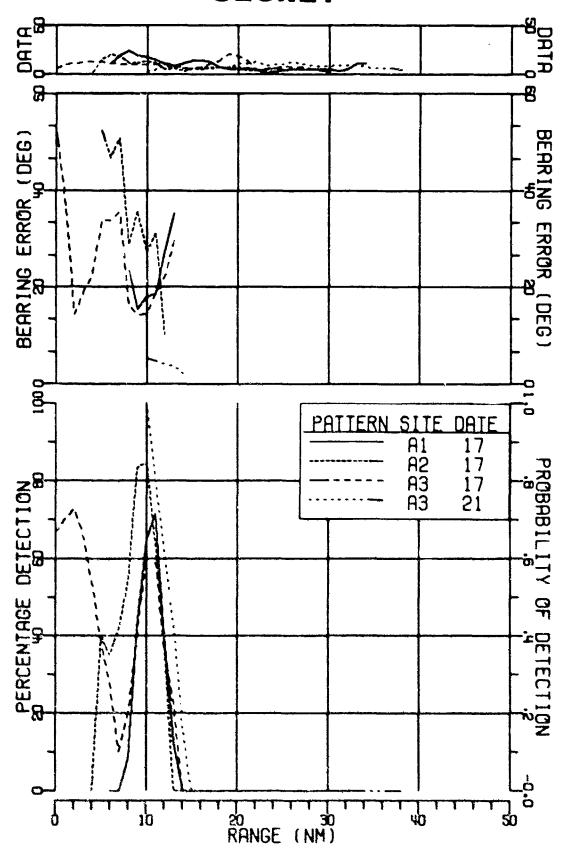


FIGURE 111-201 MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR DETECTION RESULTS FOR 55HZ AT 141DB (U)

SECRET

AS-77-2891

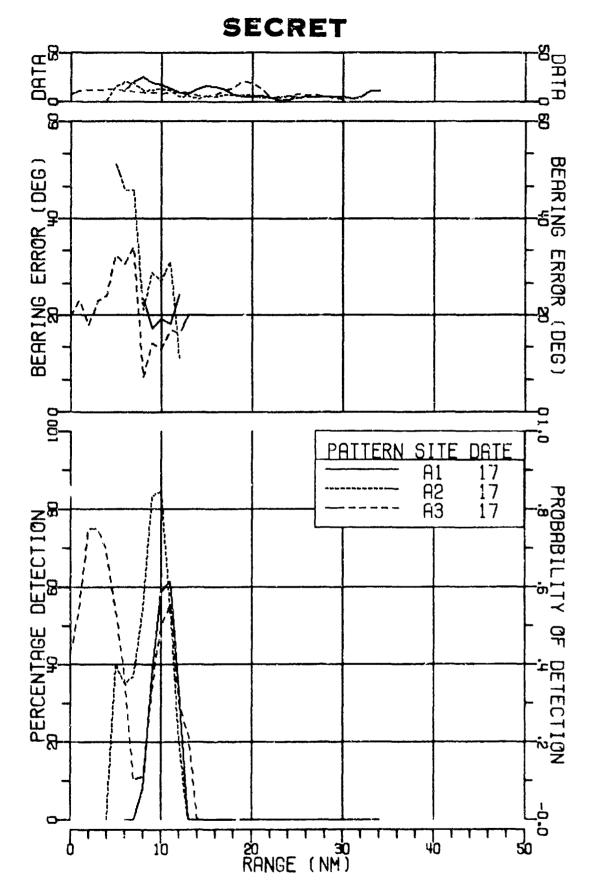


FIGURE III-202
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
DETECTION RESULTS FOR 55HZ AT 141DB (U)

AS-77-2802

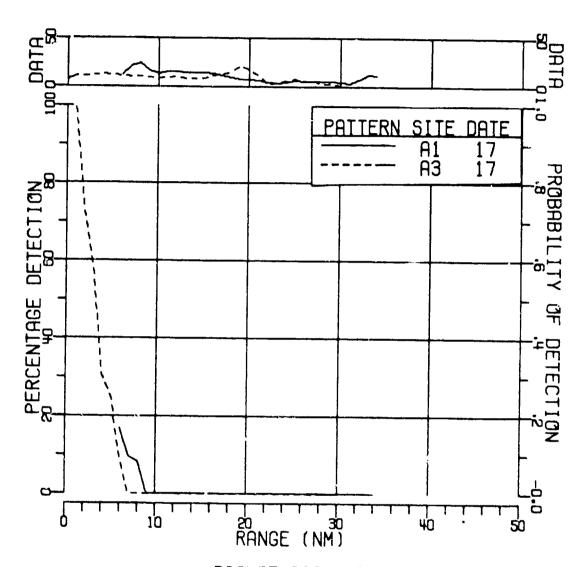


FIGURE III-203 MSS-FVT NEAR BOTTOM VERTICAL DIPOLE SENSOR DETECTION RESULTS FOR 55HZ AT 141DB (U)

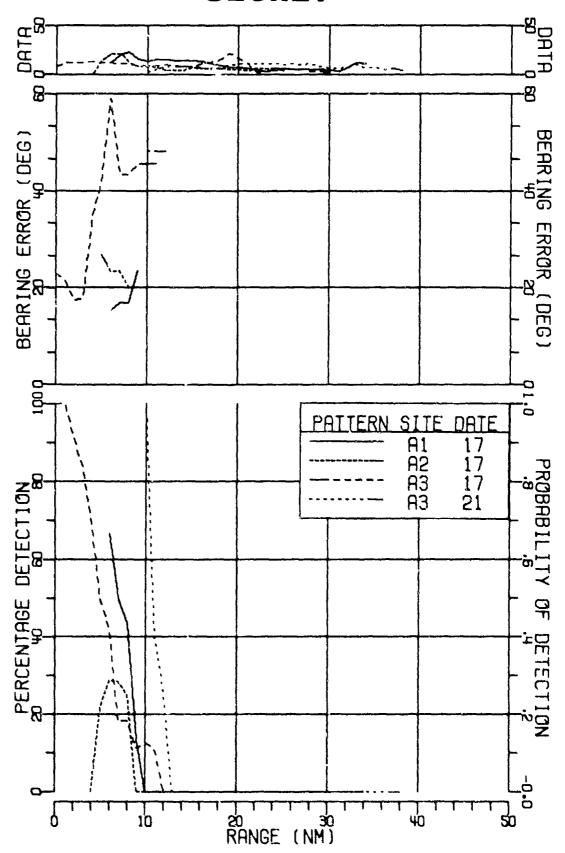


FIGURE III-204
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
DETECTION RESULTS FOR 55HZ AT 141DB (U)
SECRET

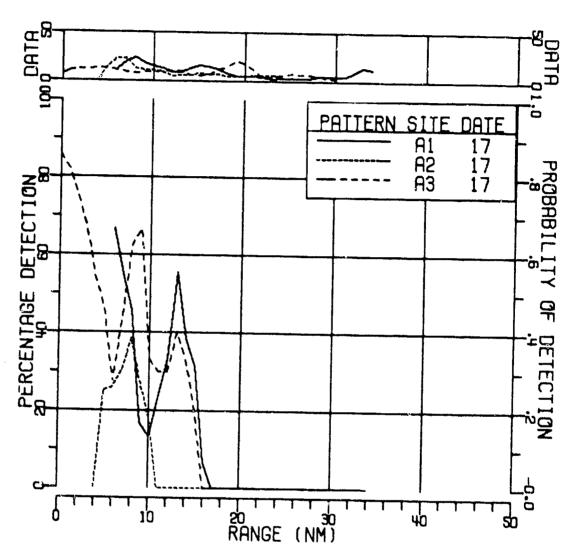


FIGURE III-205
MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR
DETECTION RESULTS FOR 155HZ AT 134DB (U)

AS-77-2805

SECRET

South Black Black States

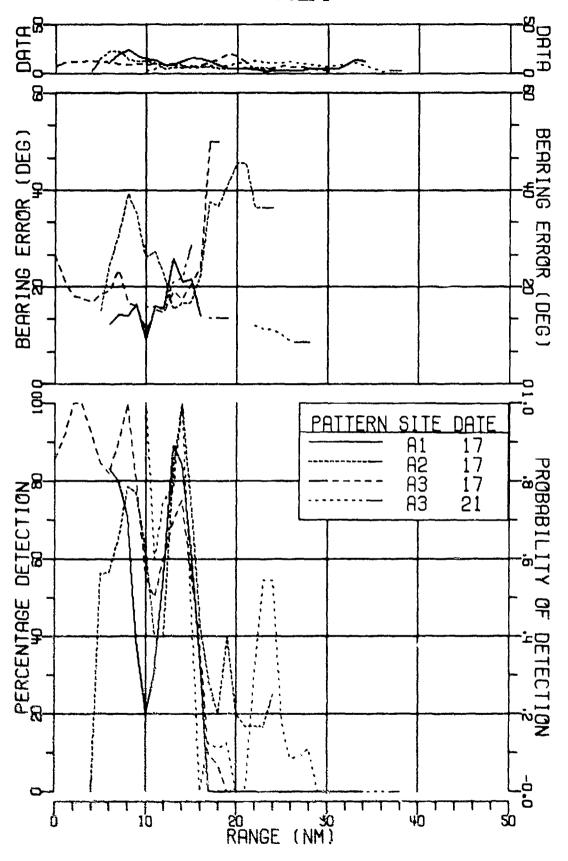


FIGURE III-206
MSS-FVT NEAR BOTTOM SINGLE CARDIDIDS SENSOR
DETECTION RESULTS FOR 155HZ AT 134DB (U)
SECRET

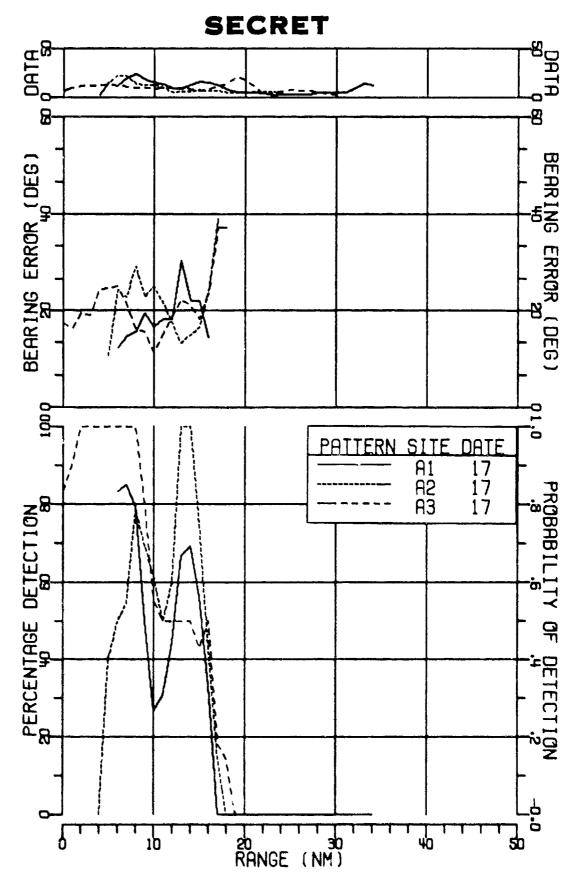


FIGURE III-207
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
DETECTION RESULTS FOR 155HZ AT 134DB (U)

AS-77-2807

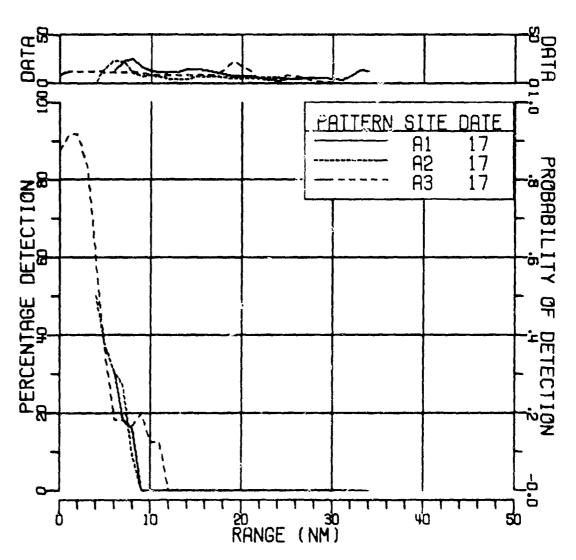


FIGURE III-208
MSS-FVT NEAR BOTTOM VERTICAL DIPOLE SENSOR
DETECTION RESULTS FOR 155HZ AT 134DB (U)

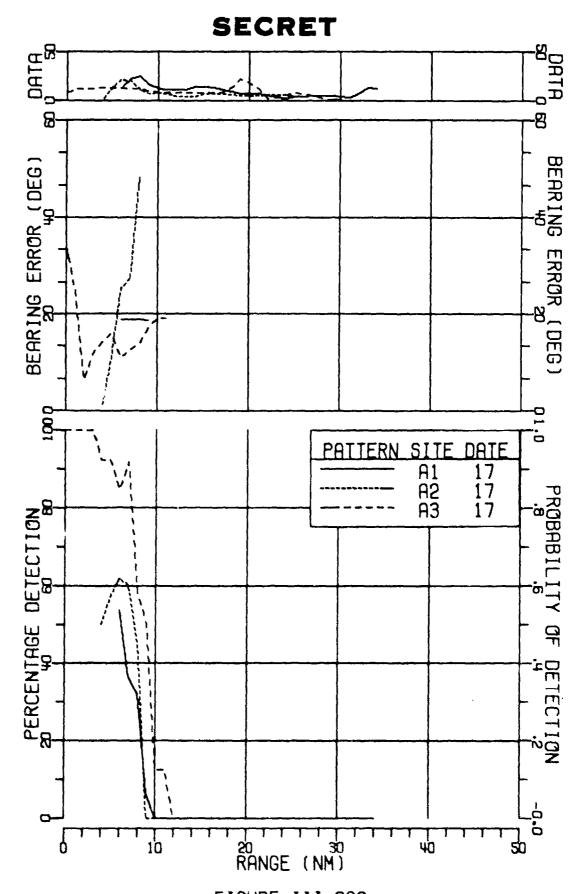


FIGURE III-209 MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSON DETECTION RESULTS FOR 155HZ AT 134DB (U) 244

AS-77-2809

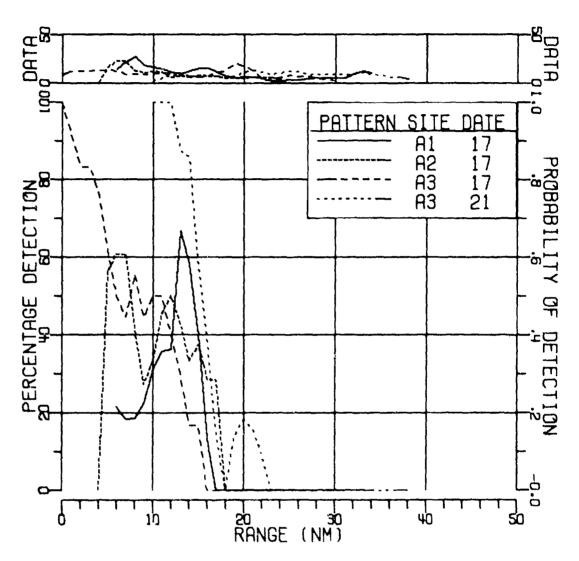


FIGURE III-210
MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR
DETECTION RESULTS FOR 305HZ AT 136DB (U)

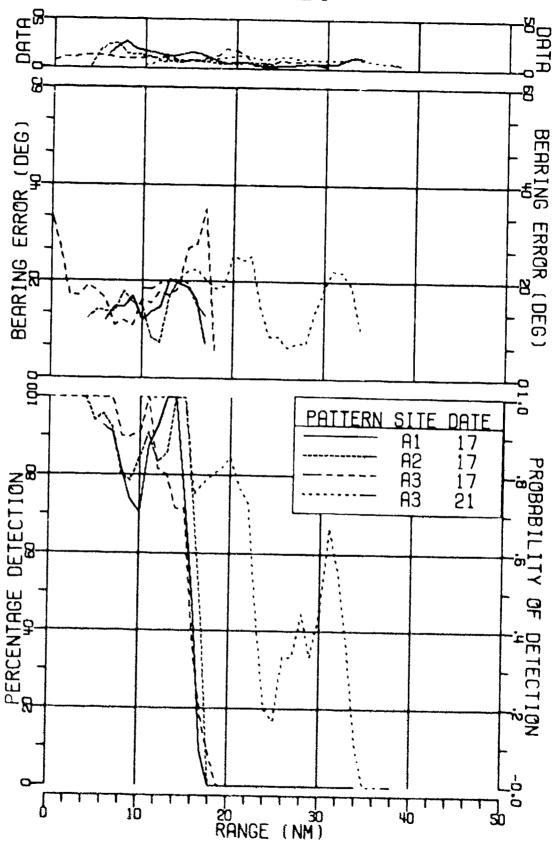


FIGURE III-211
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
DETECTION RESULTS FOR 305HZ AT 136DB (U)

SECRET

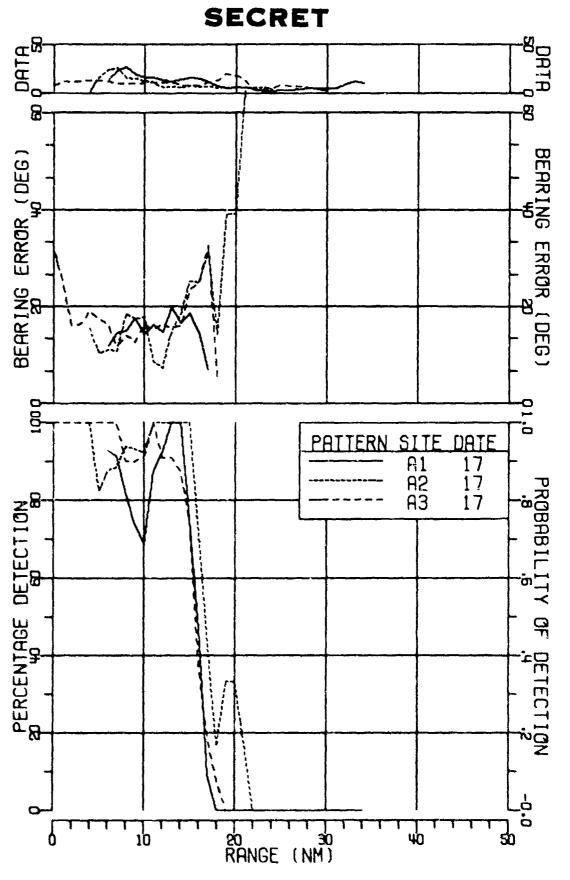


FIGURE III-212 MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR DETECTION RESULTS FOR 305HZ AT 136DB (U)

AS-77-281

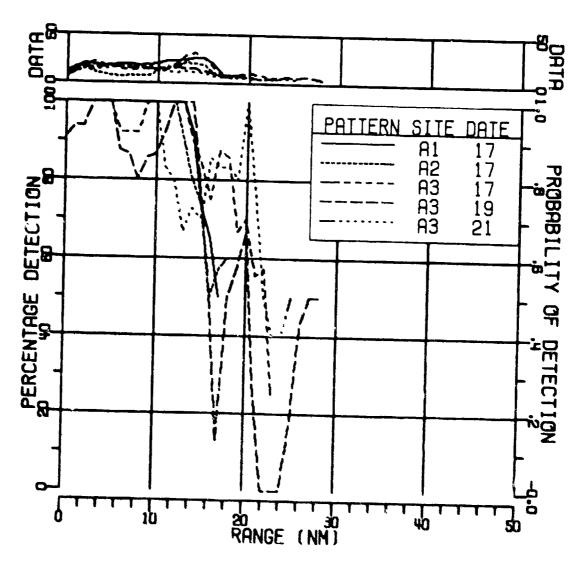


FIGURE III-213
MSS-FVT NERR BOTTOM OMNIDIRECTIONAL SENSOR
DETECTION RESULTS FOR 64HZ AT 162DB (U)

AS-77-2813

SECRET

117

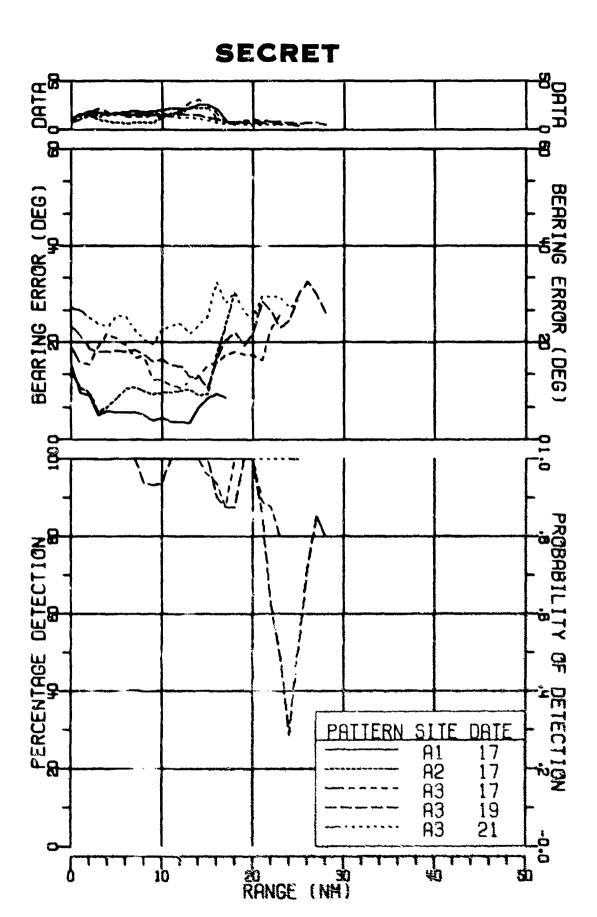


FIGURE 111-214
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
DETECTION RESULTS FOR 64HZ AT 16208 (U)

AC-77-281

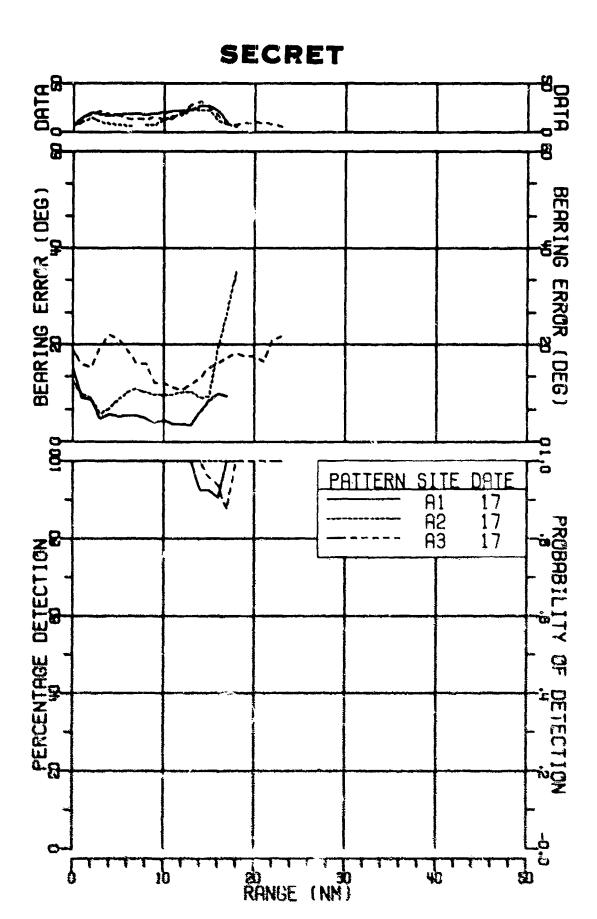


FIGURE III-215
NSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSON
DETECTION RESULTS FOR 64HZ AT 162DB (U)

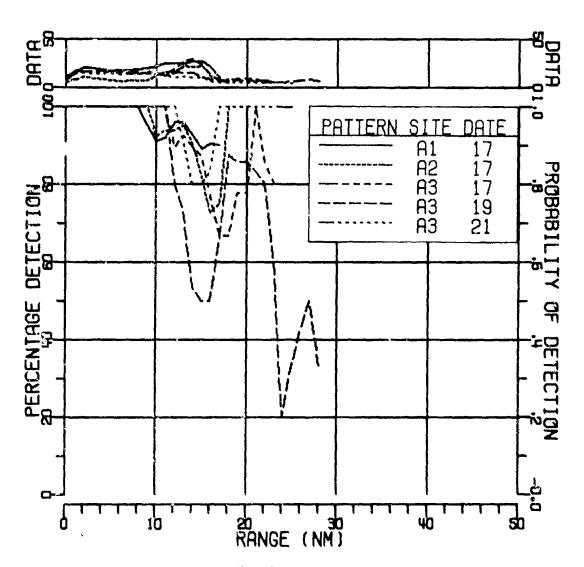


FIGURE III-216
MSS-FVT NEAR BOTTOM VERTICAL DIPOLE SENSOR
DETECTION RESULTS FOR 64HZ AT 162DB (U)

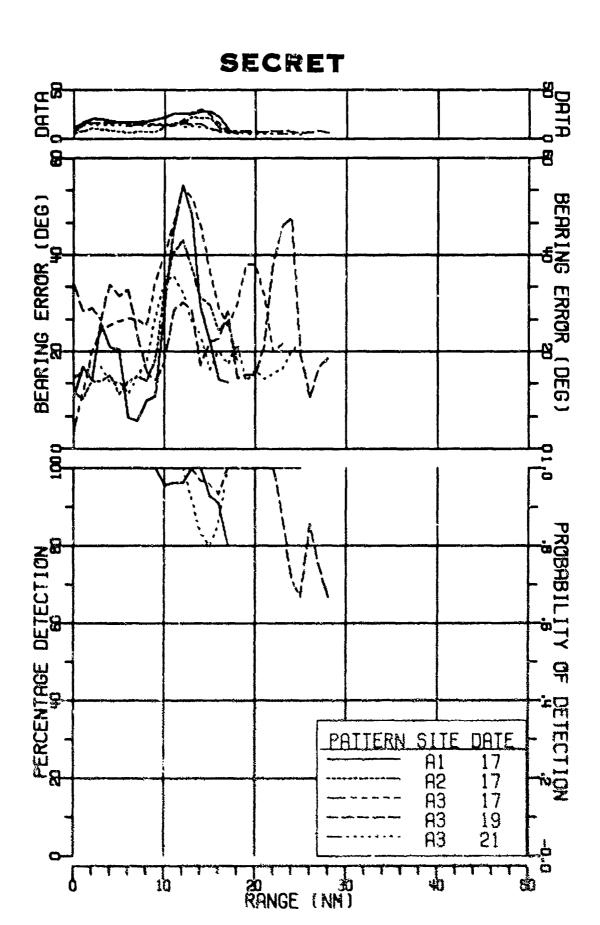


FIGURE III-217
MSS-FVI NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
DETECTION RESULTS FOR 64HZ AT 162DB (U)

AS-77-2817

-. 816

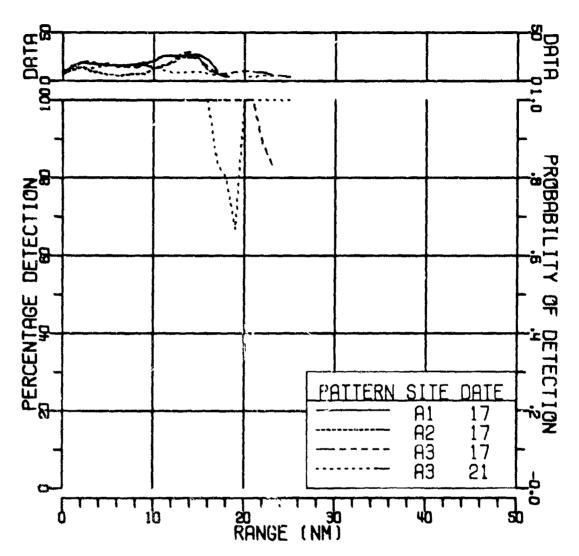


FIGURE III-218
MSS-FVT NERR BOTTOM OMNIDIRECTIONAL SENSOR
DETECTION RESULTS FOR 160HZ AT 161DB (U)

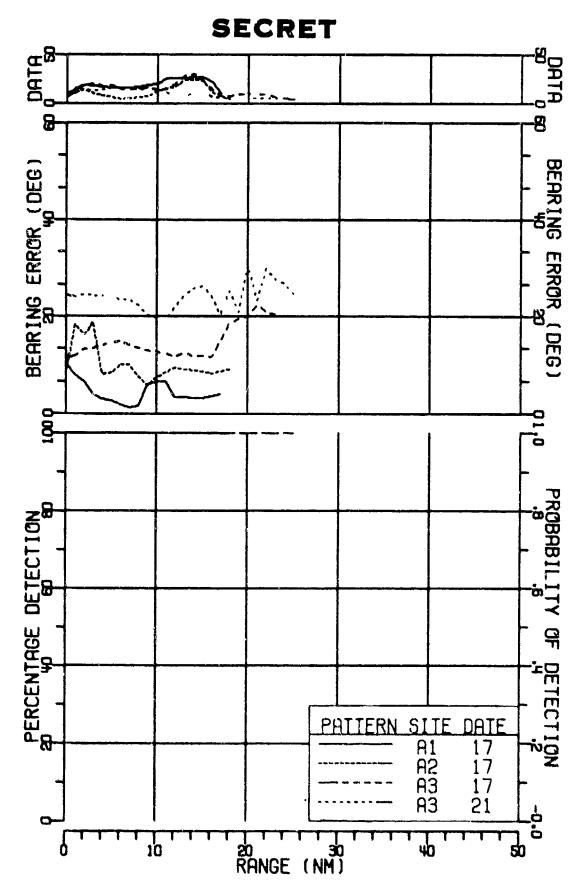


FIGURE III-219
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
DETECTION RESULTS FOR 160HZ AT 161DB (U)

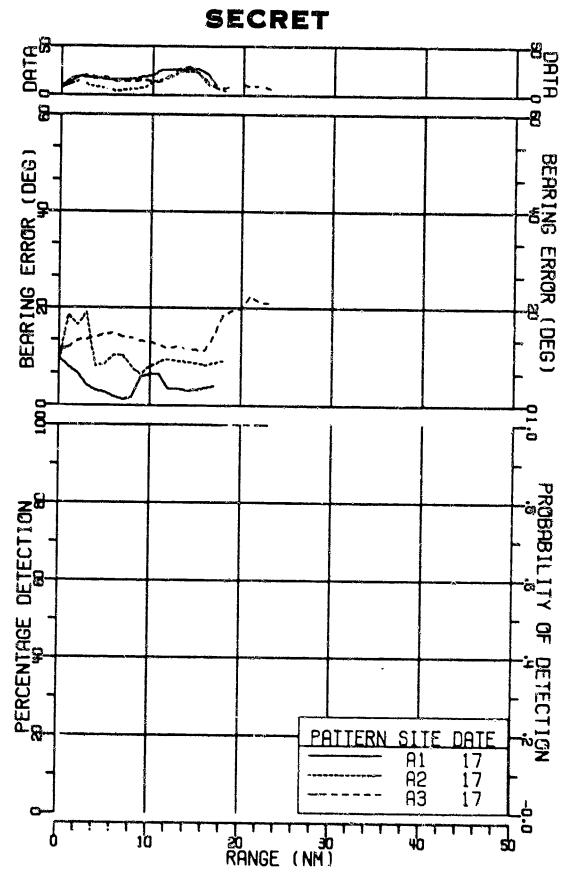


FIGURE III-220
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
DETECTION RESULTS FOR 160HZ AT 161DB (U)

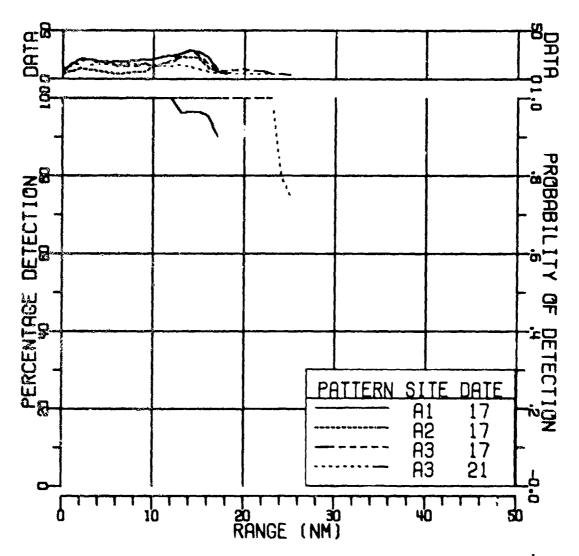


FIGURE III-221
MSS-FVT NEAR BOTTOM VERTICAL DIPOLE SENSOR
DETECTION RESULTS FOR 160HZ AT 161DB (U)

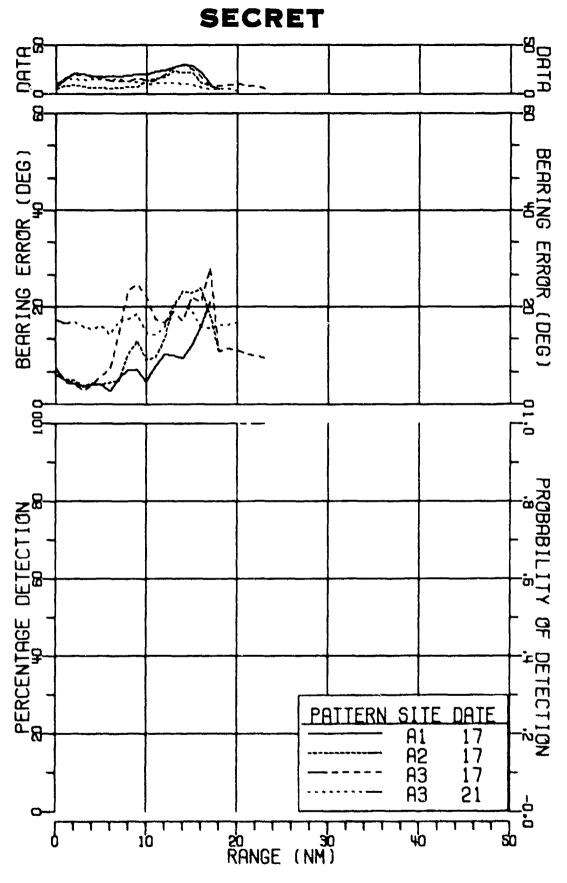


FIGURE III-222
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
DETECTION RESULTS FOR 160HZ AT 161DB (U)

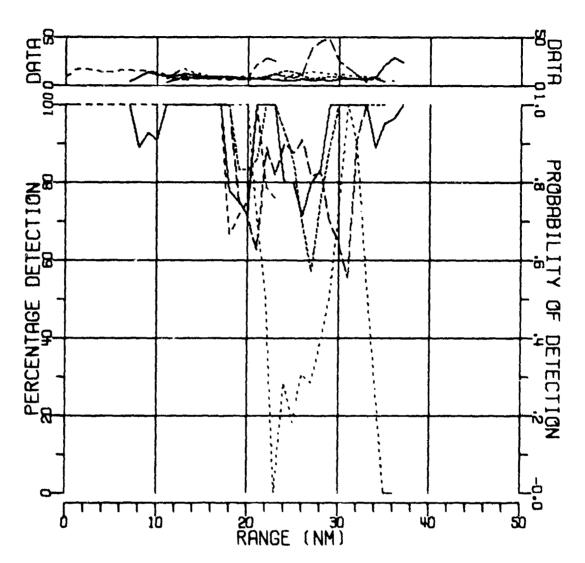


FIGURE III-223
MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR
DETECTION RESULTS FOR 70HZ AT 166DB (U)

SITE	DATE
AI	17
	17
	17 19
—	21

AS-77-2823

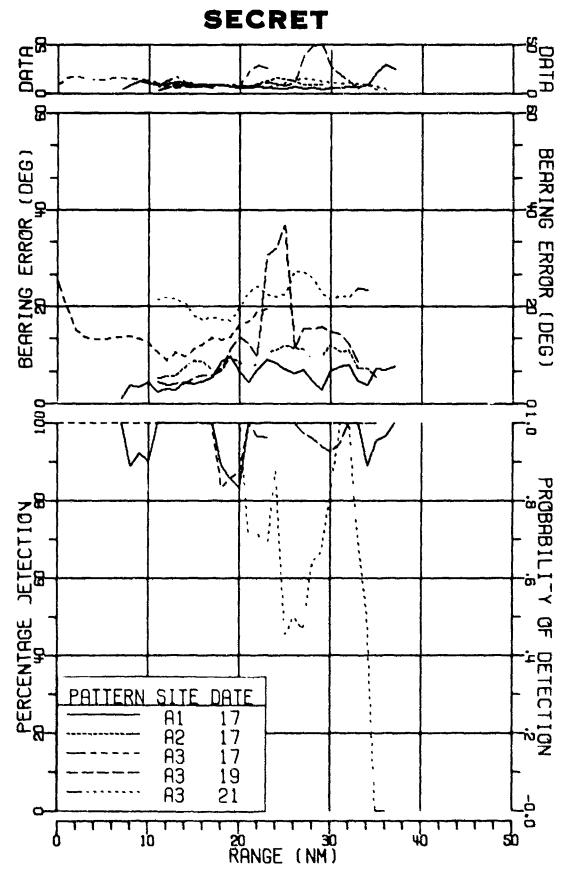


FIGURE III-224
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
DETECTION RESULTS FOR 70HZ AT 166DB (U)

AS-77-28

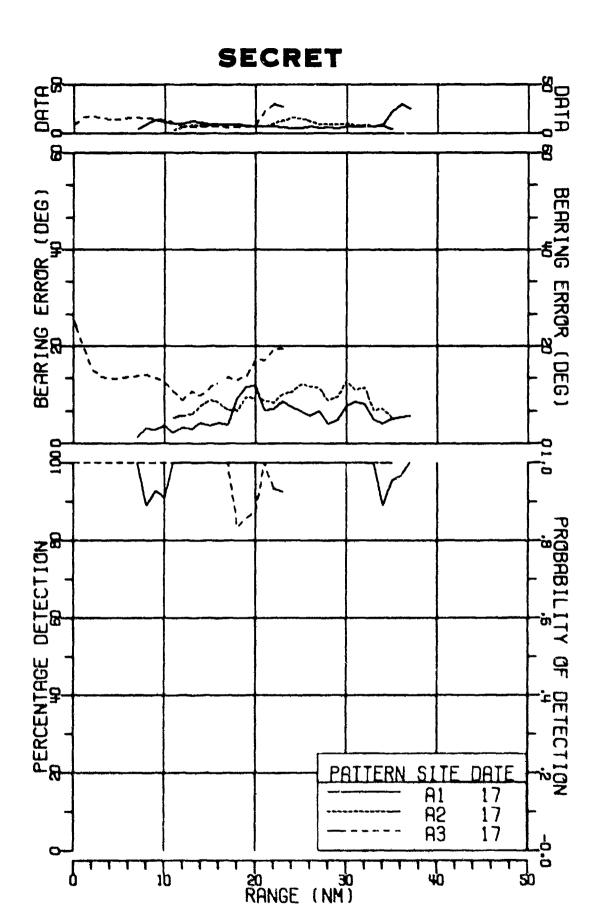


FIGURE III-225
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
DETECTION RESULTS FOR 70HZ AT 166DB (U)

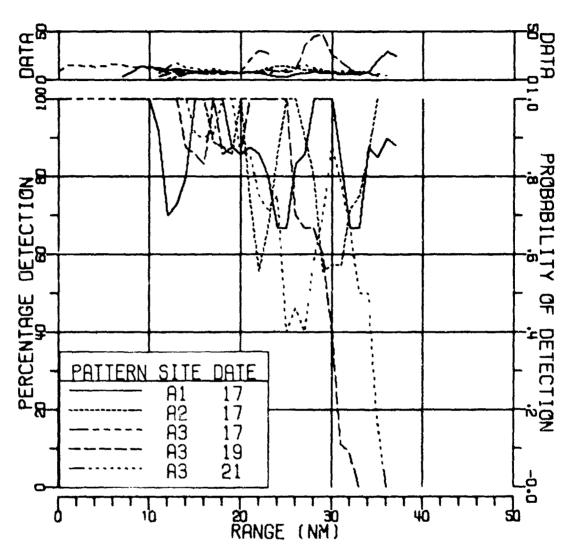


FIGURE III-226
MSS-FVT NEAR BOTTOM VERTICAL DIPOLE SENSOR
DETECTION RESULTS FOR 70HZ AT 166DB (U)

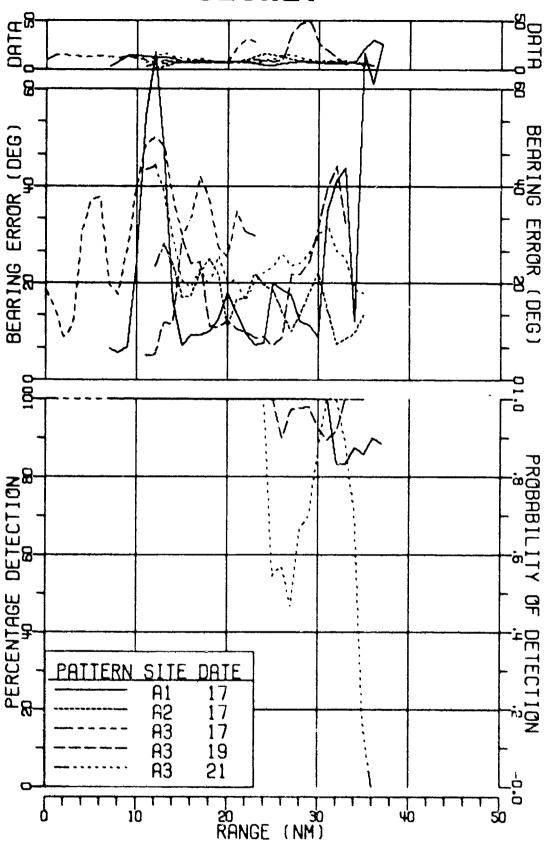


FIGURE III-227
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
DETECTION RESULTS FJR 70HZ AT 166DB (U)

SECRET

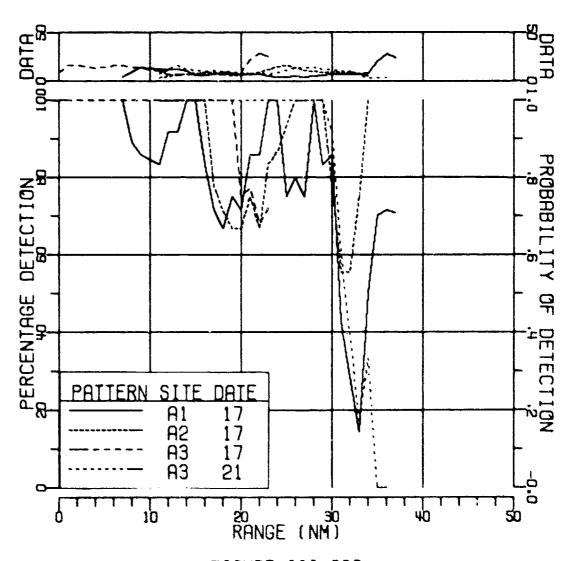


FIGURE III-228
MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR
DETECTION RESULTS FOR 170HZ AT 156DB (U)

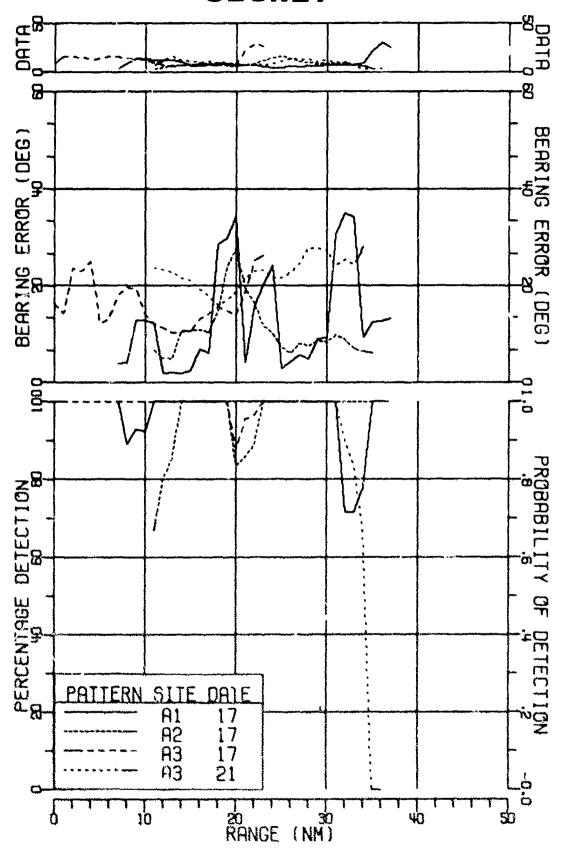


FIGURE III-229
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
DETECTION RESULTS FOR 170HZ AT 156DB (U)

SECRET

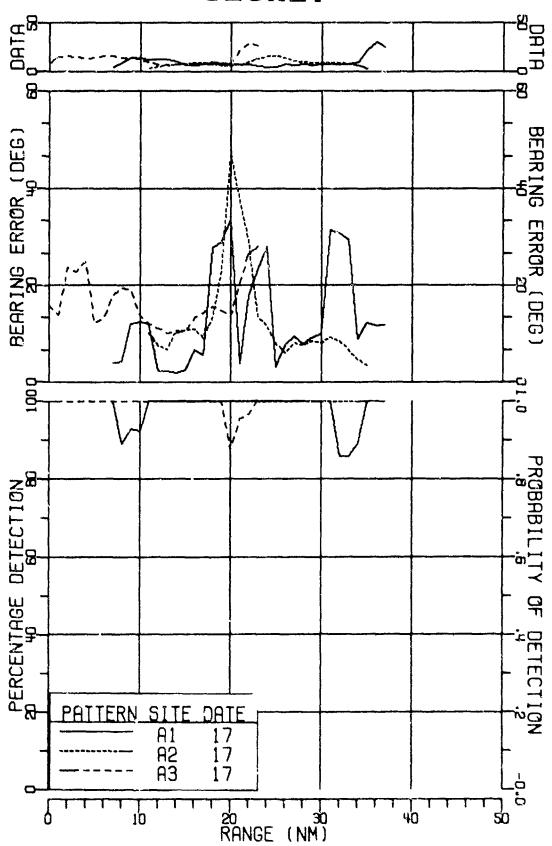


FIGURE III-230
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
DETECTION RESULTS FOR 170HZ AT 156DB (U)

SECRET

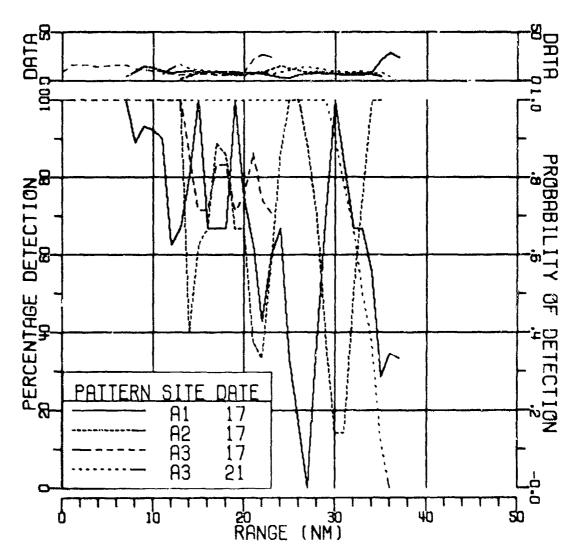


FIGURE III-231
MSS-FVT NEAR BOTTOM VERTICAL DIPOLE SENSOR
DETECTION RESULTS FOR 170HZ AT 156DB (U)

AS-77-2831

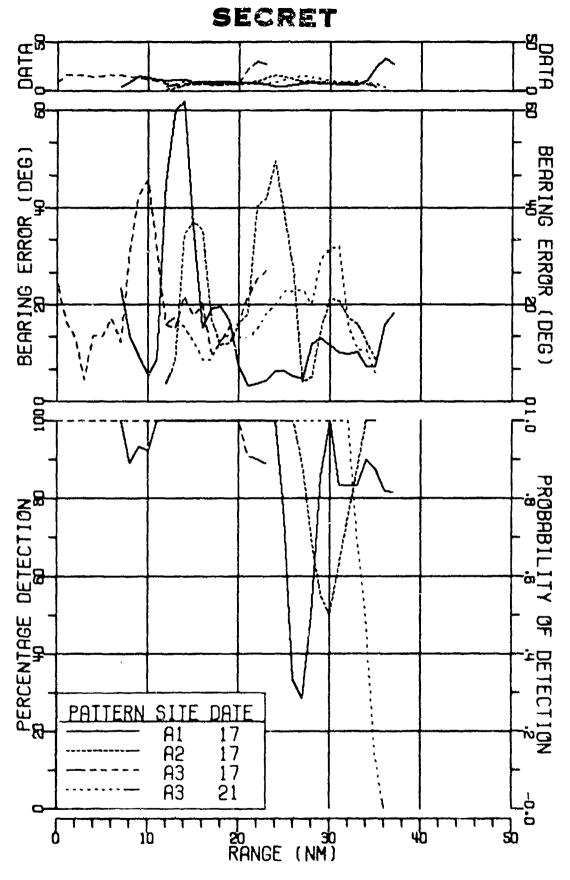


FIGURE III-232
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
DETECTION RESULTS FOR 170HZ AT 156DB (U)

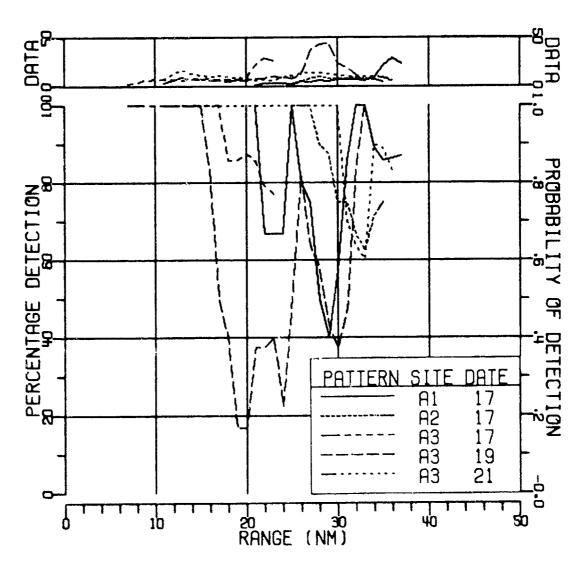


FIGURE III-233
MSS-FVT NEAR BCTTOM OMNIDIRECTIONAL SENSOR
DETECTION RESULTS FOR 335HZ AT 154DB (U)

AS- 77-2833

SECRET DATA O -8 BEARING ERROR (DEG) BEARING ERROR (DEG) PROBABILITY OF DETECTION ED PERCENTAGE 30 DETECTION SITE DATE PATTERN A1 17 A2 A3 17 17 A3 19 A3 21 20 30 RANGE (NM) 10

The state of the s

FIGURE III-234
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
DETECTION RESULTS FOR 335HZ AT 154DB (U)

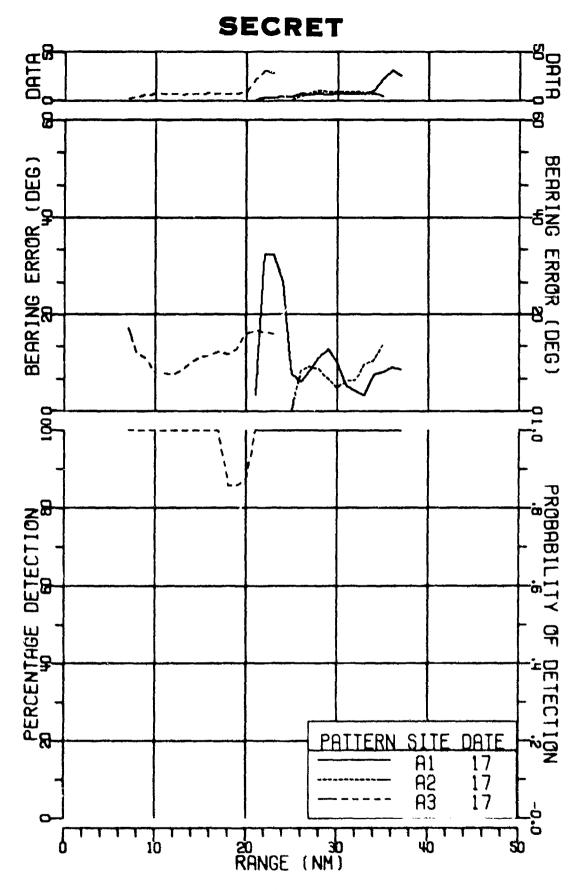


FIGURE III-235
NSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
DETECTION RESULTS FOR 335HZ AT 154DB (U)

UNCLASSIFIED

APPENDIX F

BEARING ERROR versus SIGNAL-TO-NOISE RATIO CURVES (U)

(FIGURES III-236 - III-257)

(The reverse of this page is blank.)
UNCLASSIFIED

SECRET MEAN ERROR (DEG) MEAN ERROR (DEG) ERROR (DEG) RAS 12 SITE DATE A1 A2 A3 A3 17 17 17 21

FIGURE III-236
MSS-FVT NEAR BOTTOM SINGLE CARDIDIDS SENSOR
BEARING ERROR RESULTS FOR 55HZ AT 141DB (U)

S/N (DB// 1 HZ)

AS-77-28]

ab

10

-10

-50

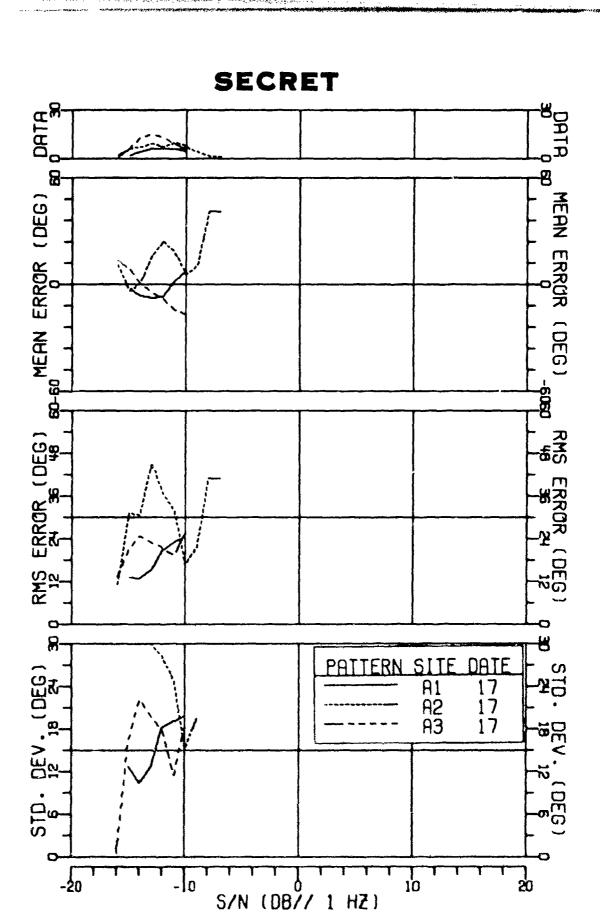


FIGURE III-237
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
BEARING ERROR RESULTS FOR 55HZ AT 141DB (U)

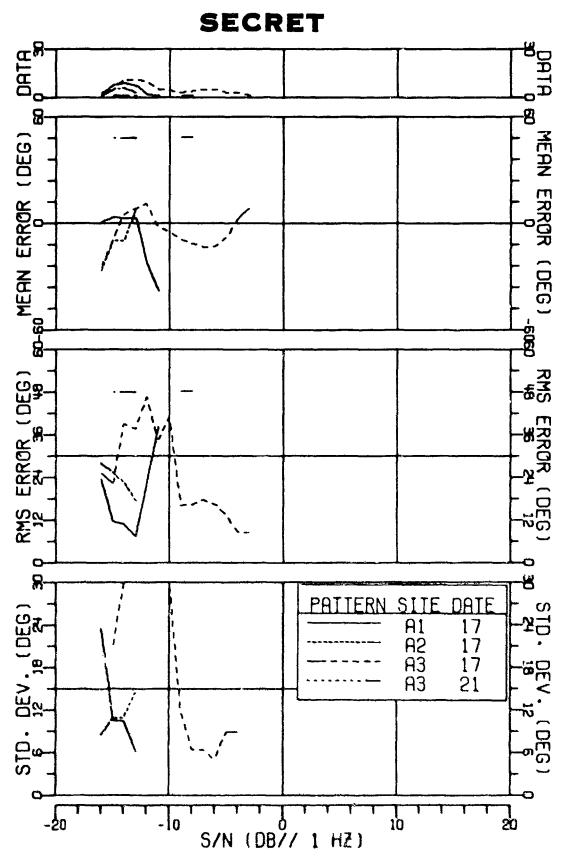


FIGURE III-238
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
BEARING ERROR RESULTS FOR 55HZ AT 141DB (U)

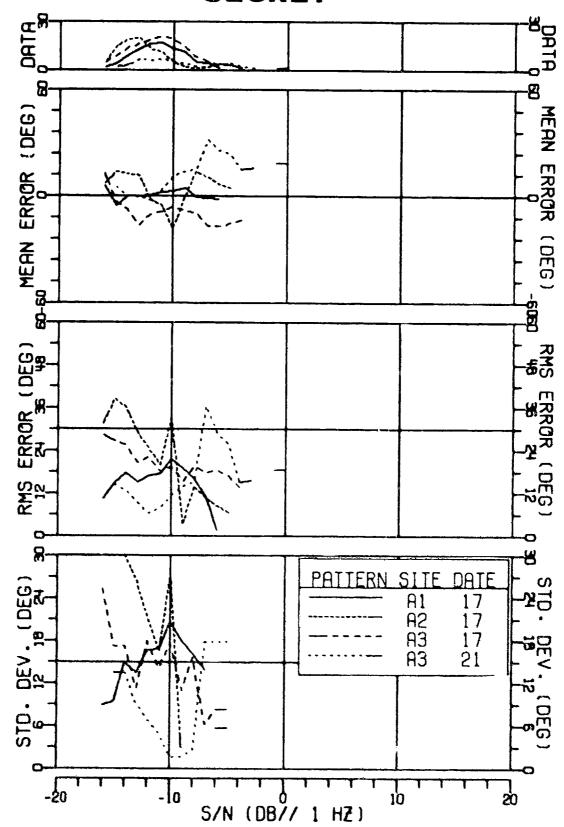


FIGURE III-239
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
BEARING ERROR RESULTS FOR 155HZ AT 134DB (U)

SECRET

AS-71-2839

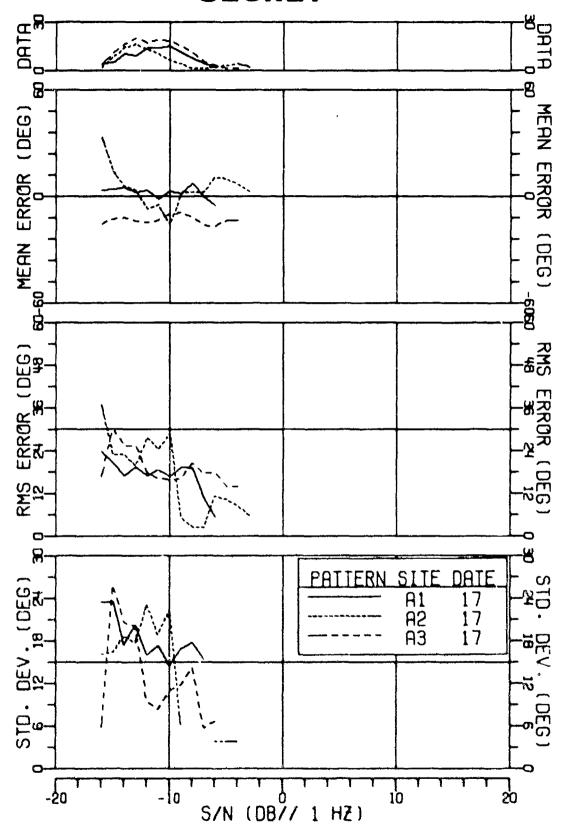


FIGURE III-240
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
BEARING ERROR RESULTS FOR 155HZ AT 134DB (U)

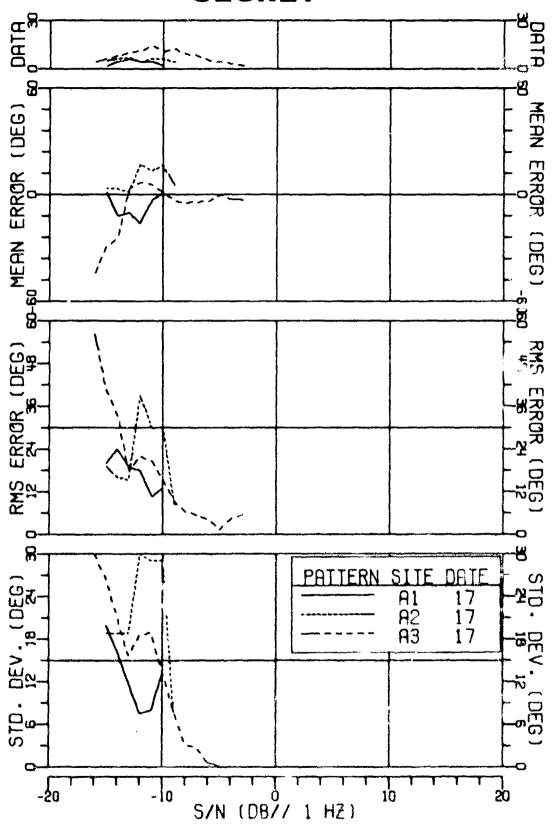


FIGURE III-241
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
BEARING ERROR RESULTS FOR 155HZ AT 134DB (U)

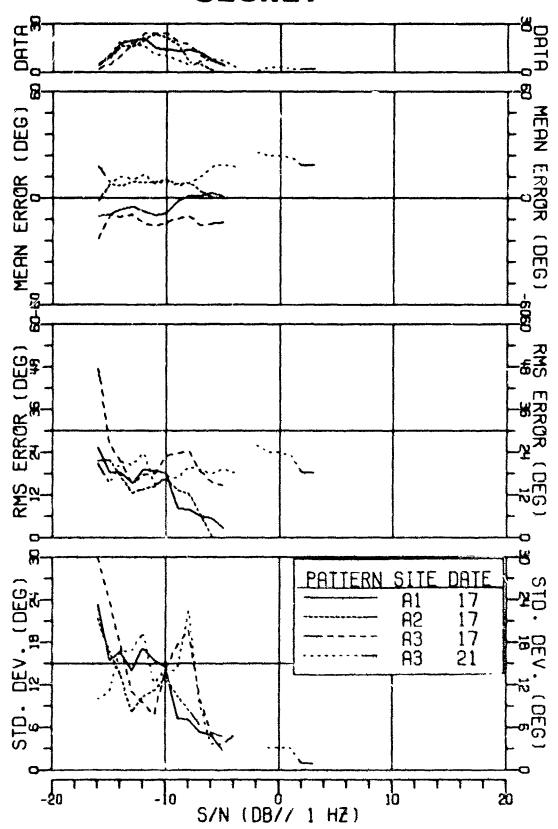


FIGURE III-242 MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR BEARING ERROR RESULTS FOR 305 HZ AT 136DB (U)

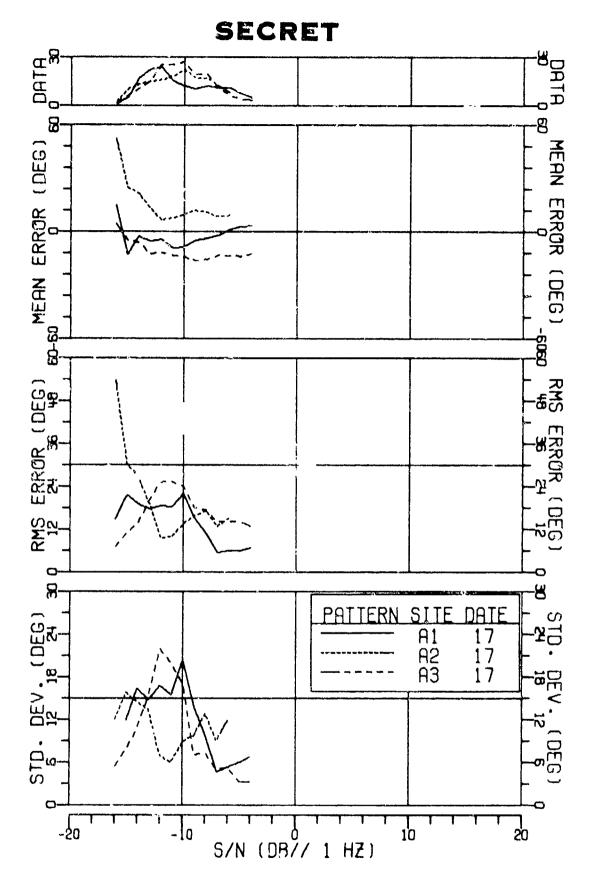


FIGURE III-243 MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR BEARING ERROR RESULTS FOR 305 HZ AT 136DB (U)

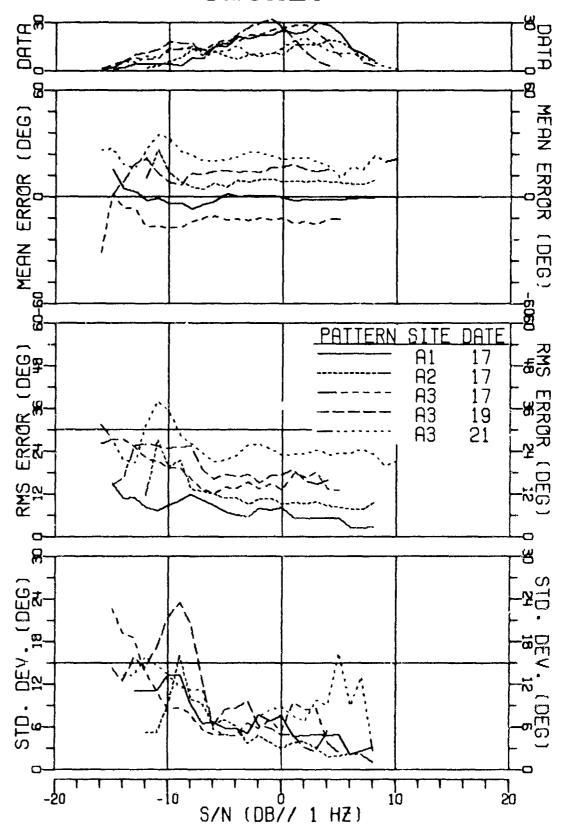


FIGURE III-244 MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR BEARING ERROR RESULTS FOR 64HZ AT 162DB (U)

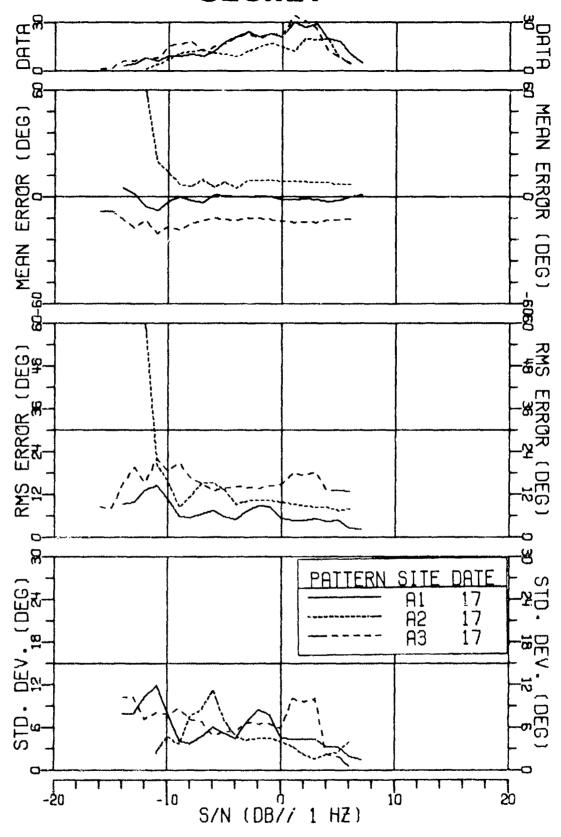


FIGURE III-245 MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR BEARING ERROR RESULTS FOR 64HZ AT 162DB (U)

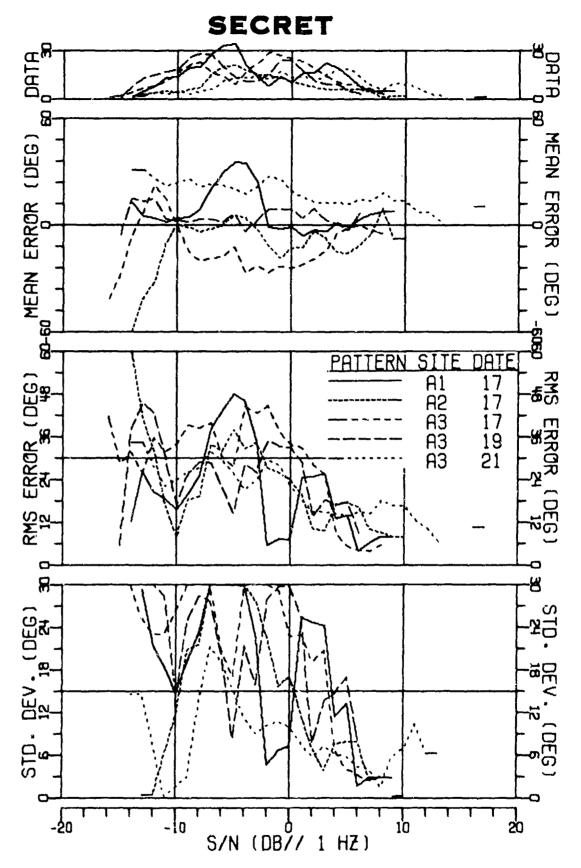


FIGURE III-246
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
BEARING ERROR RESULTS FOR 64HZ AT 162DB (U)

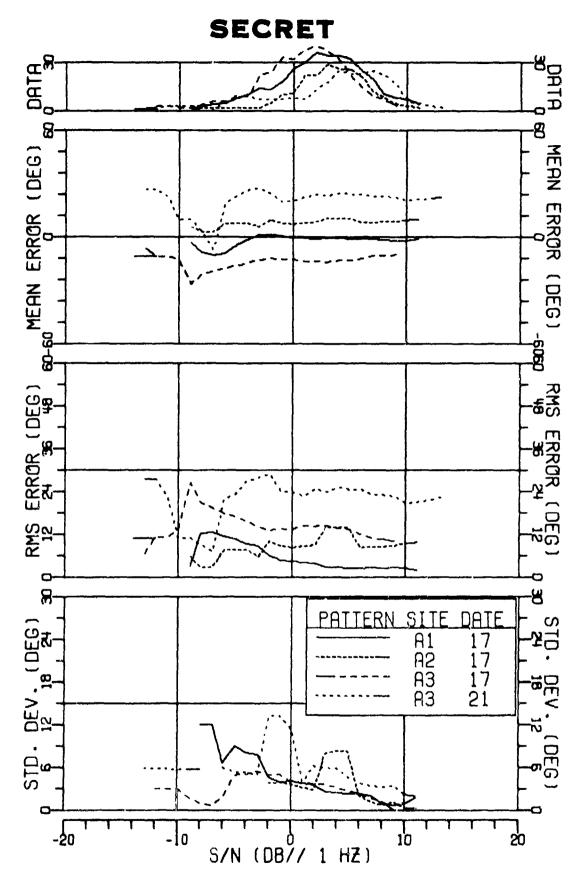


FIGURE III-247 MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR BEARING ERROR RESULTS FOR 160HZ AT 161DB (U)

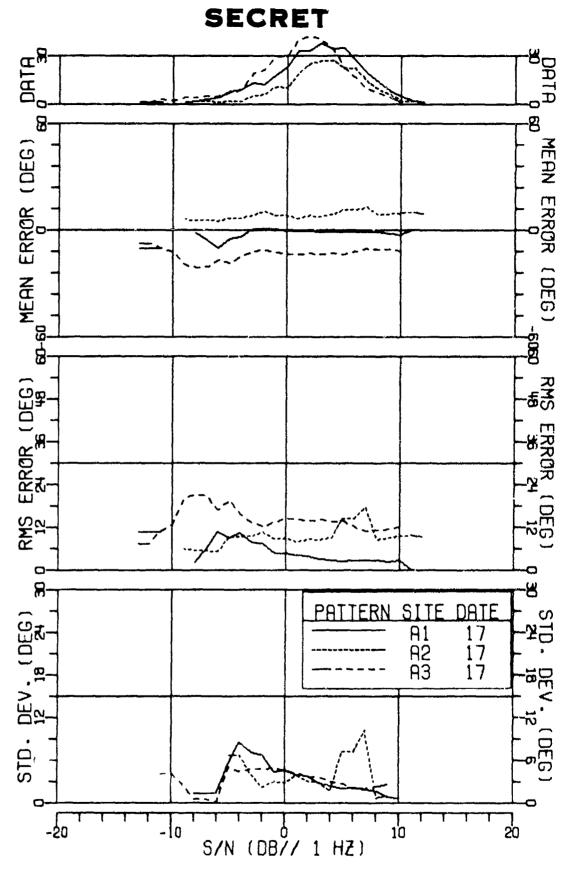


FIGURE III-248
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
BEARING ERROR RESULTS FOR 160HZ AT 161DB (U)

285

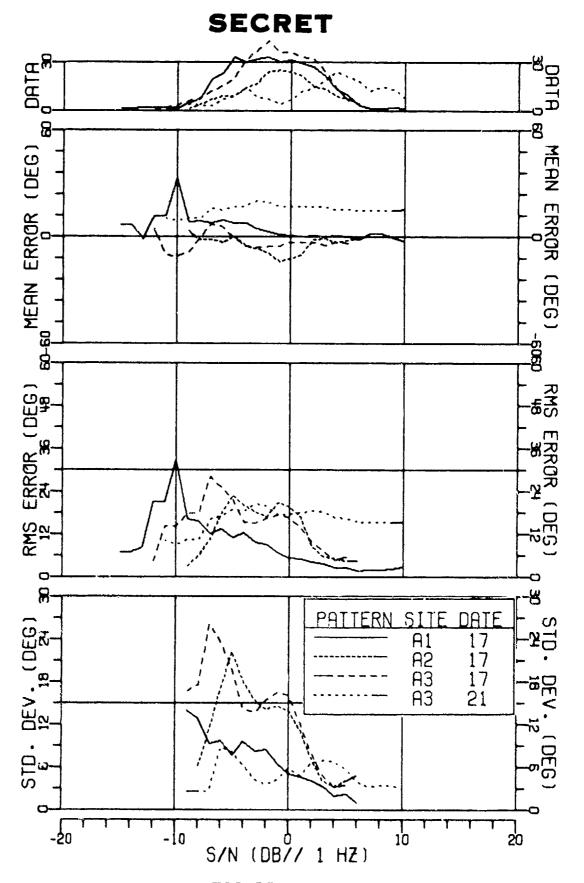


FIGURE III-249
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
BEARING ERROR RESULTS FOR 160HZ AT 161DB (U)

AC-77-2849

SECRET MEAN ERRUR (DEG) MEAN ERROR (DEG) ERROR (DEG) RMS 12 8 SITE DATE PATTERN DEV. (DEG) 17 A1 A2 A3 A3 A3 .7 17 19 21 STD. 20 -20

FIGURE III-250
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
BEARING ERROR RESULTS FOR 70HZ AT 166DB (U)

S/N (DB// 1 HZ)

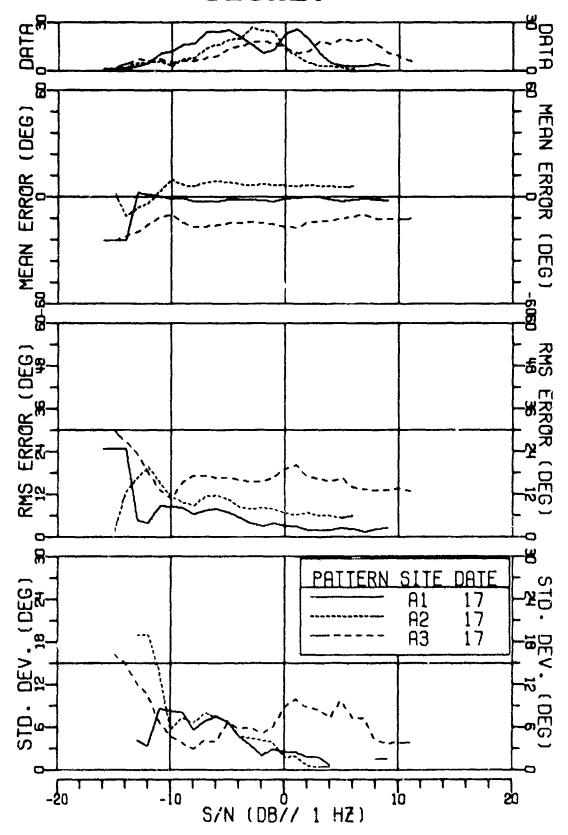


FIGURE III-251
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
BEARING ERROR RESULTS FOR 70HZ AT 166DB (U)

AS-77-2851

850

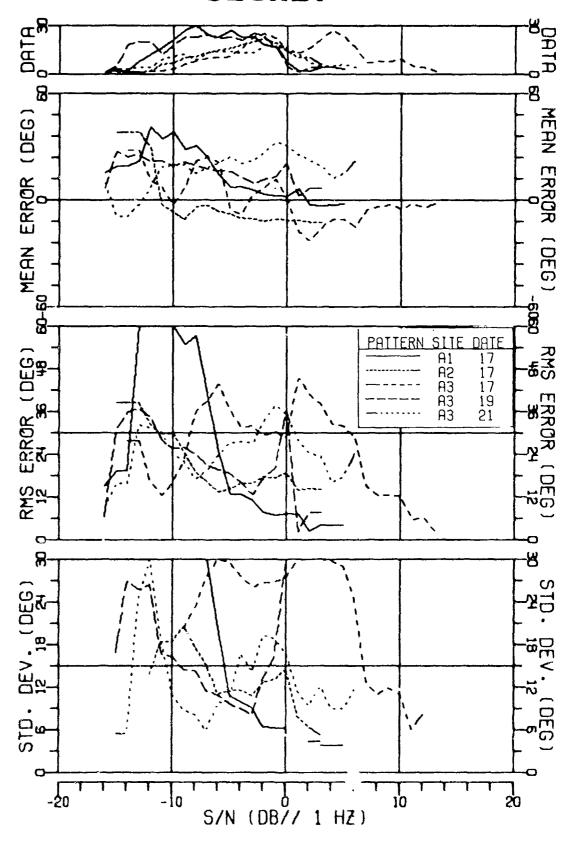


FIGURE TII-252
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
BEARING ERROR RESULTS FOR 70HZ AT 166DB (U)

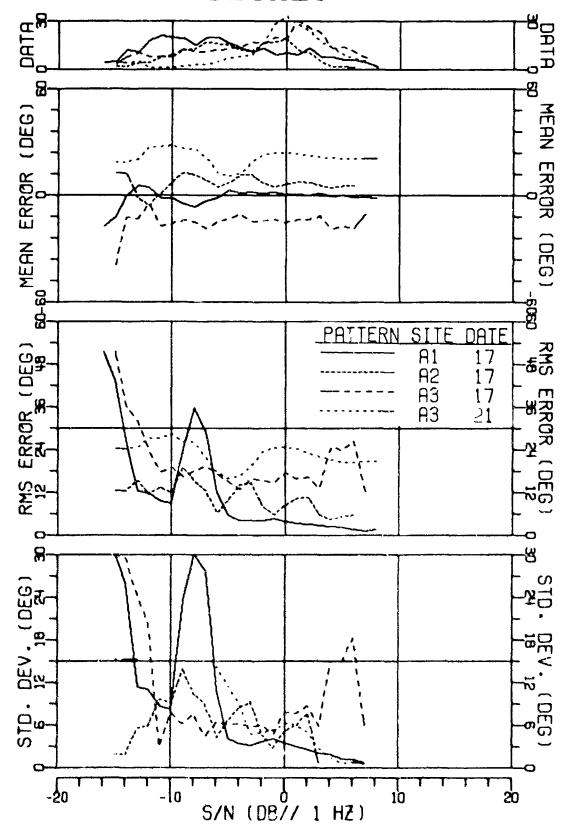


FIGURE III-253
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
BEARING ERROR RESULTS FOR 170HZ AT 156DB (U)

SECRET DATA O MEAN MEAN ERROR (DEG) ERROR (DEG) 89-69 -50EO SITE PATTERN DATE RAS Season ERROR (DEG) A1 A3 17 17 A3 A3 19 21 SE Se 8 . (DEG) 25. 25. STD 20 10 -20 S/N (DB// 1 HZ)

FIGURE III-255
MSS-FVT NEAR BOTTOM DIFFERENCED CARDIOIDS SENSOR
BEARING ERROR RESULTS FOR 170HZ AT 156DB (U)

291

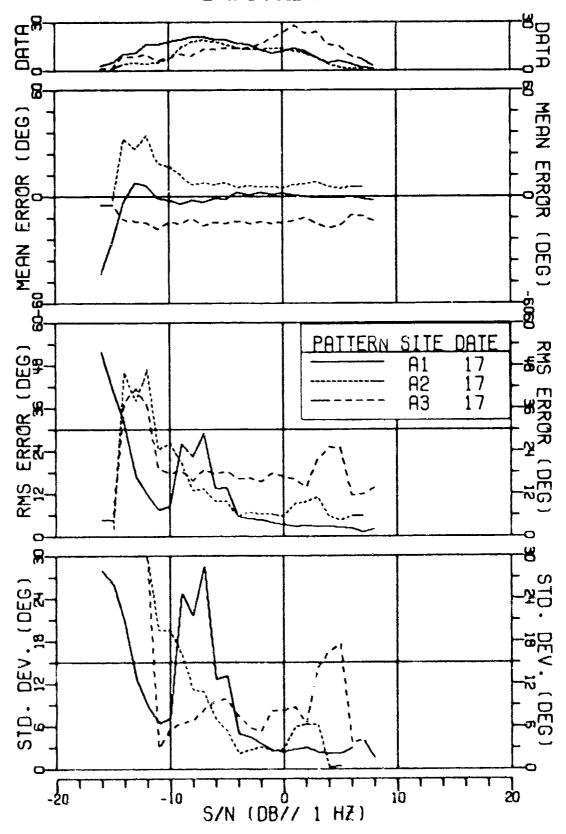


FIGURE 111-254
MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR
BEARING ERROR RESULTS FOR 170HZ AT 156DB (U)

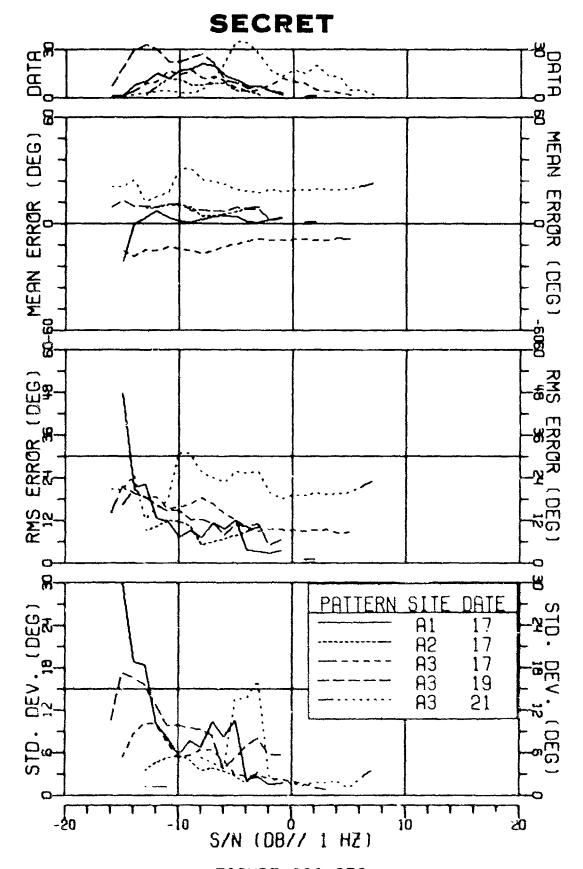


FIGURE III-256
MSS-FVT NEAR BOTTOM SINGLE CARDIOIDS SENSOR
BEARING ERROR RESULTS FOR 335HZ AT 154DB (U)

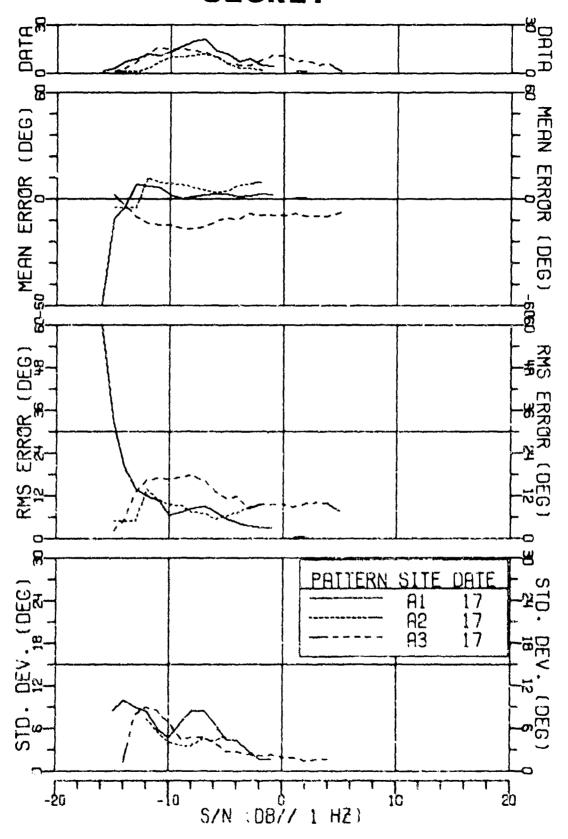


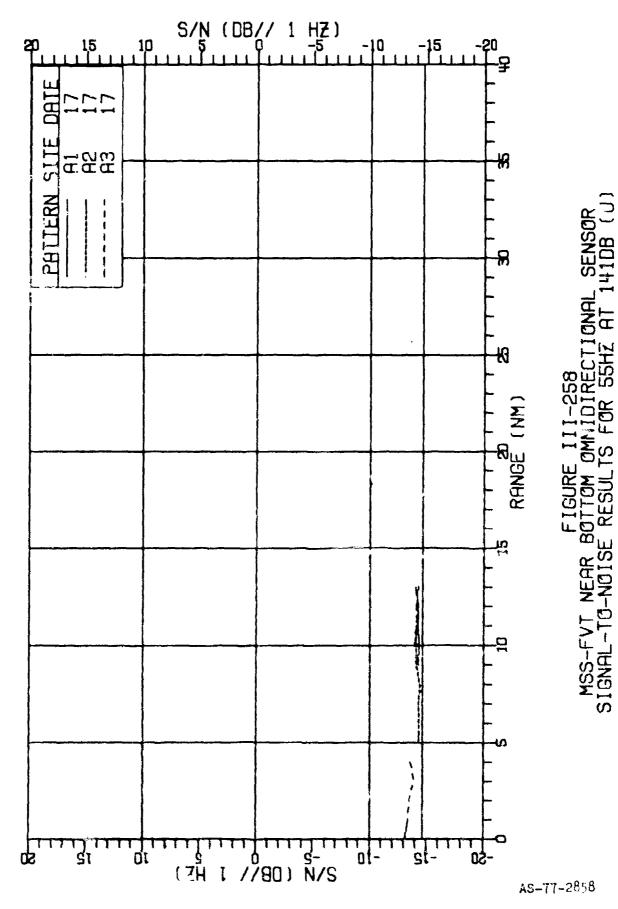
FIGURE III-257 MSS-FVT NEAR BOTTOM MAX GAIN LIMACONS SENSOR BEARING ERROR RESULTS FOR 335HZ AT 154DB (U)

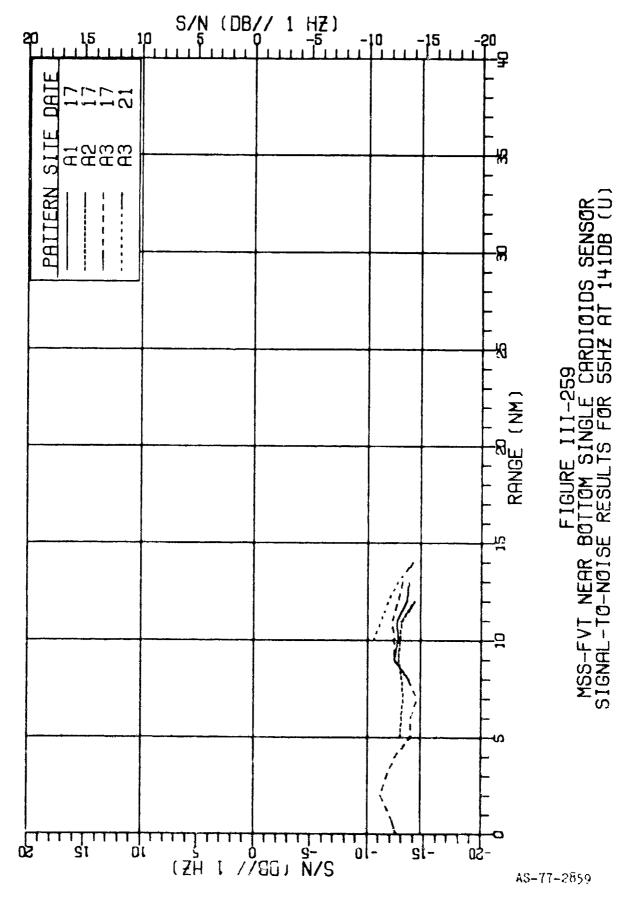
UNCLASSIFIED

APPENDIX G

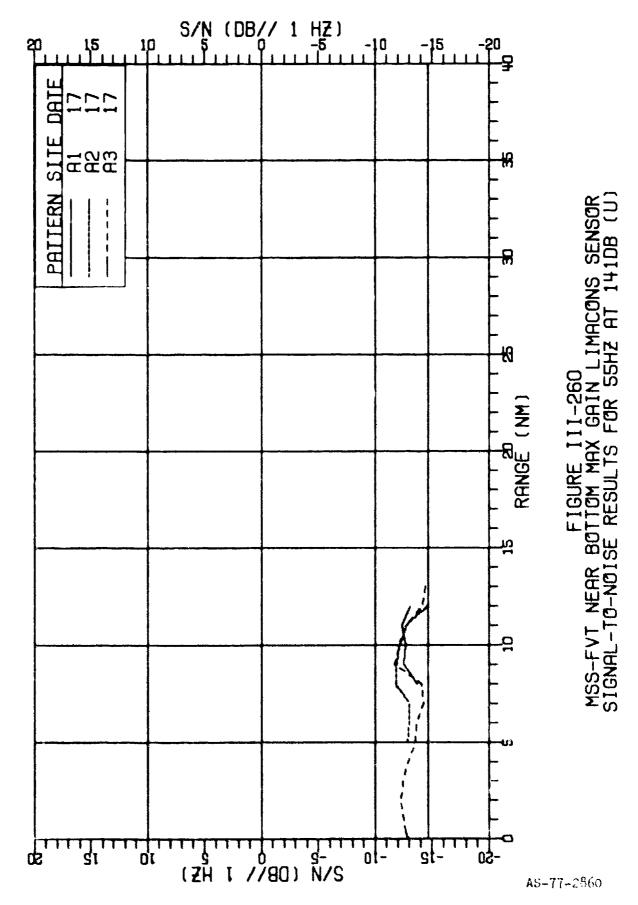
SIGNAL-TO-NOISE RATIO versus RANGE CURVES (U)

(FIGURES 111-258 - 111 293)

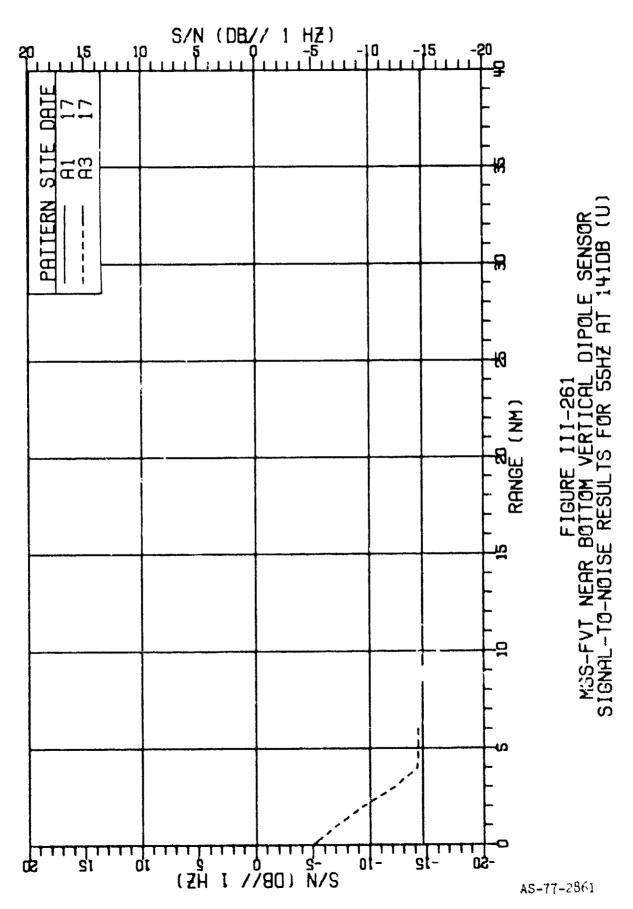




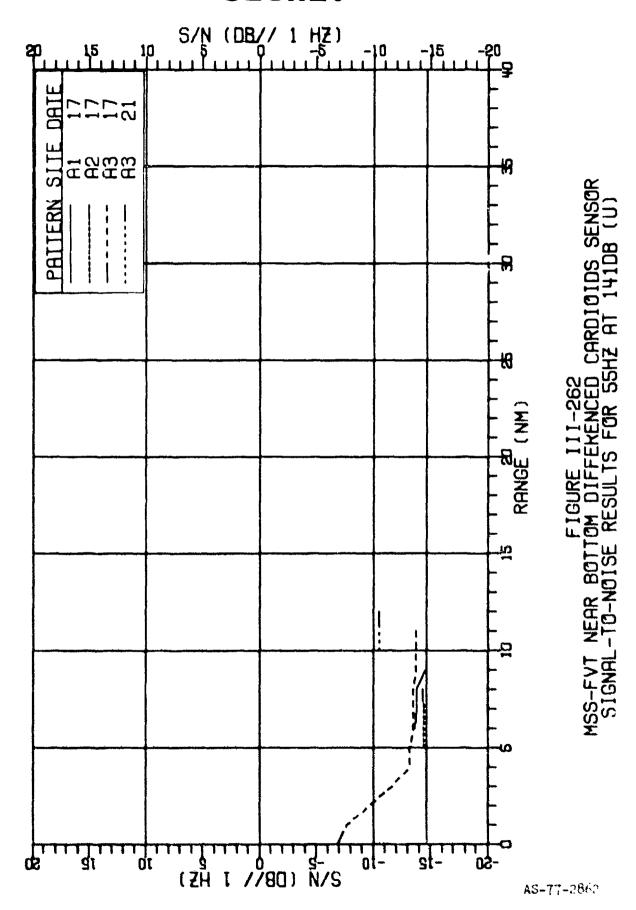
208



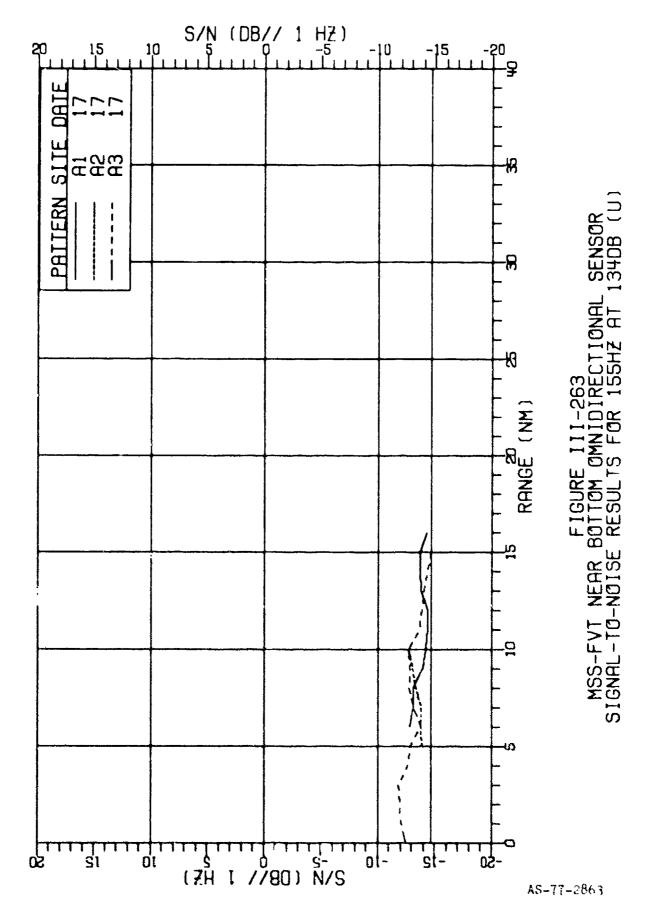
299



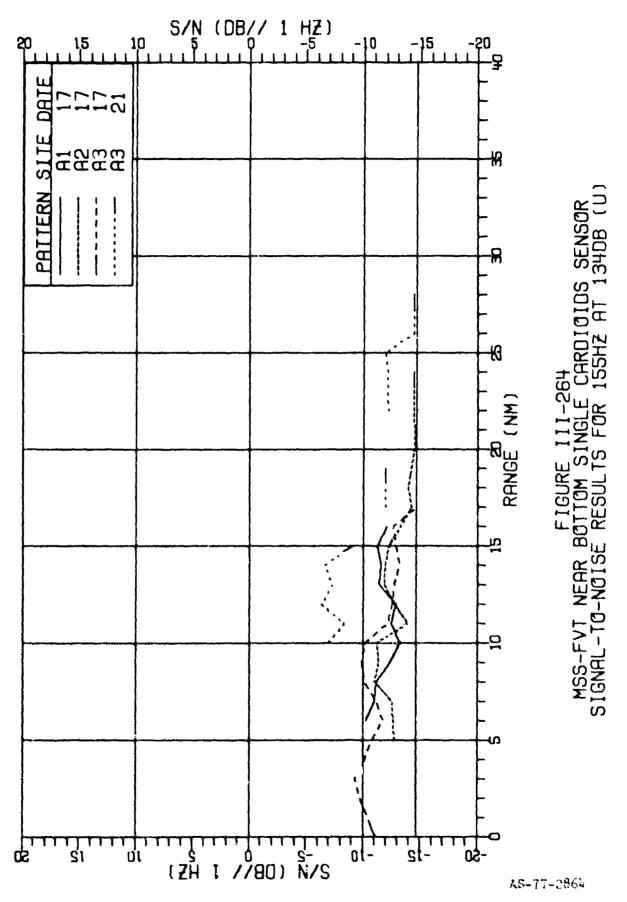
300



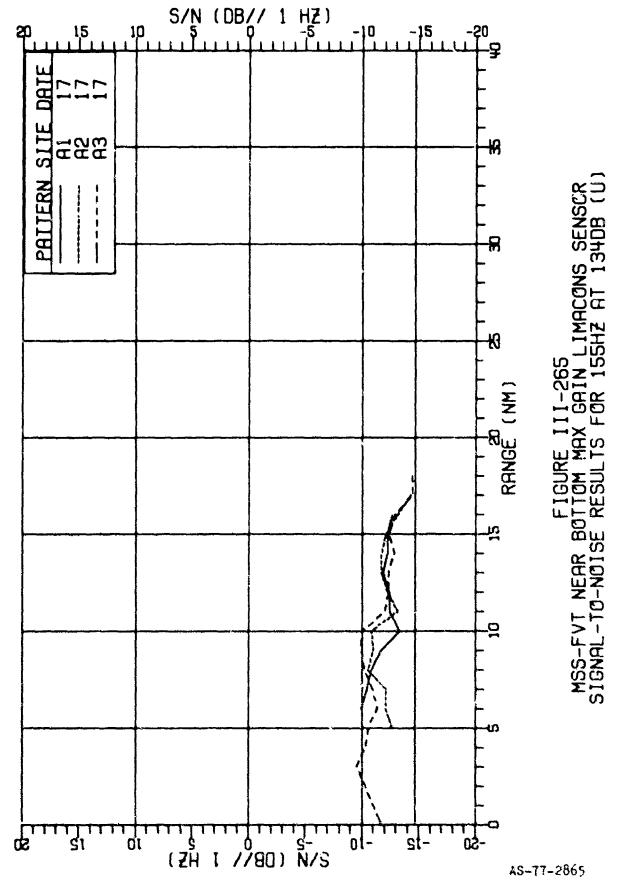
301



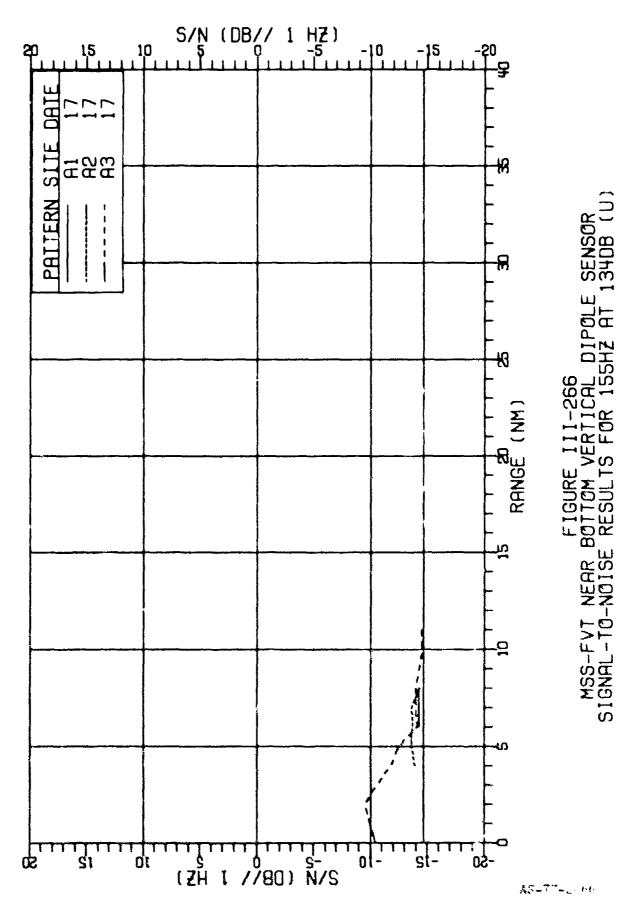
302

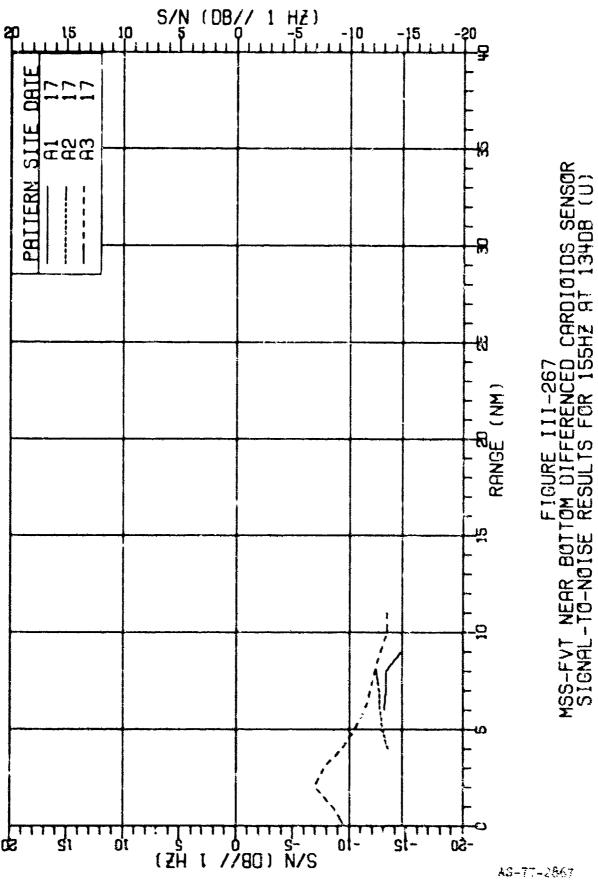


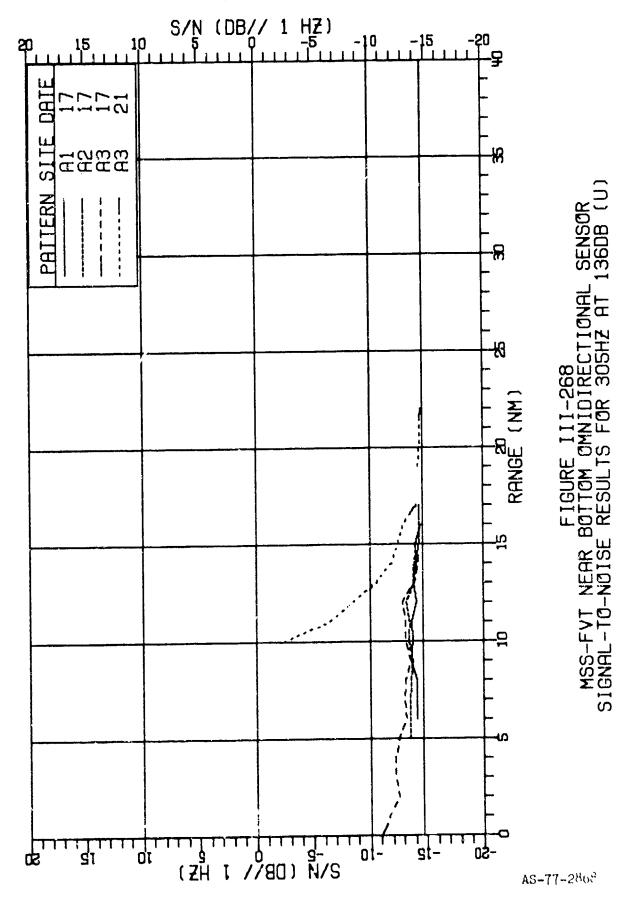
303

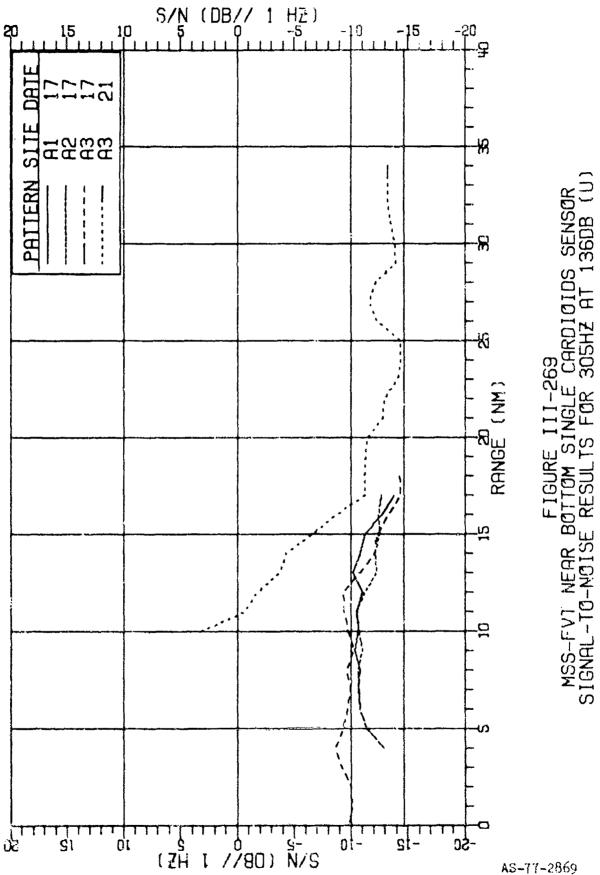


304





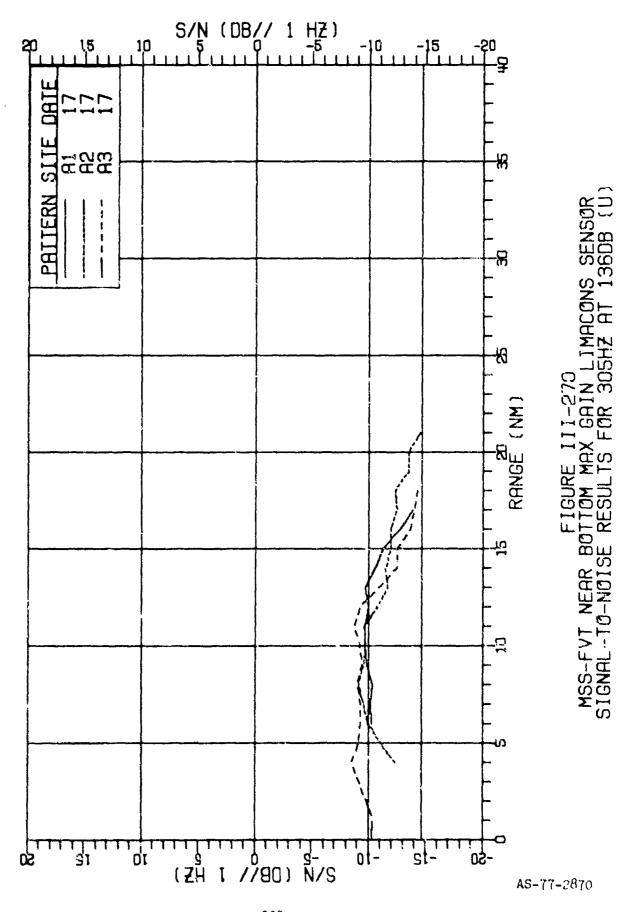




AS-77-2869

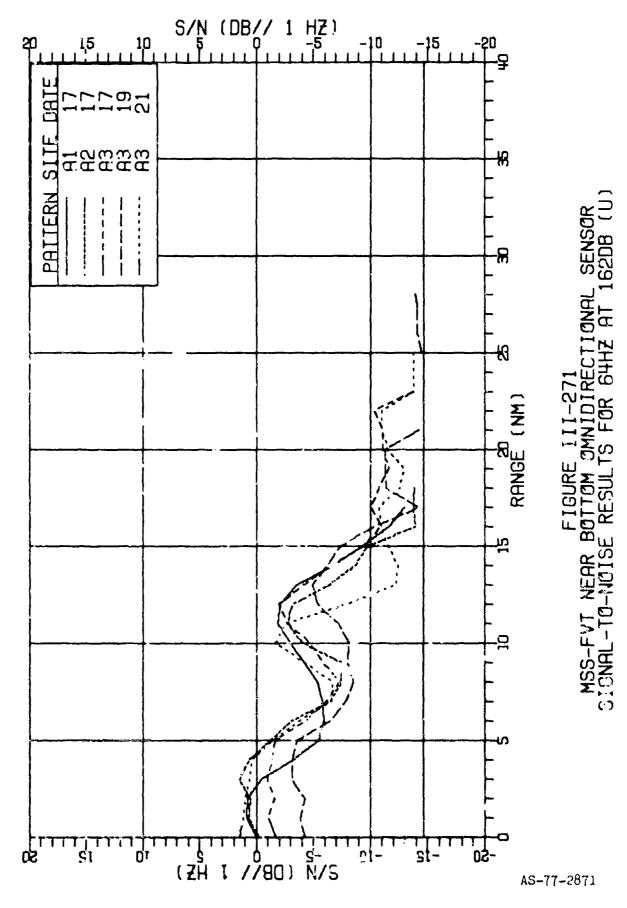
308 SECRET

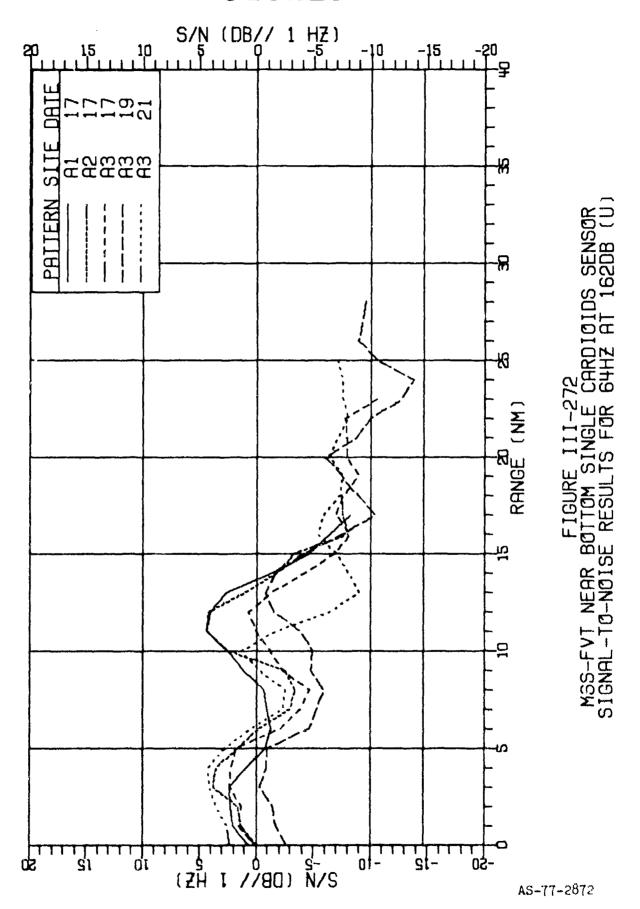
Jak Jako me



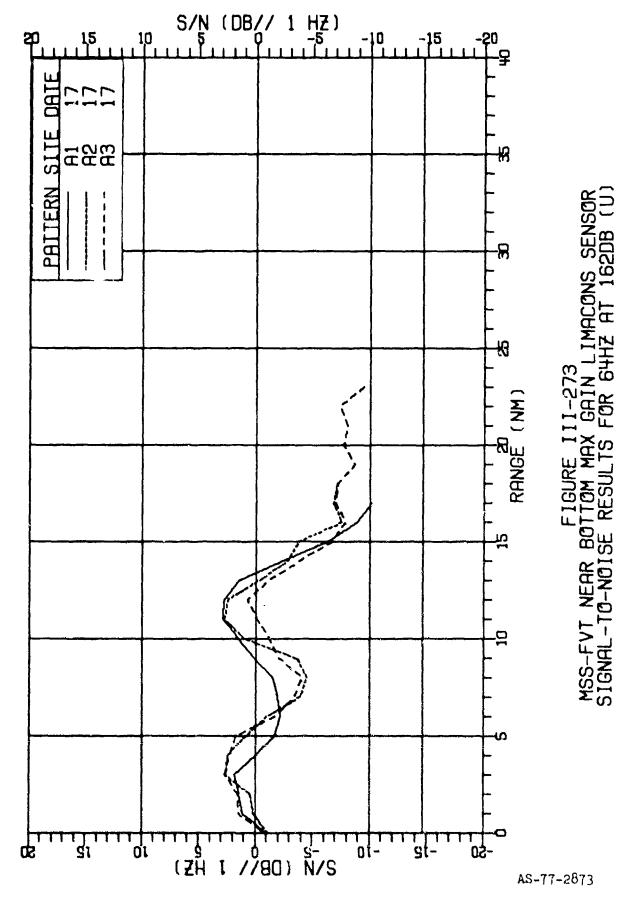
SECRET

1

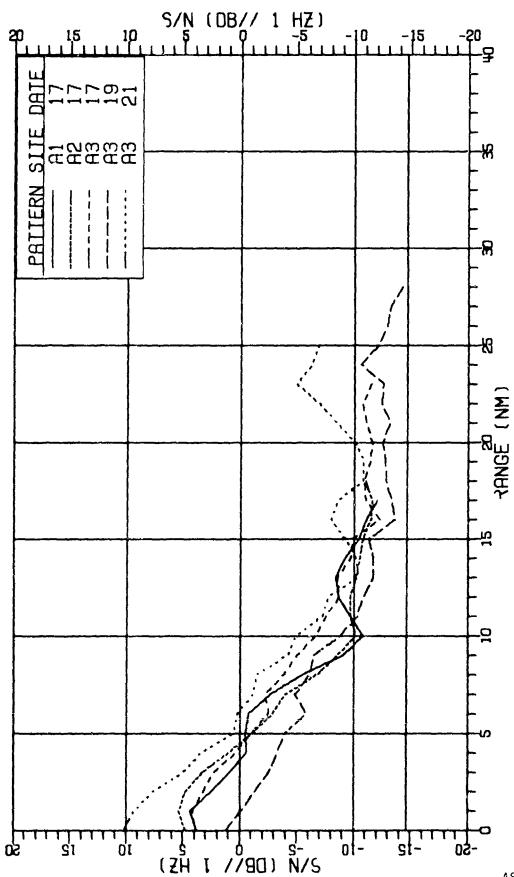




311

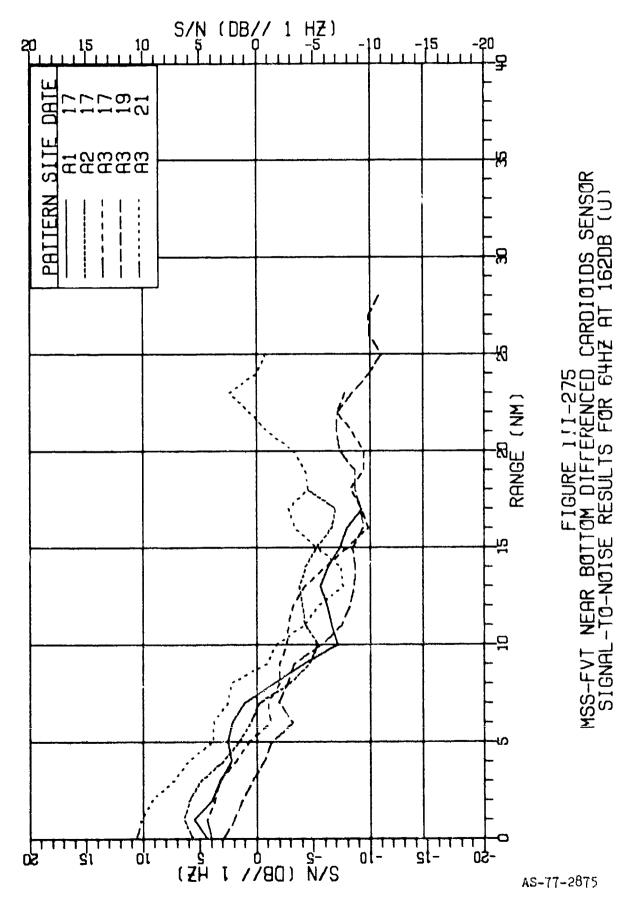


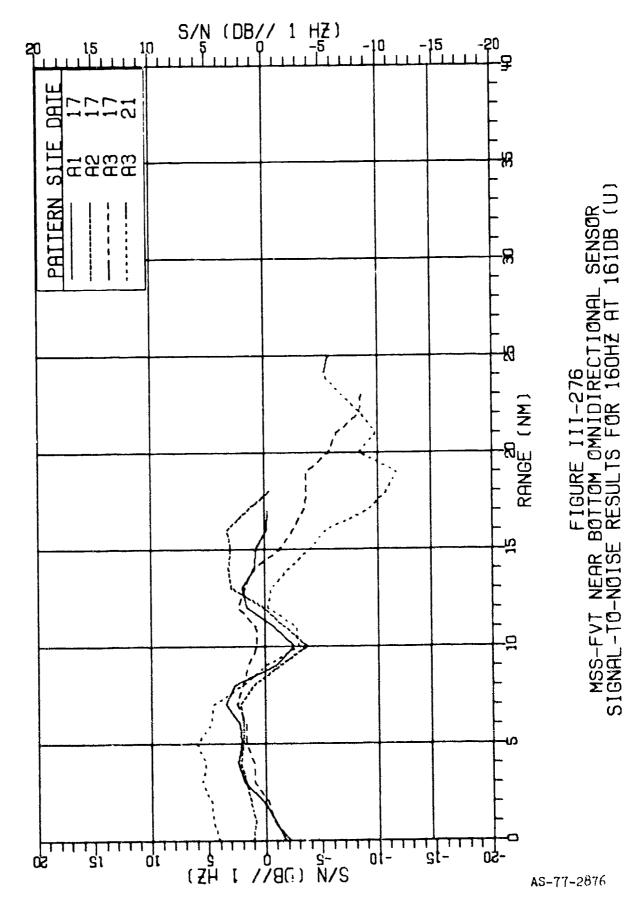
312



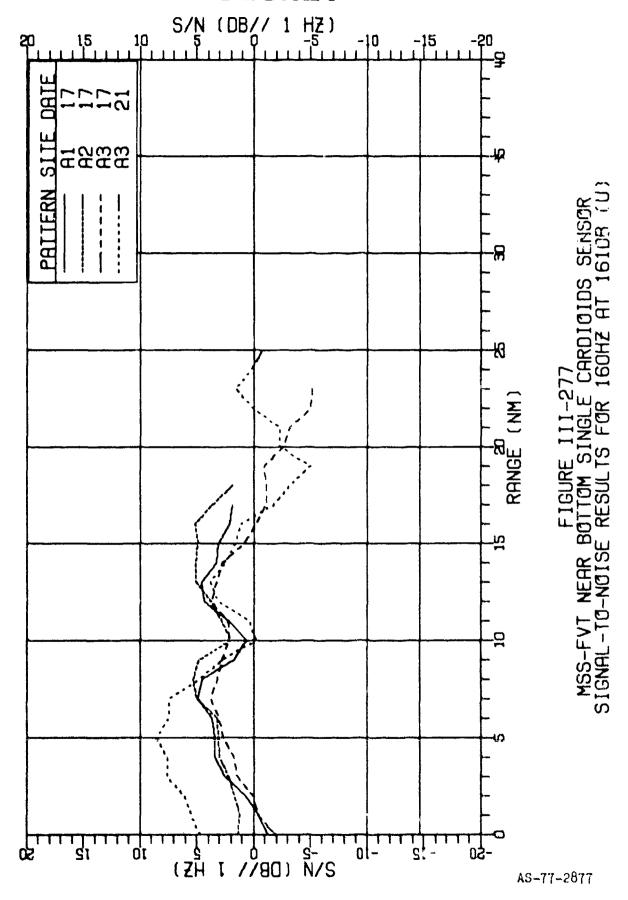
MSS-FVT NEAR BOTTOM VERTICAL DIPOLE SENSOR SIGNAL-TO-NOISE RESULTS FOR 64HZ AT 162DB (!)

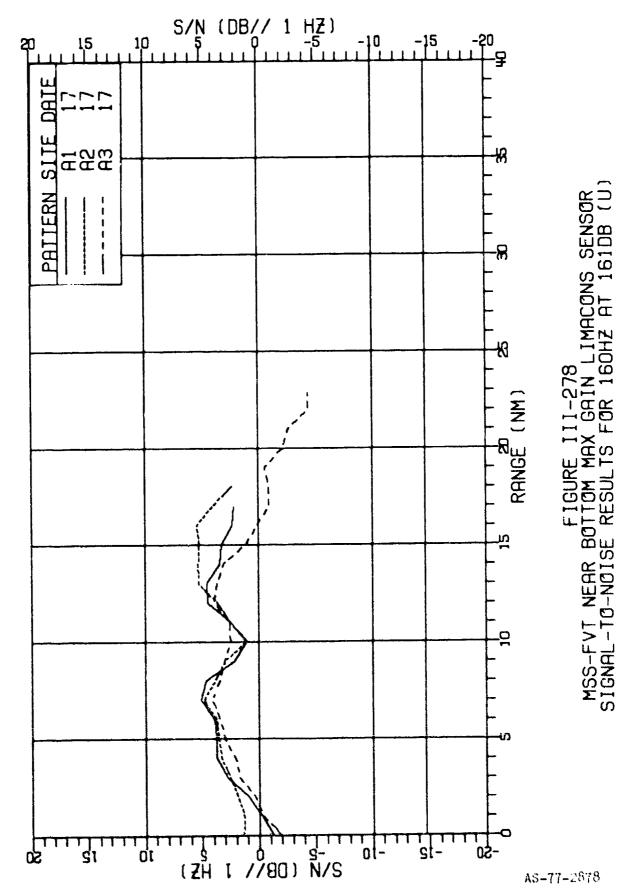
AS-77-2874



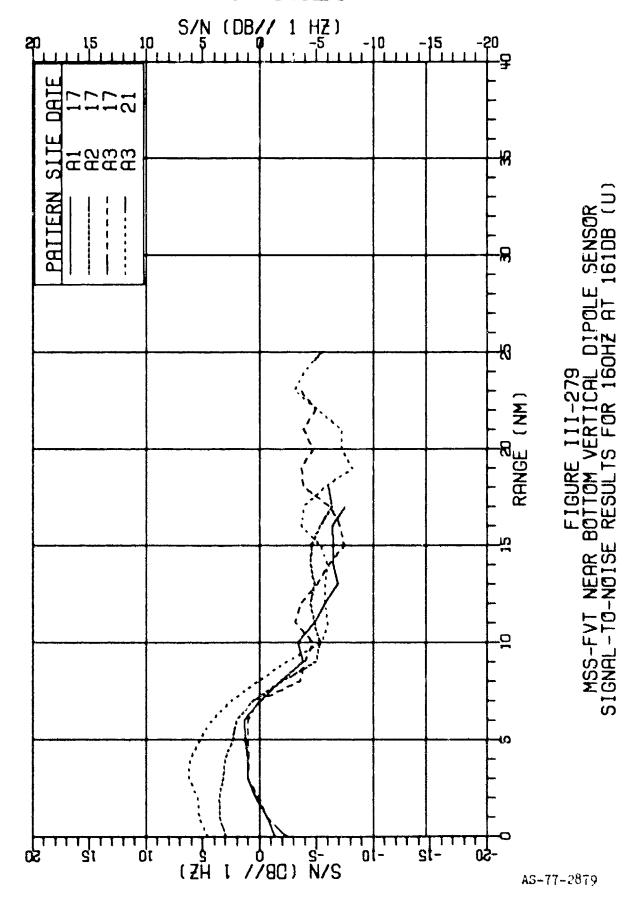


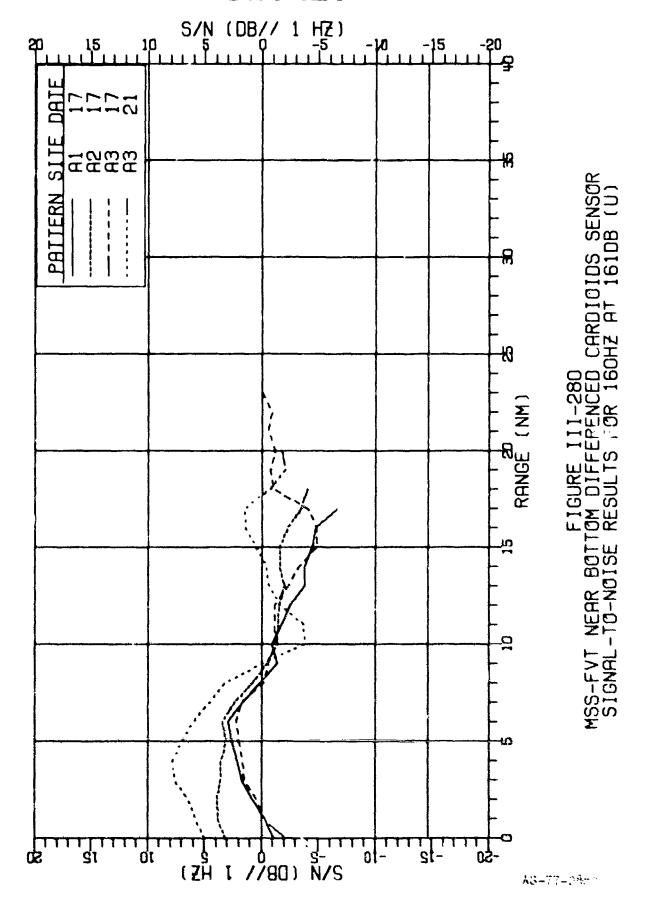
215

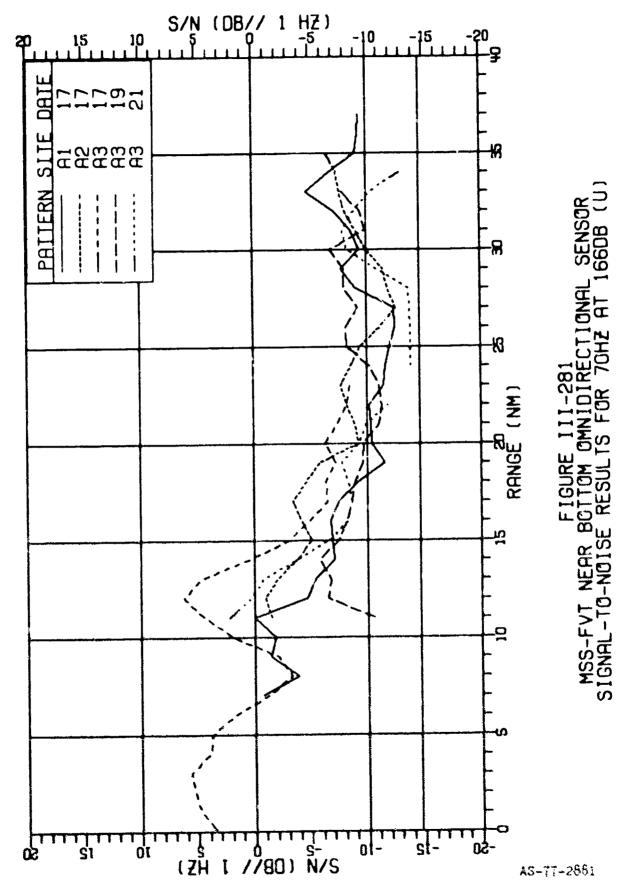


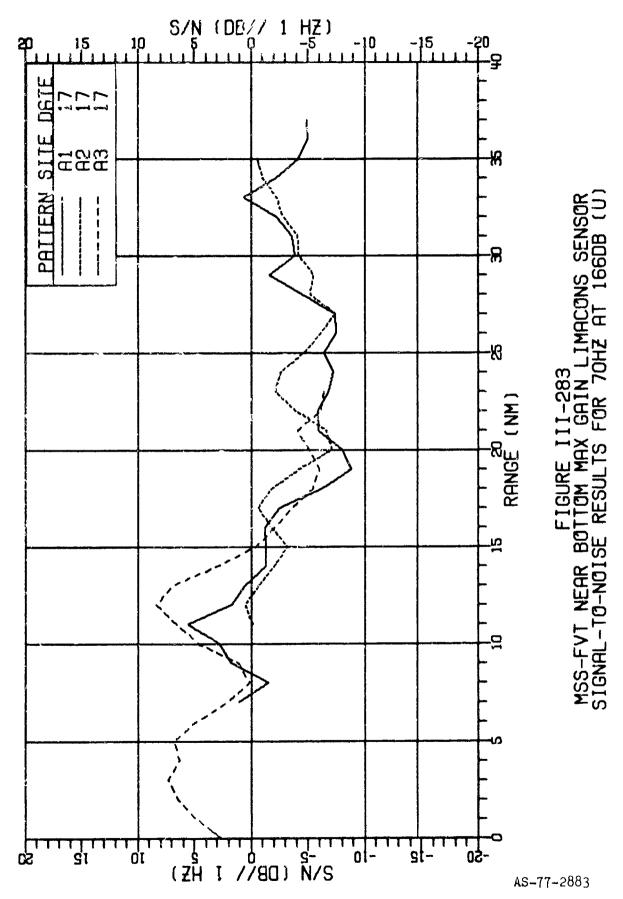


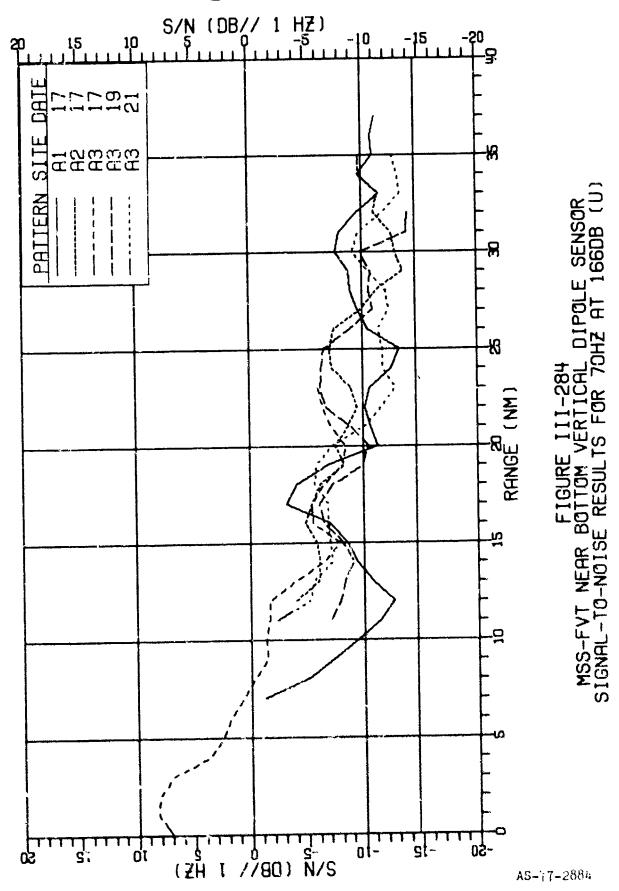
317

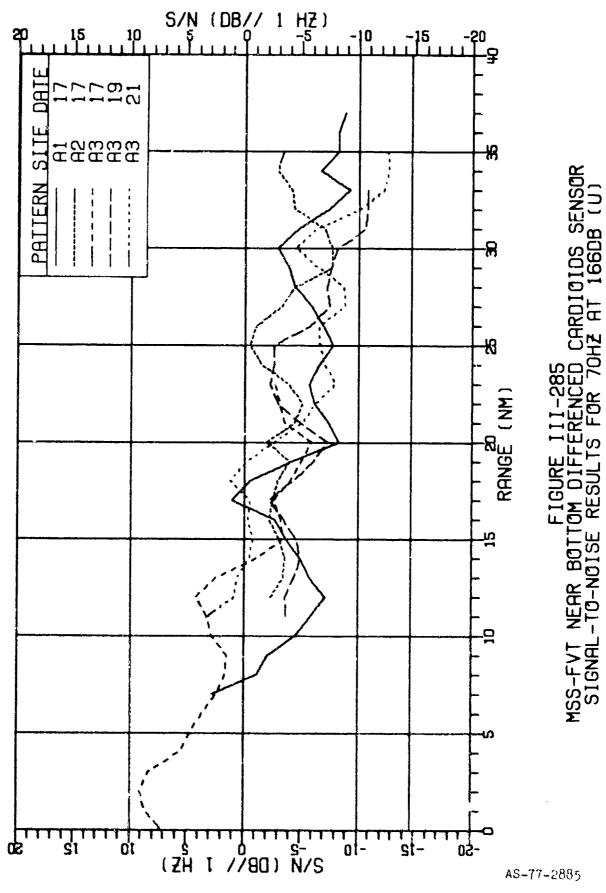












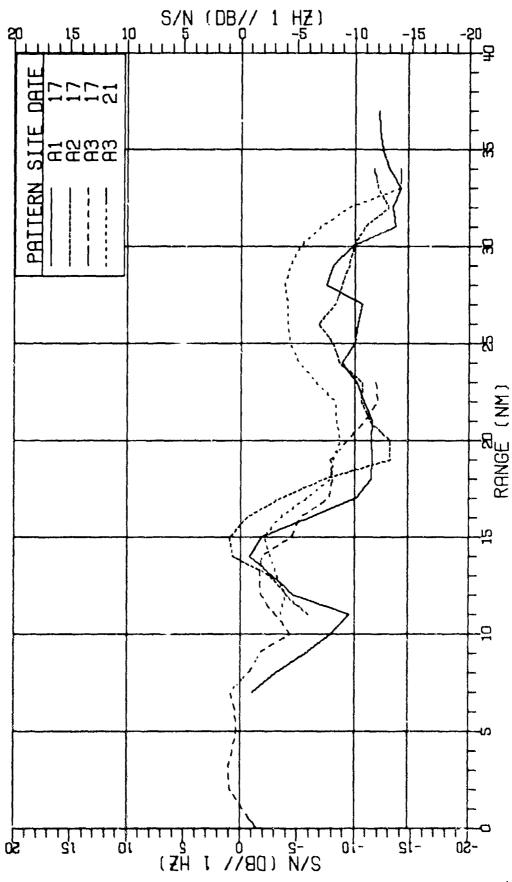
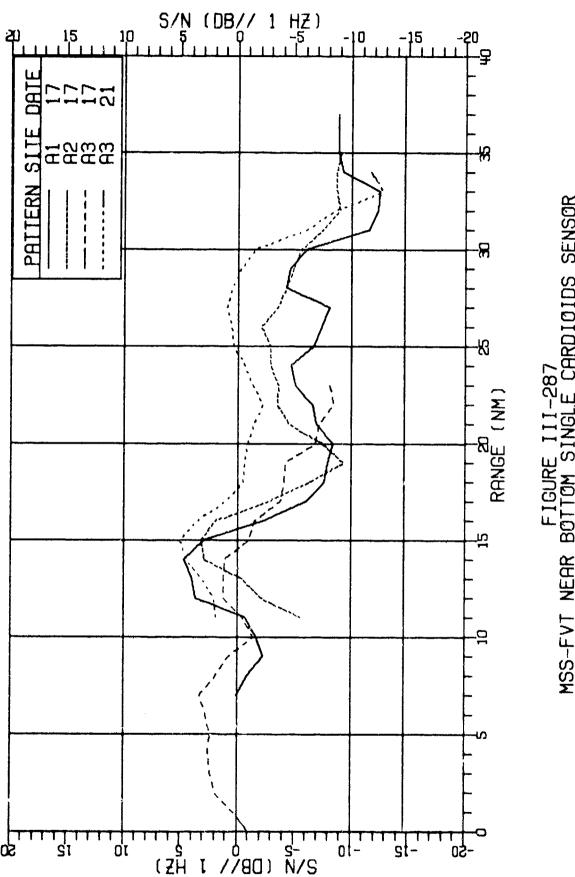


FIGURE III-286 MSS-FVT NEAR BOTTOM OMNIDIRECTIONAL SENSOR SIGNAL-TO-NOISE RESULTS FOR 170HZ AT 156DB (U)

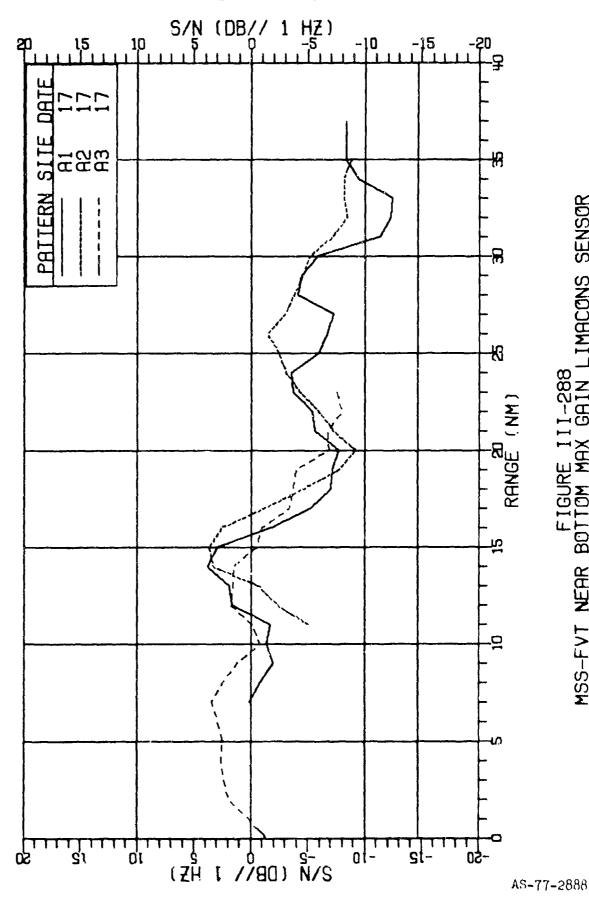
AS-77-2886

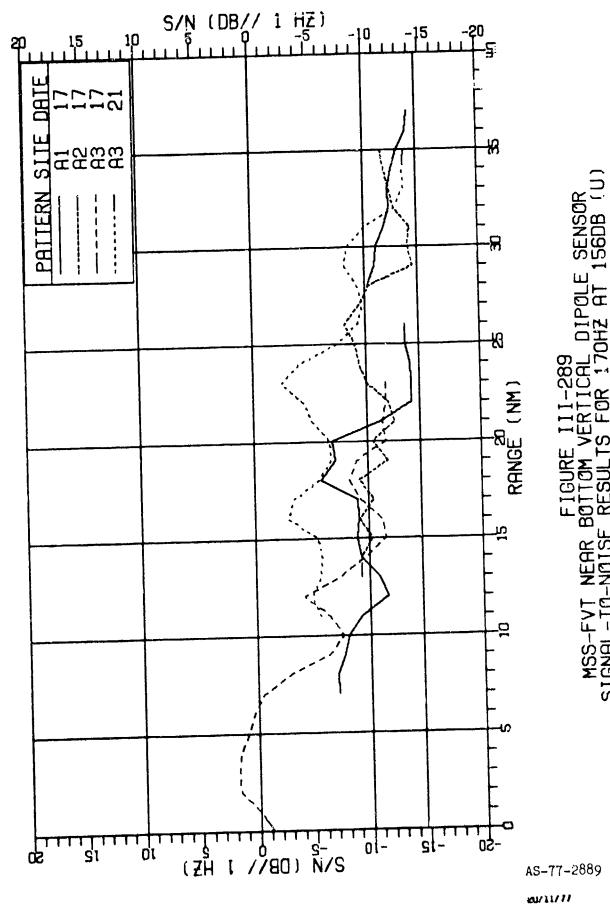


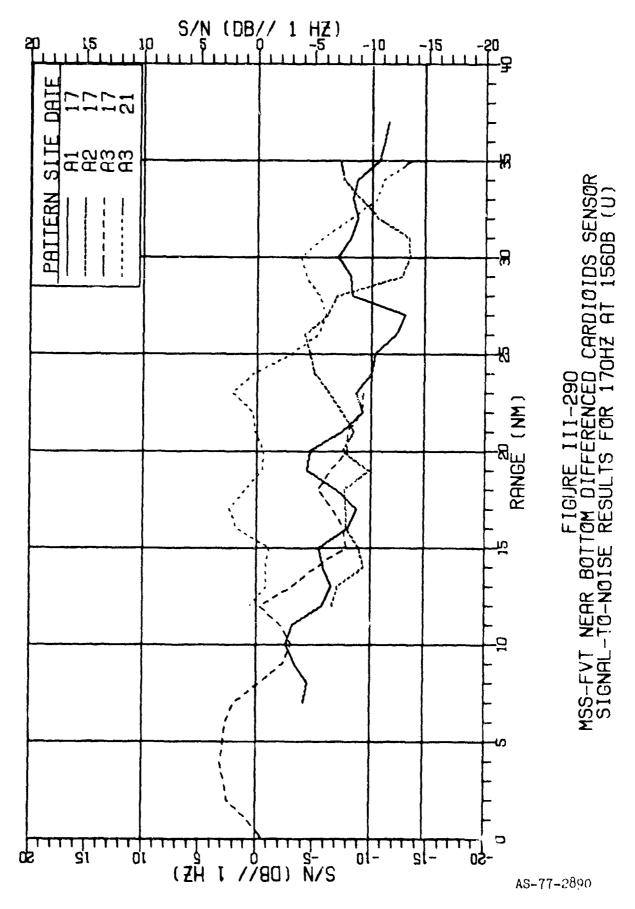
AS-77-2887

SECRET

F/96 4 450



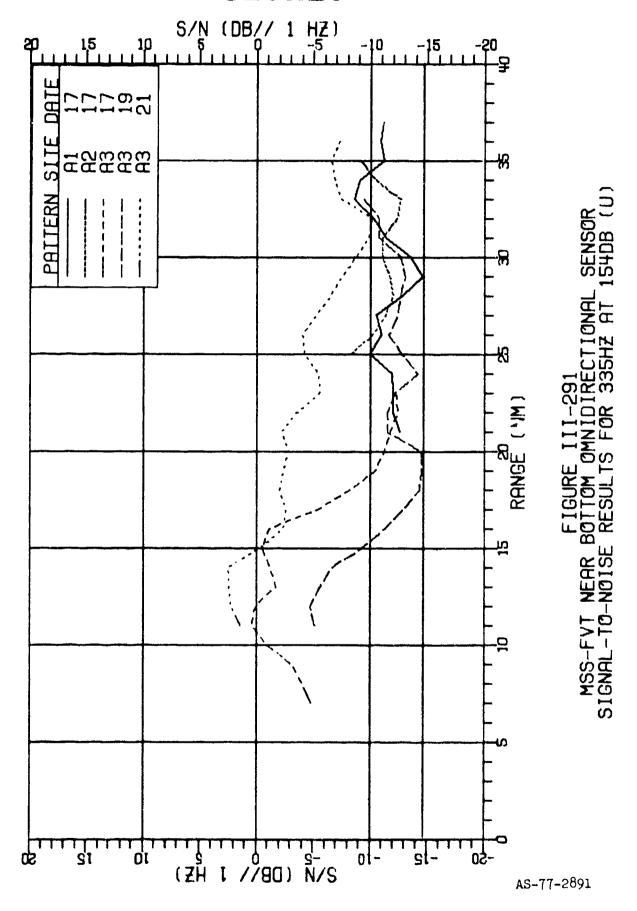




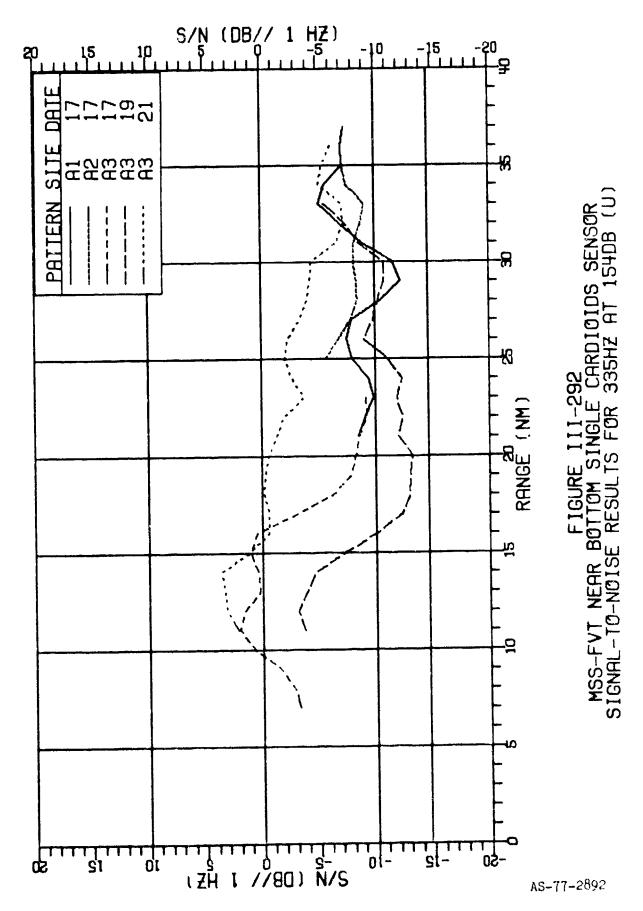
329

SECRET

and a property and the



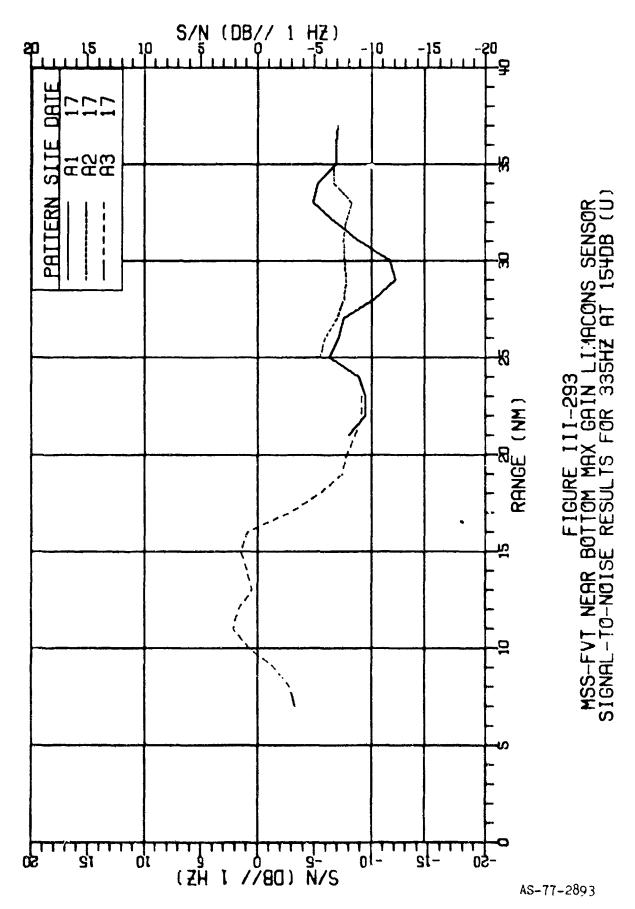
SECRET



331

SECRET

SECRET



332

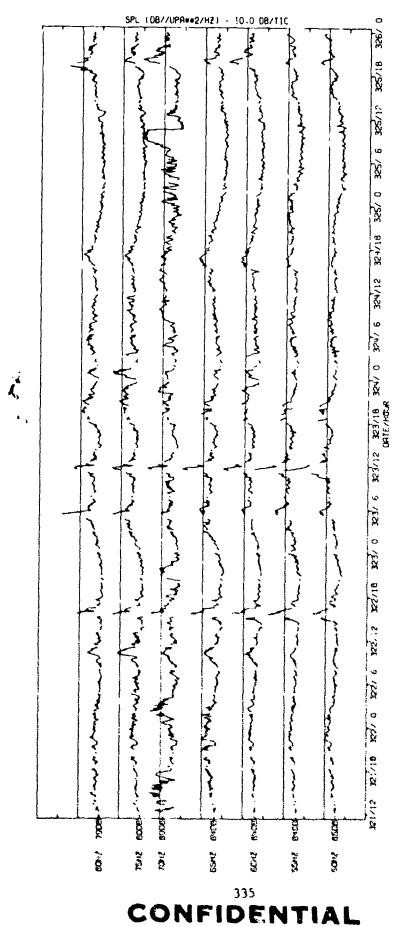
SECRET

UNCLASSIFIED

APPENDIX H

NOISE GAIN TIMESERIES CURVES (U)

(FIGURES III-294 - III-301)



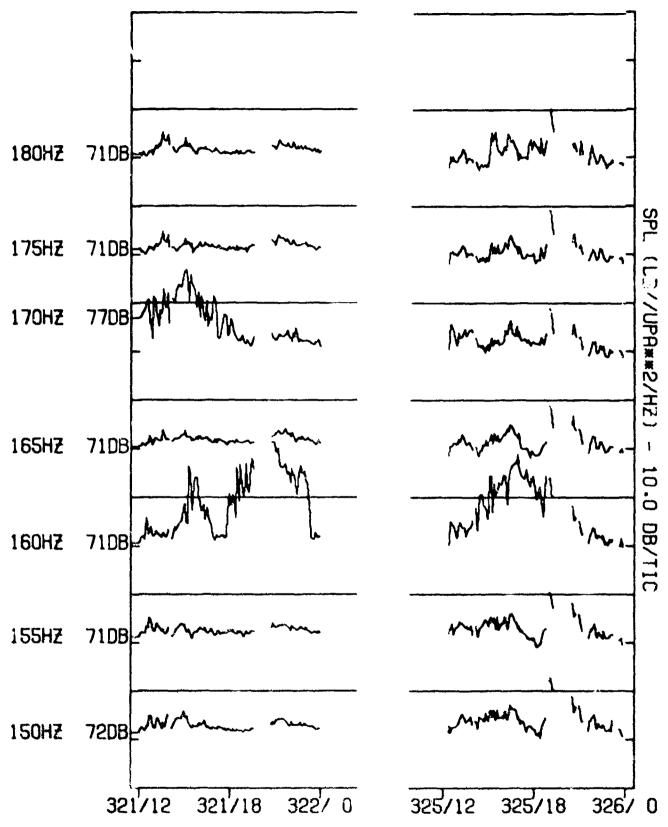
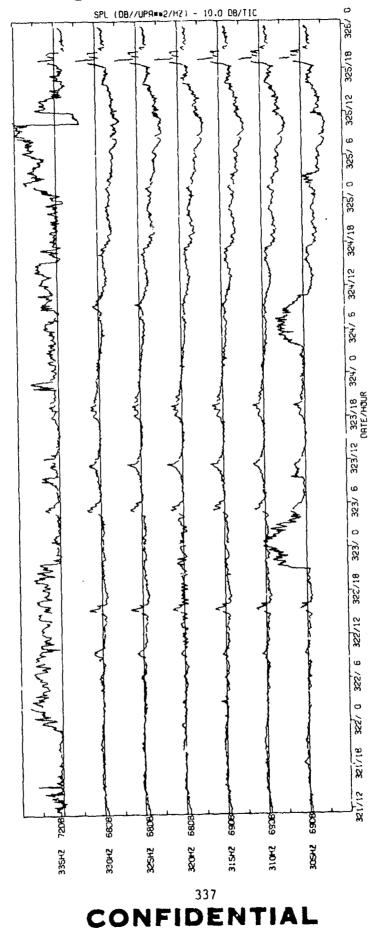


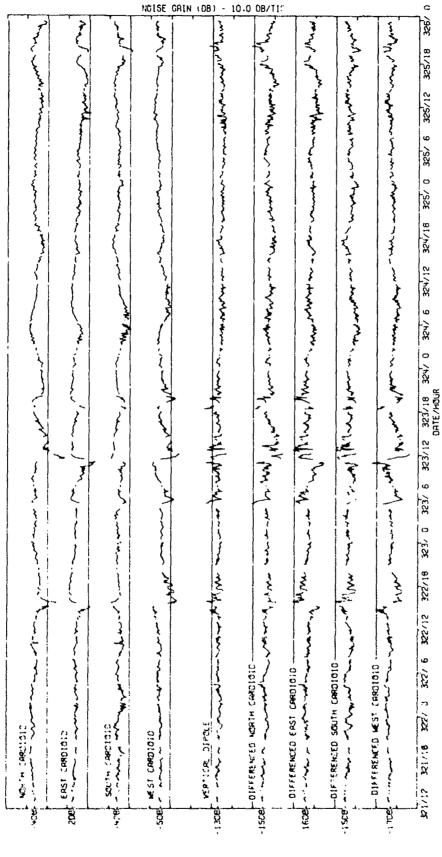
FIGURE III-295

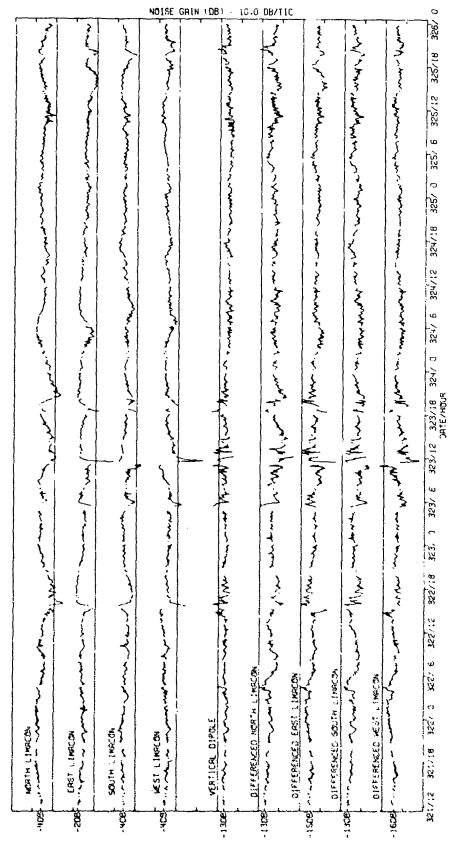
MSS-FVT PHASE II SITE A3 MID FREQUENCY VERNIER

TIME SERIES OF 5 MIN AVERAGED AMBIENT SOUND FIELD LEVELS
THROUGH 1 HZ BANDS OF THE OMNIDIRECTIONAL SENSOR (U)

336







AS-77-3391

SERIES OF FOR 1 TO

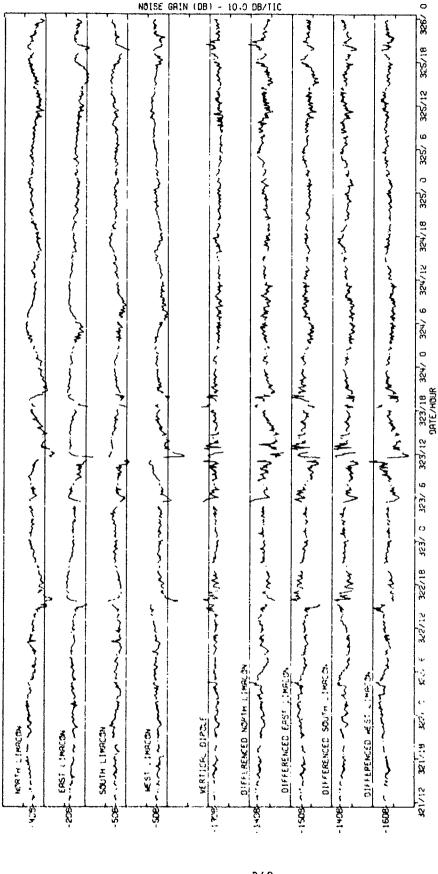


FIGURE III-299
MSS-FVT PHRSE II SITE A3 LOW FREQUENCY VERNIER
IME SERIES OF 5 MIN AVERAGED NOISE GAIN LEVELS
FOR LIMACON (0.50) BEAMS AT 50 HZ (U)

AS-77-3392

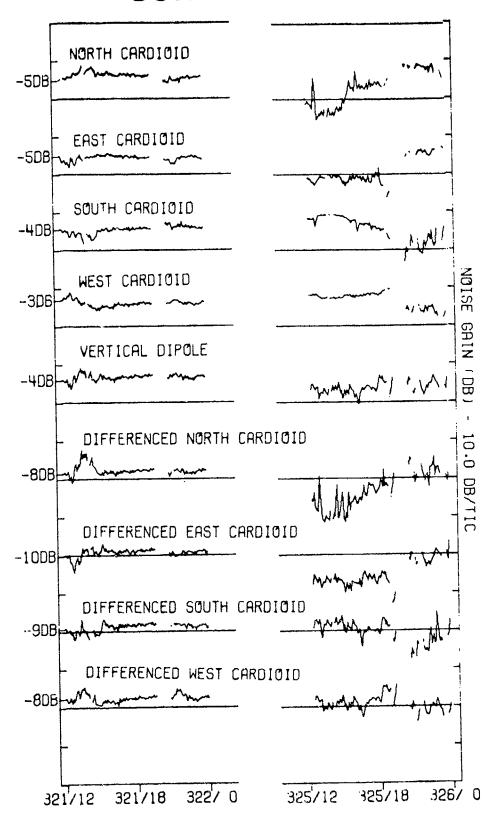


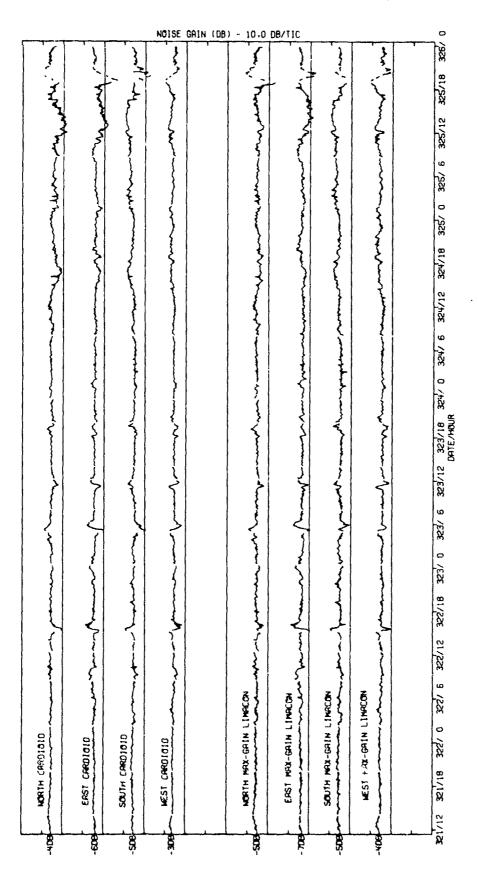
FIGURE III-300

MSS-FVT PHASE II SITE A3 MID FREQUENCY VERNIER

TIME SERIES OF 5 MIN AVERAGED NOISE GAIN LEVELS

FOR CARDIOID BEAMS AT 150 HZ (U)

AS-77-3393



FREQUENCY NOISE GRIN BEAMS AT 3 FIGURE III-301 II SITE A3 HIGH F 5 MIN AVERAGED P LIMACON (0.33)

UNCLASSIFIED

APPENDIX I

CLUTTER TIMESERIES CURVES (U)

(FIGURES III-302 - III-312)

(The reverse of this page is blank.)
UNCLASSIFIED

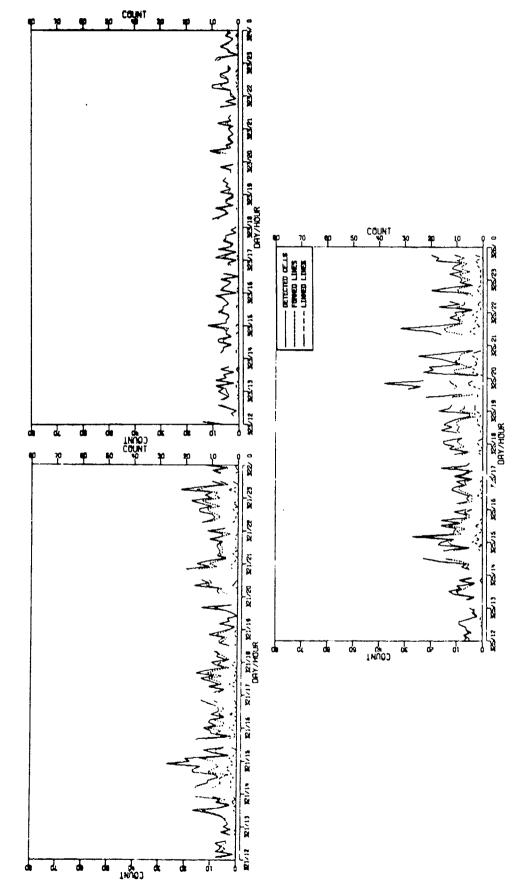
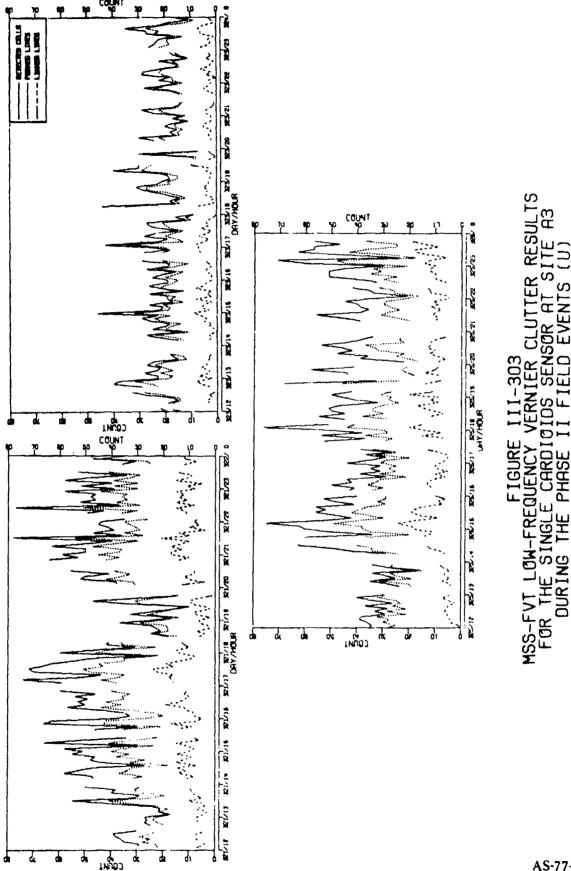
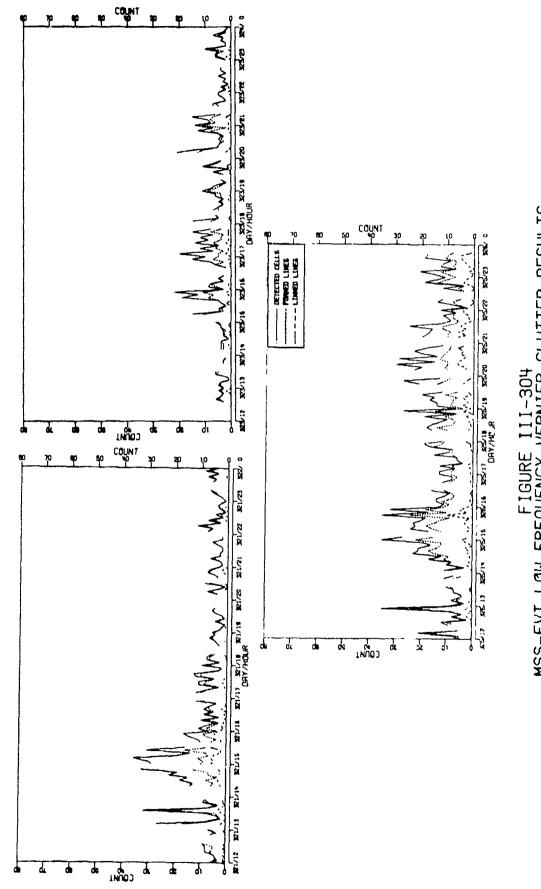


FIGURE III-302 MSS-FVT LOW-FREQUENCY VERNIER CLUTTER RESULTS FOR THE OMNIDIRECTIONAL SENSOR AT SITE A3 DURING THE PHASE II FIELD EVENTS (U)





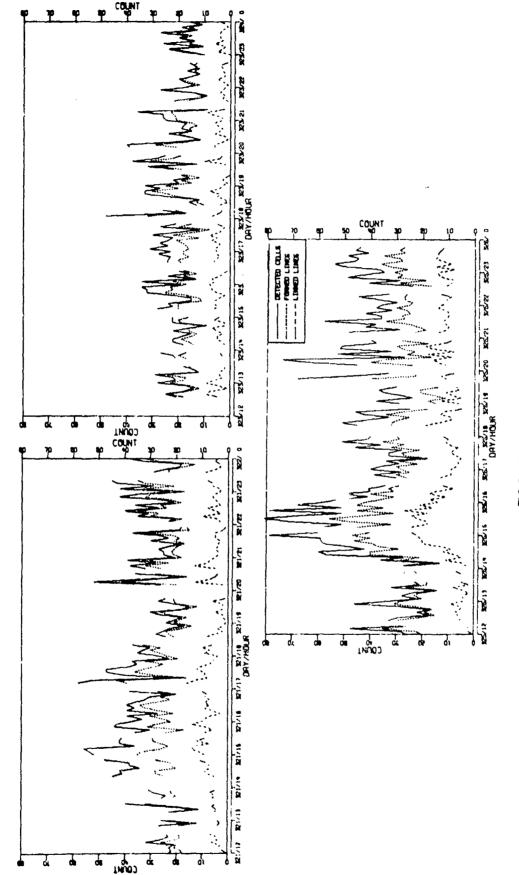
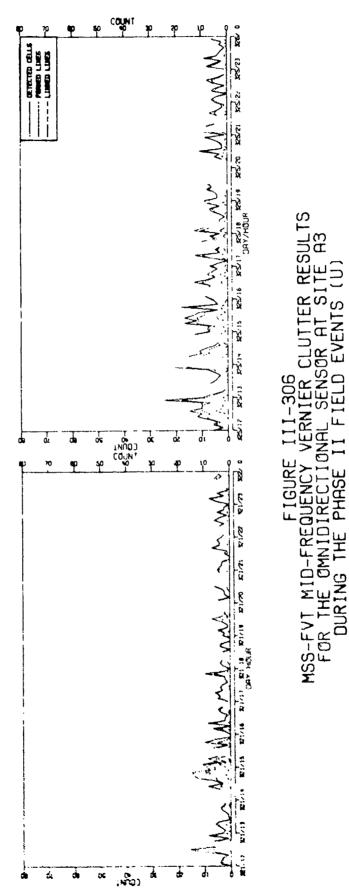
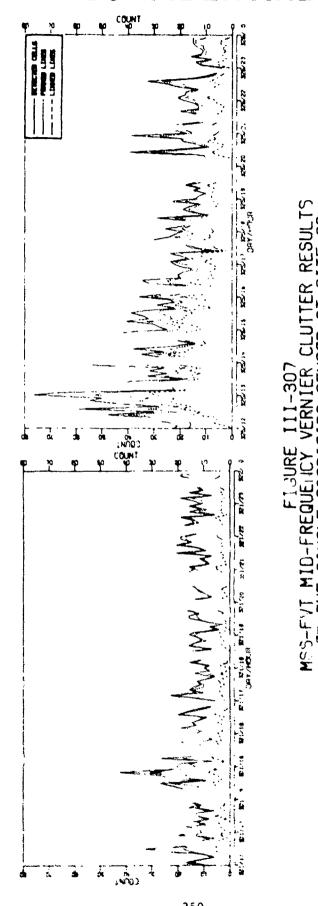
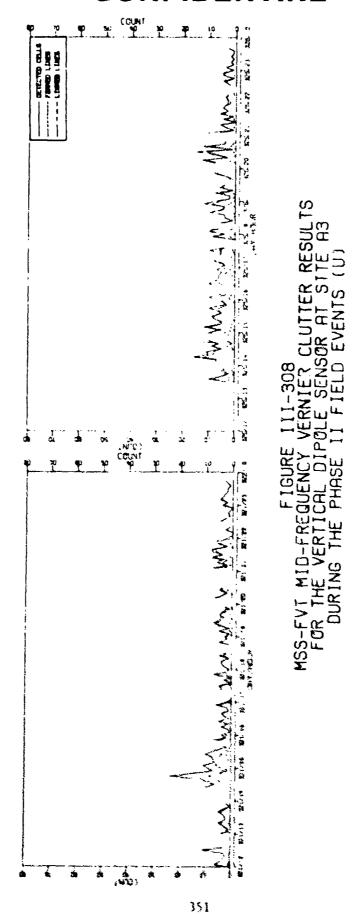


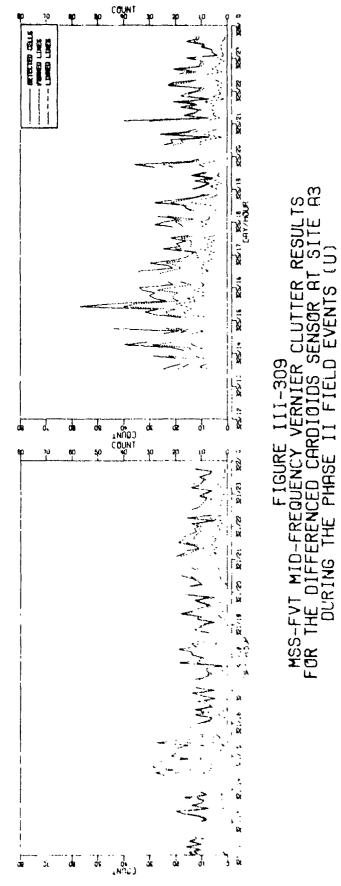
FIGURE III-305
MSS-FVT LOW-FREQUENCY VERNIER CLUTTER RESULTS
FOR THE DIFFERENCED CARDIGIDS SENSOR AT SITE A3
DURING THE PHASE II FIELD EVENTS (11)

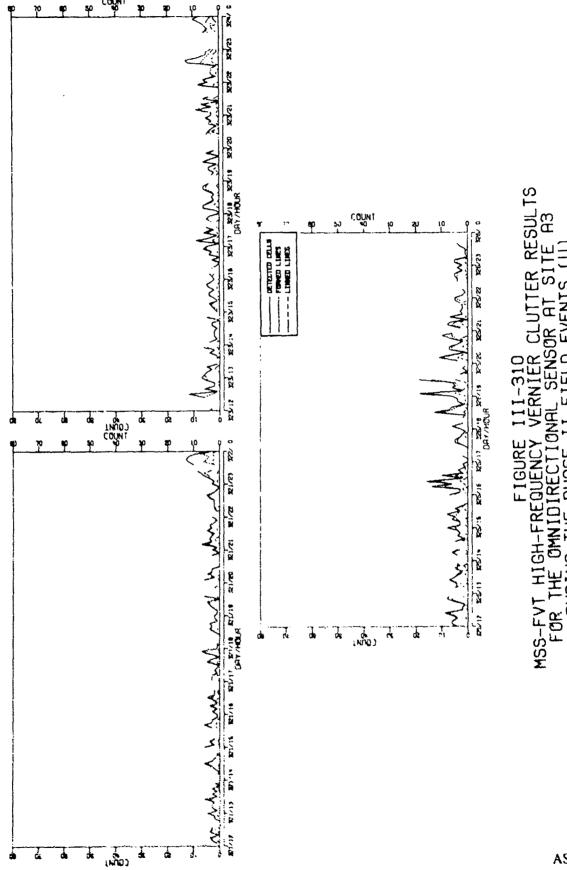


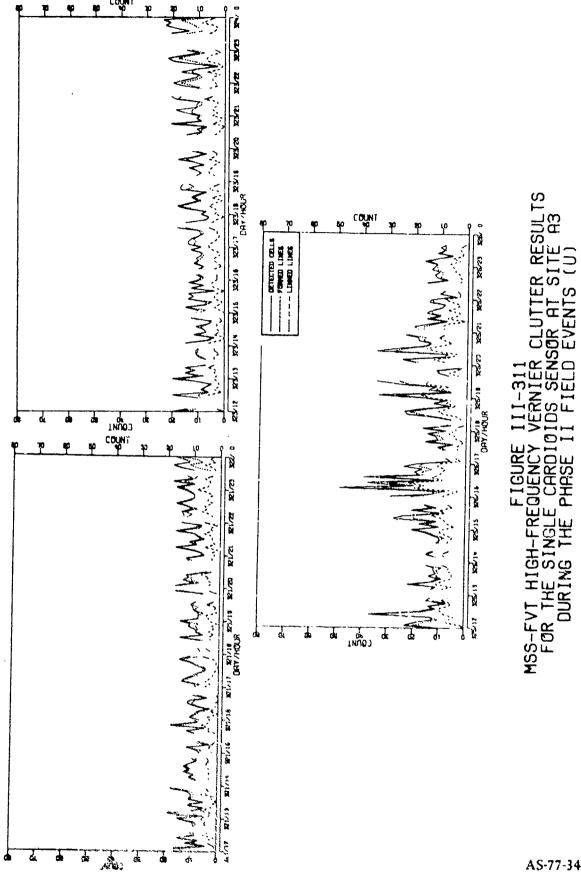


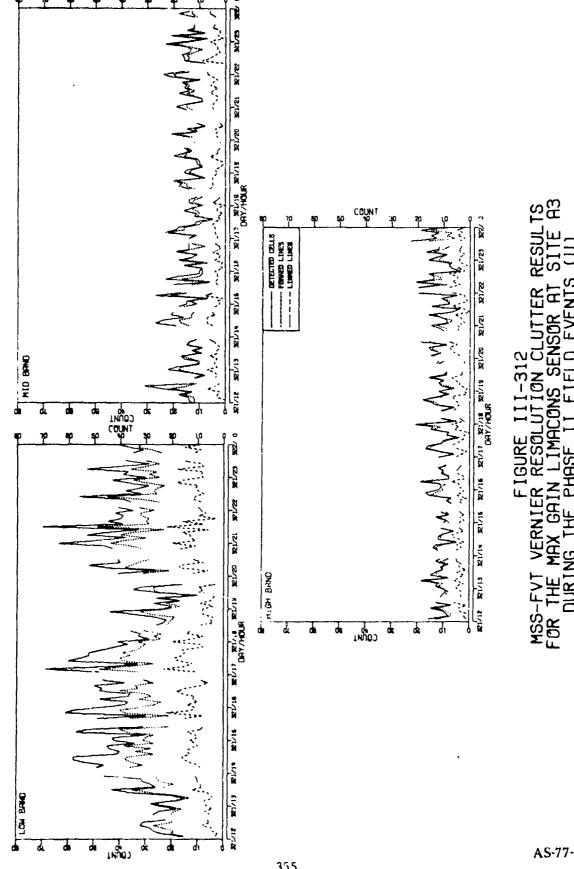


AS-77-3401









AS-77-3405

(The reverse of this page is blank.) CONFIDENTIAL

UNCLASSIFIED

APPENDIX J AMBIENT SOUND FIELD 3D PLOTS

(U) This appendix contains plots of a 3-dimensional representation of the ambient sound field. These plots were generated from vernier resolution calibrated covariance matrices. Only omnidirectional and vertical dipole data were plotted. Such displays are intended to aid the analyst in obtaining an overview of the available data base, in identifying artifacts, and by serving as a guide to later data selection and processing. Each plot covers a 12 h time interval. Each trace represents an intensity average over a 10 min time interval. The data identifier is described below.

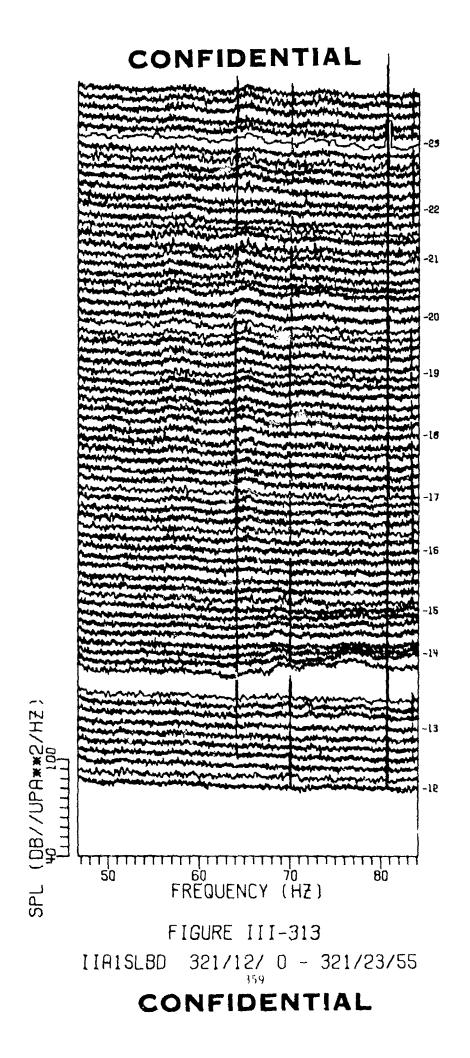
or High Band (HBD) Data

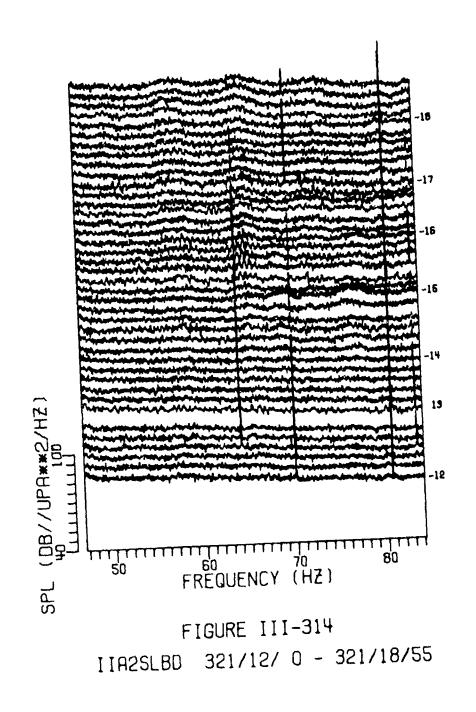
B +Low Band (LBD), Midband (MBD),

O +Single (S) or Differenced (D) Array

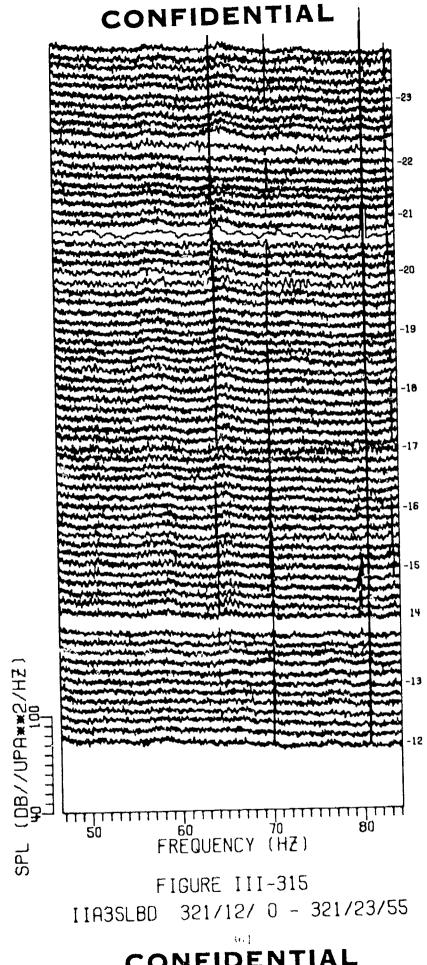
A +ACODAC Site Al

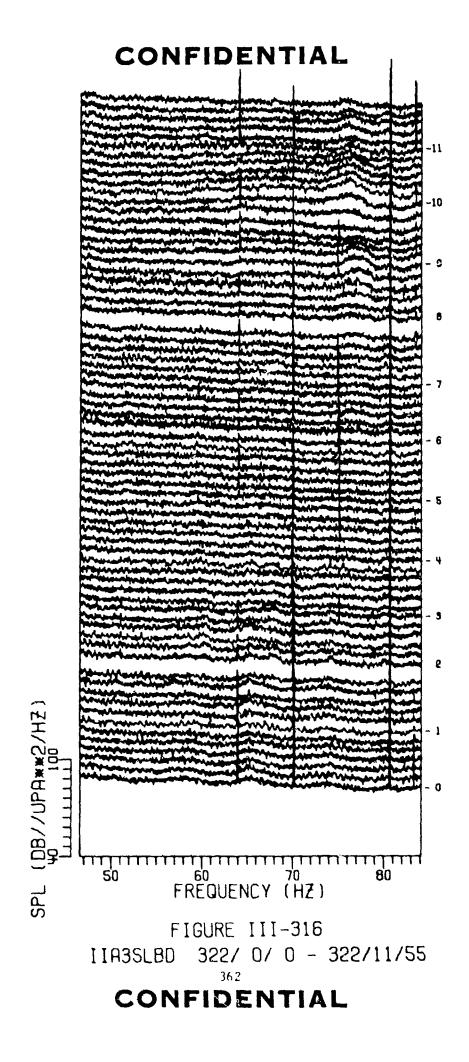
H +Phase II

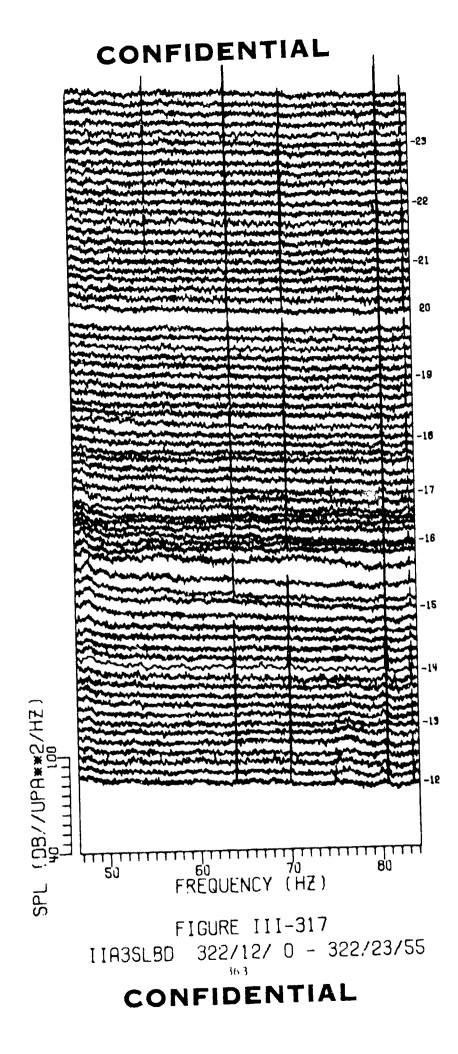


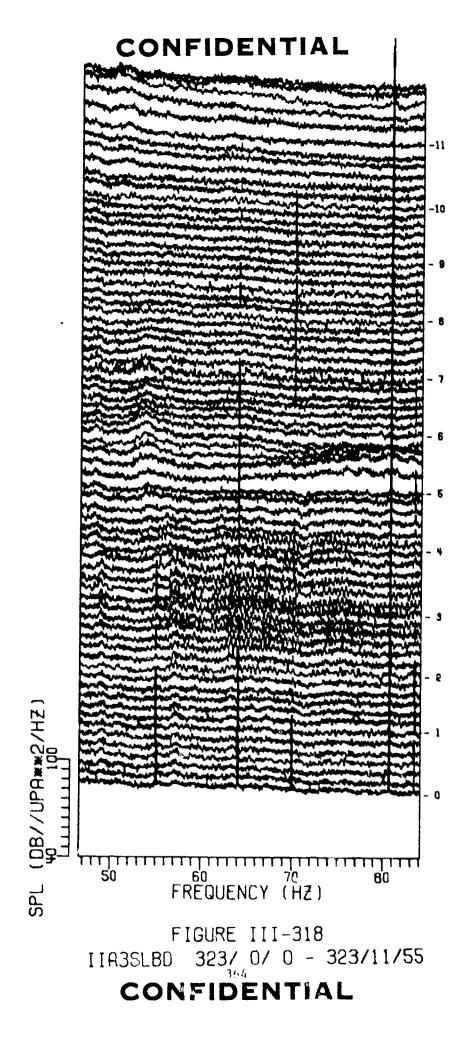


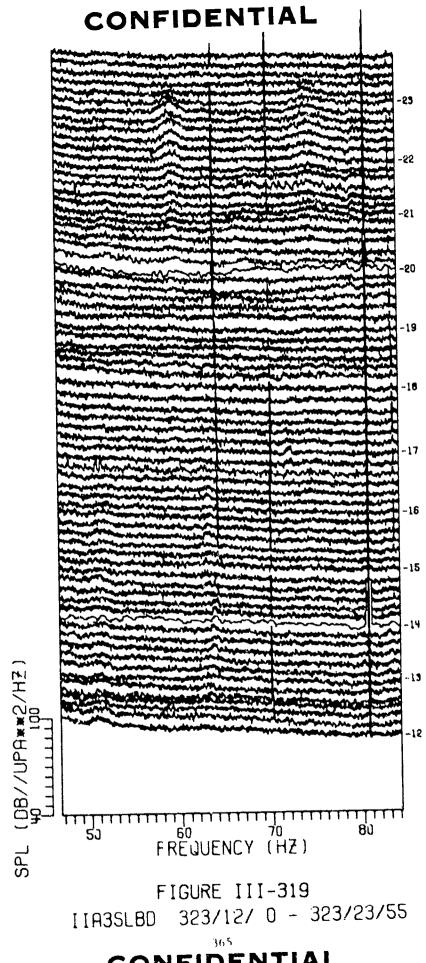
CONFIDENTIAL

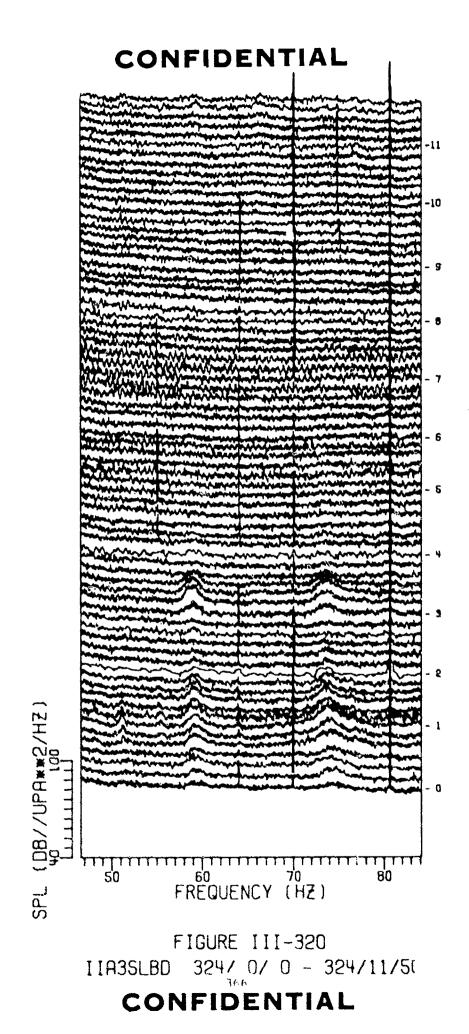


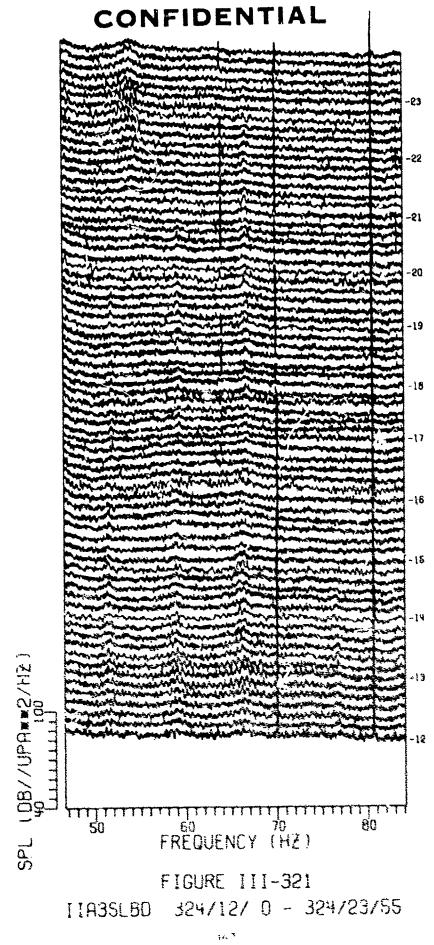


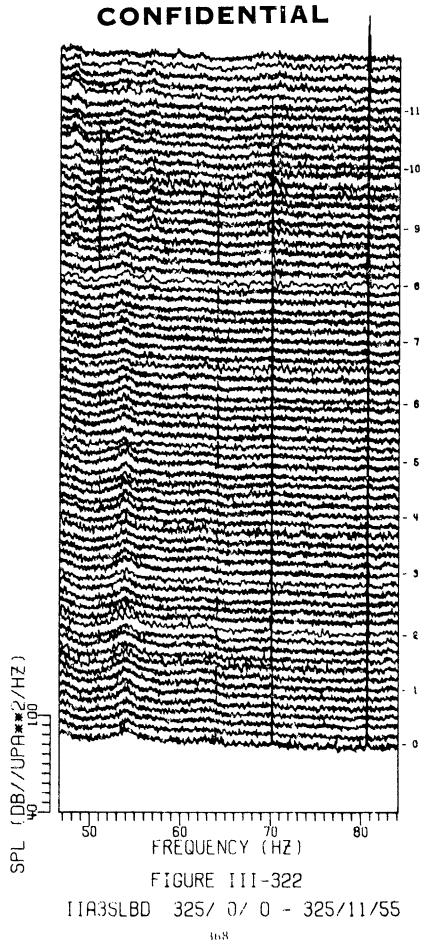


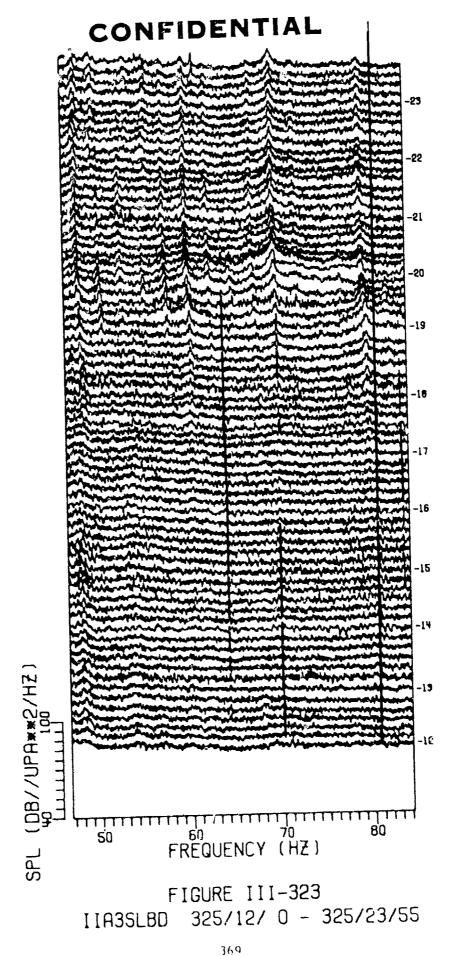


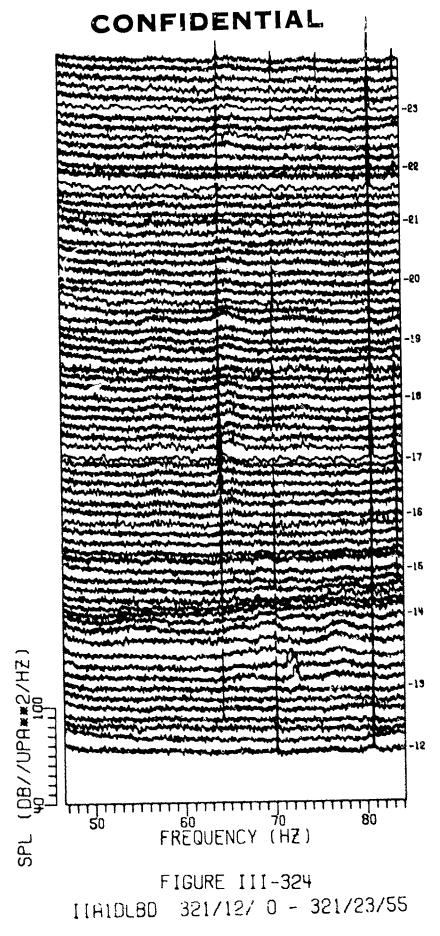




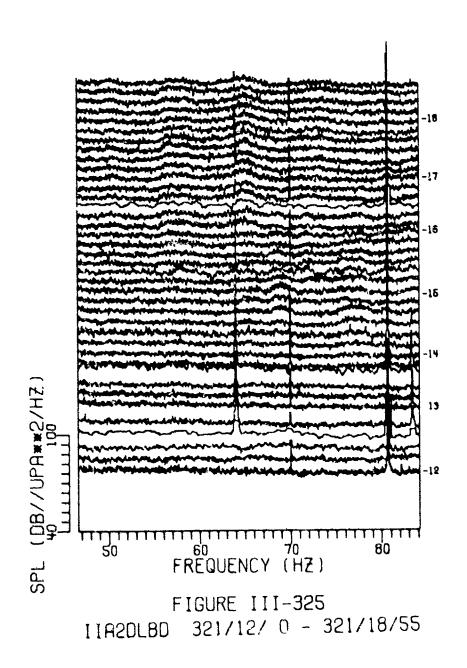








370



CONFIDENTIAL

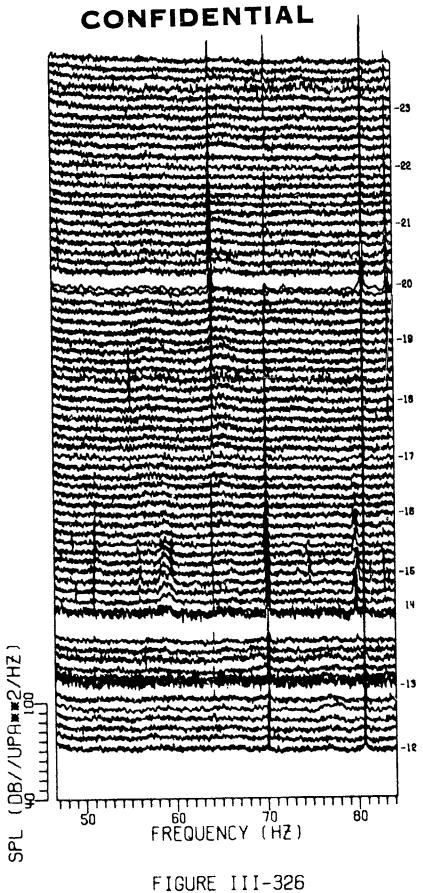


FIGURE III-326 IIA3DLBD 321/12/ 0 - 321/23/55

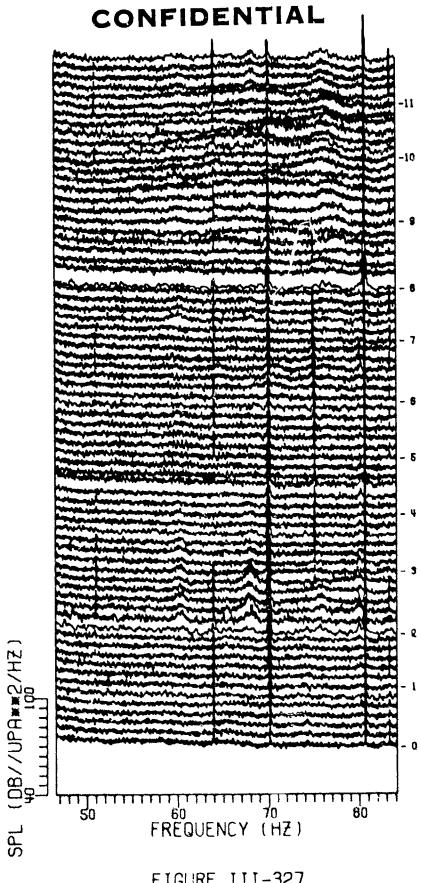
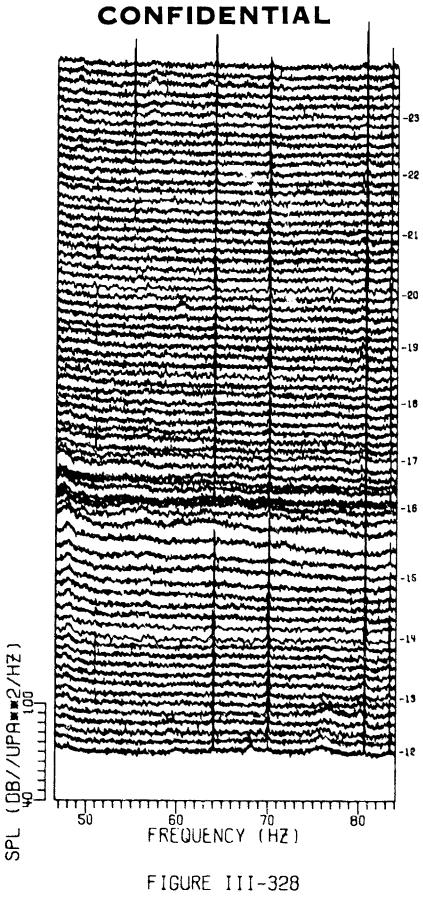
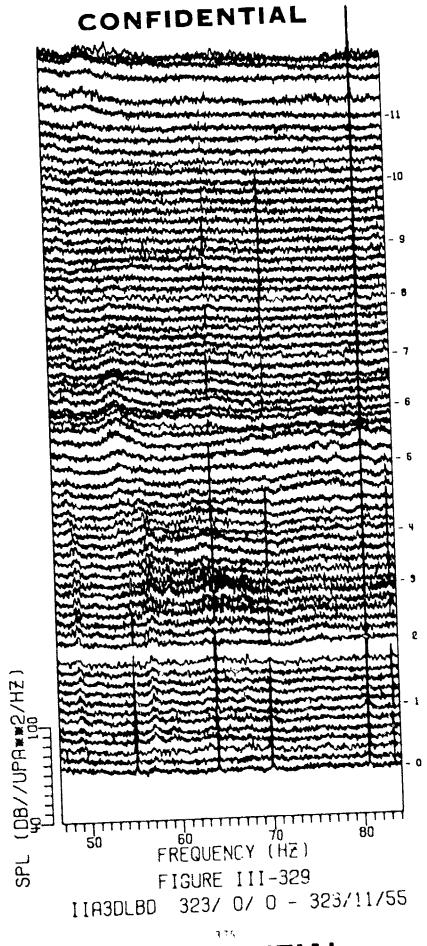
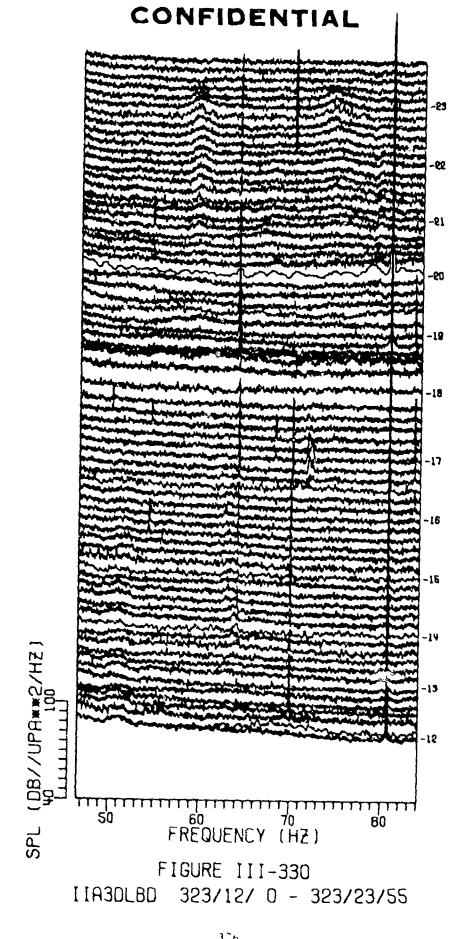


FIGURE III-327 IIA3DLBD 322/ 0/ 0 - 322/11/55



I1930LBD 322/12/ 0 - 322/23/55





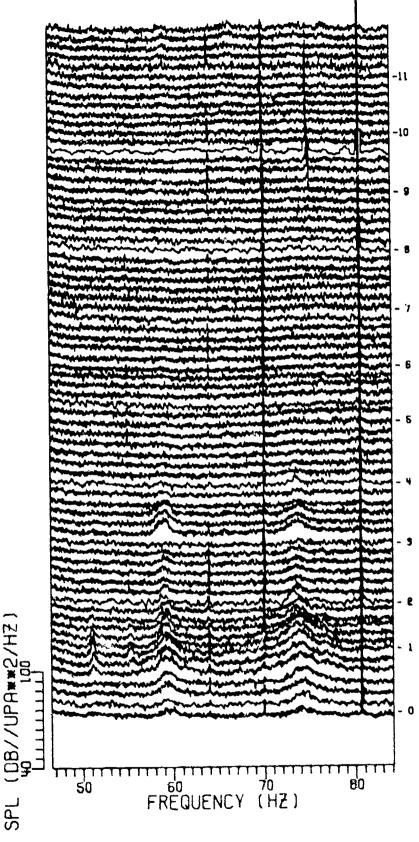
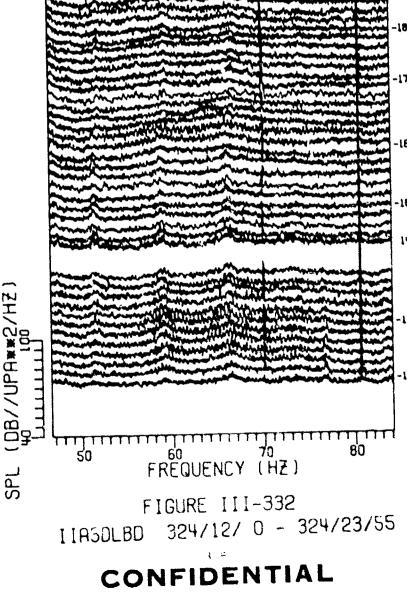
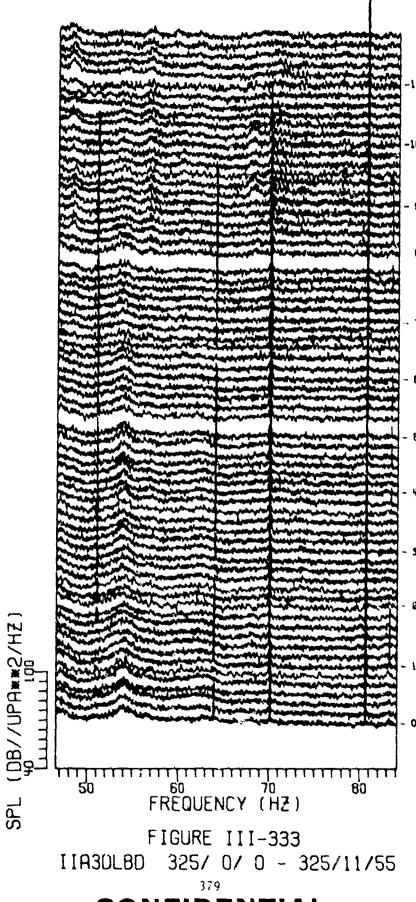
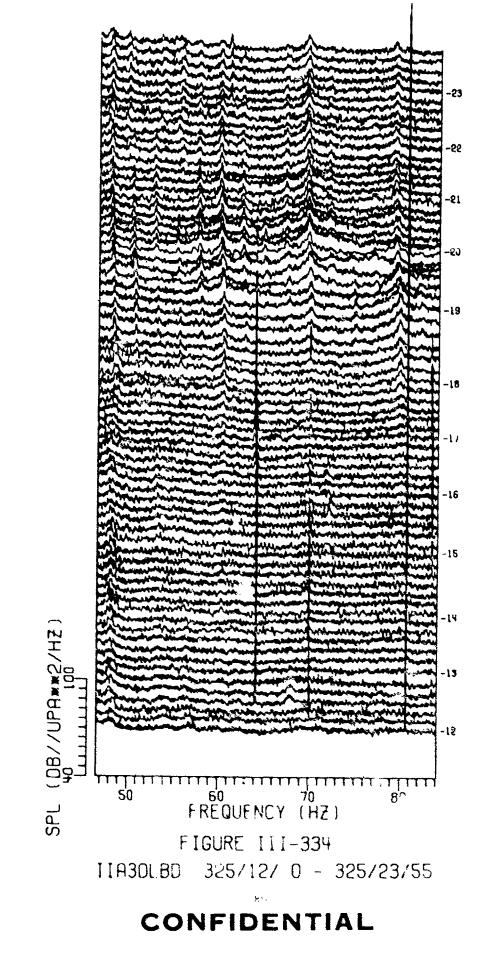
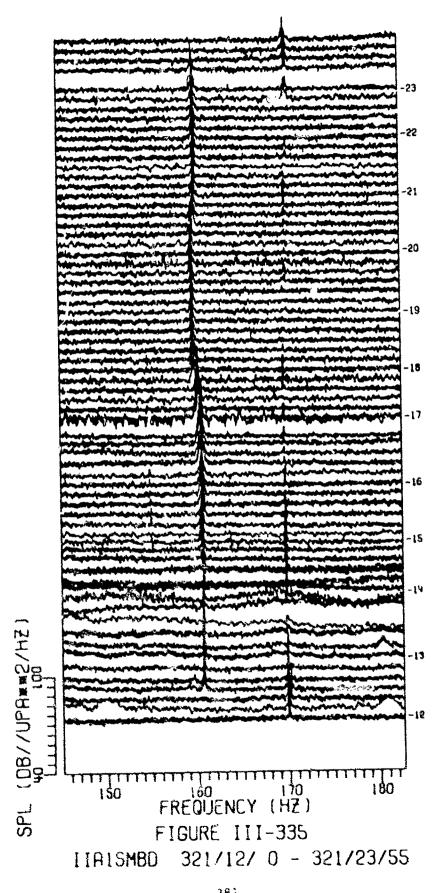


FIGURE III-331 IIA3DLBD 324/0/0 - 324/11/55









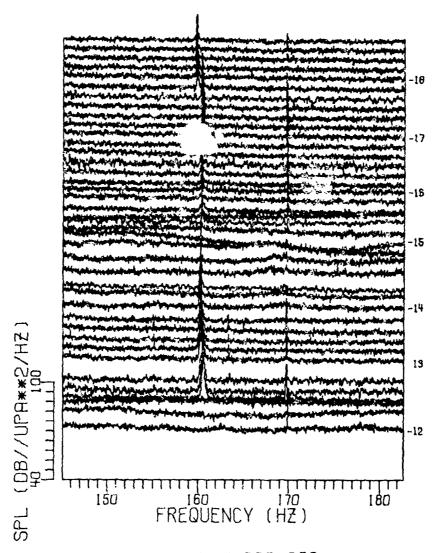
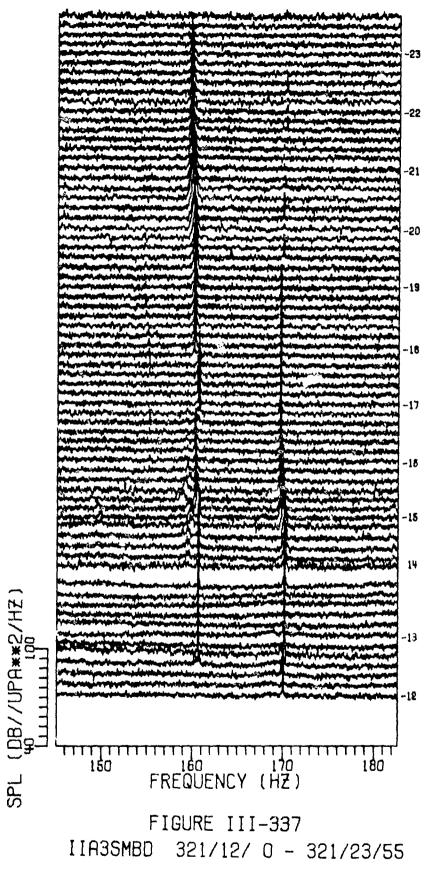
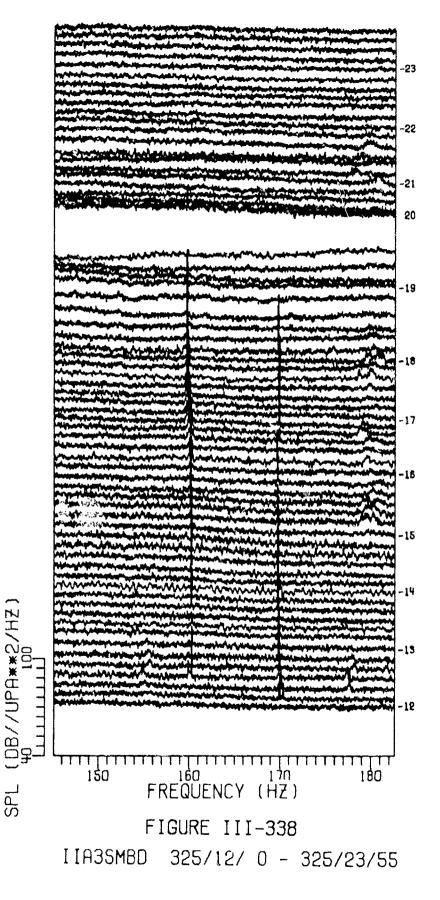


FIGURE III-336 IIA2SMBD 321/12/ 0 - 321/18/55

382



383



384

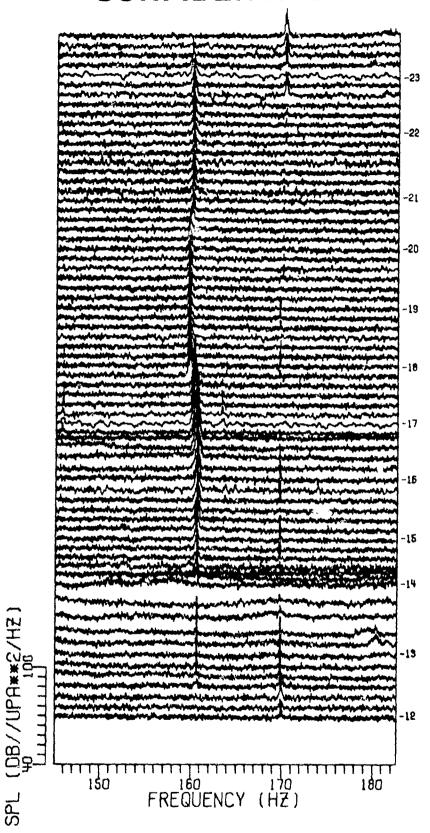


FIGURE III-339 IIA1DMBD 321/12/ 0 - 321/23/55

385

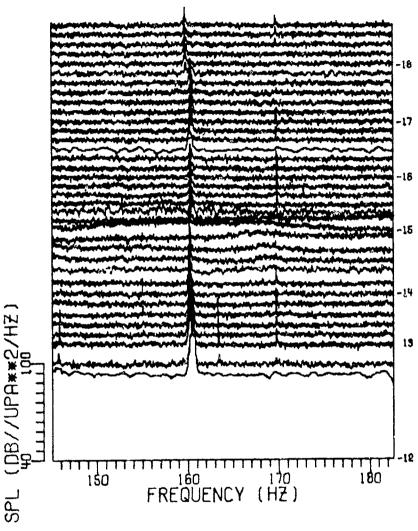


FIGURE III-340 IIA2DMBD 321/12/ 0 - 321/18/55

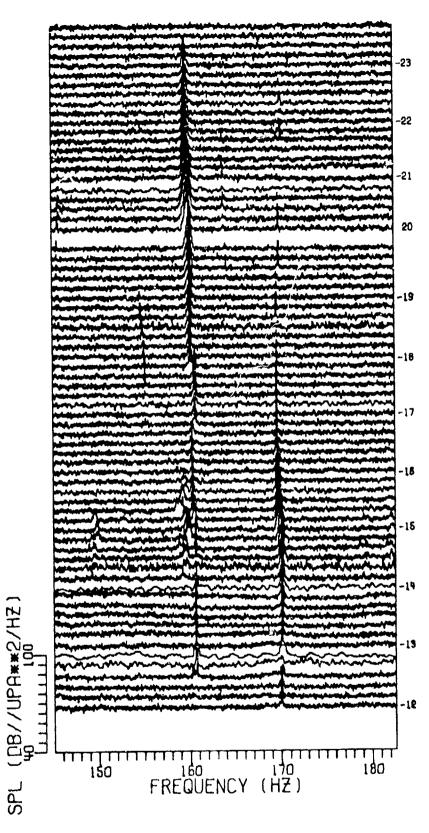
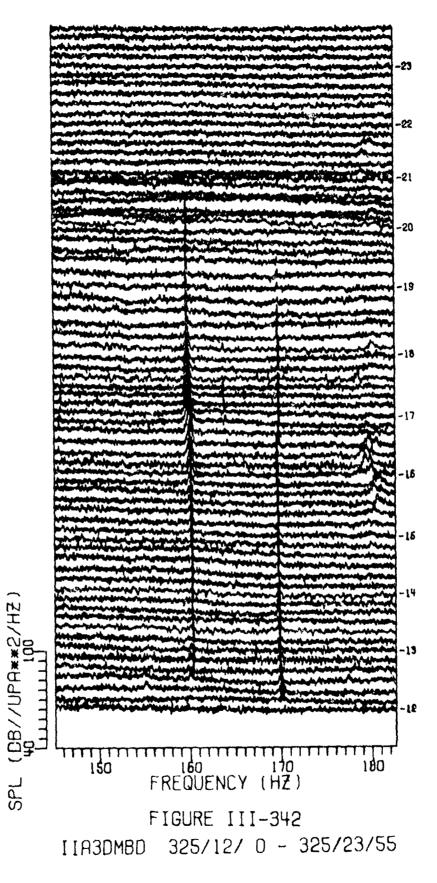


FIGURE III-341 IIA3DMBD 321/12/ 0 - 321/23/55



388

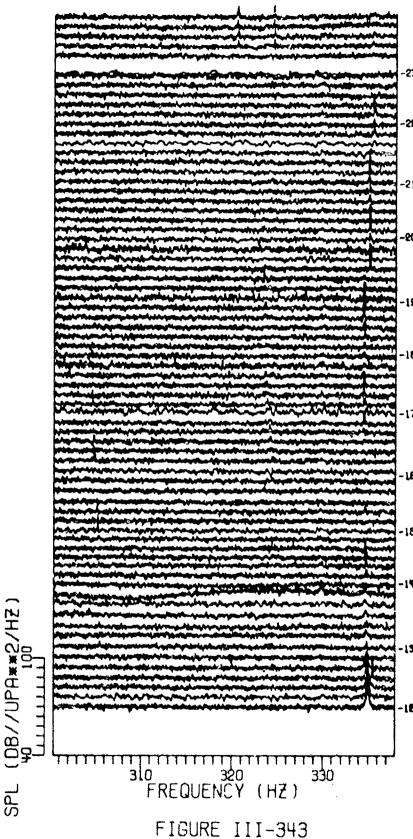
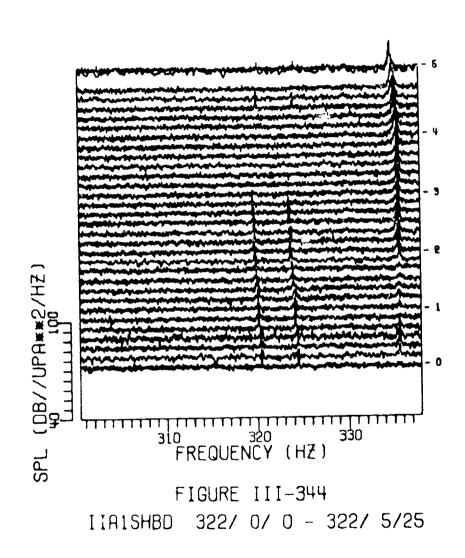


FIGURE III-343 IIA1SHBD 321/12/ 0 - 321/23/55

189



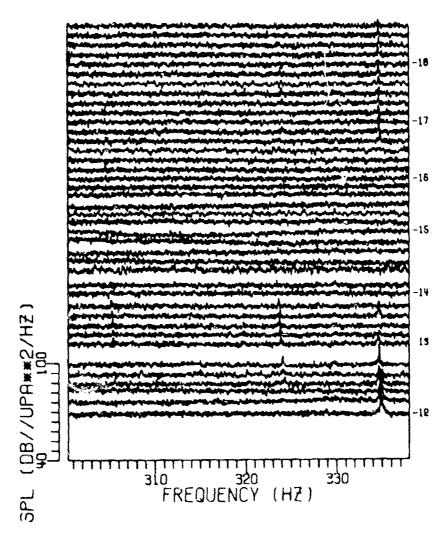
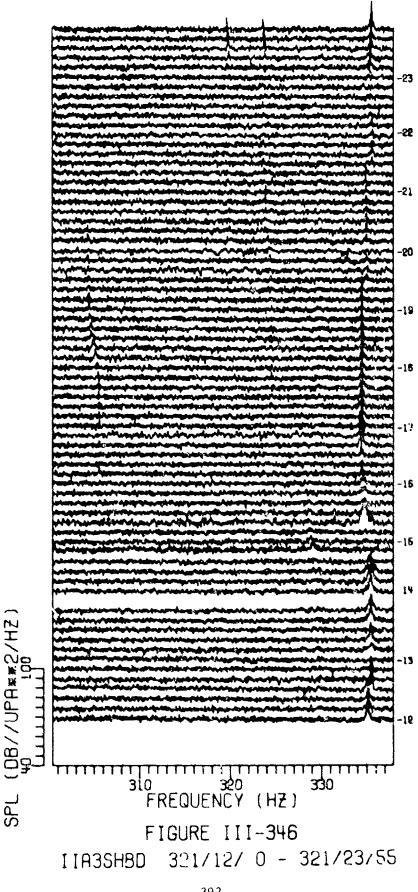
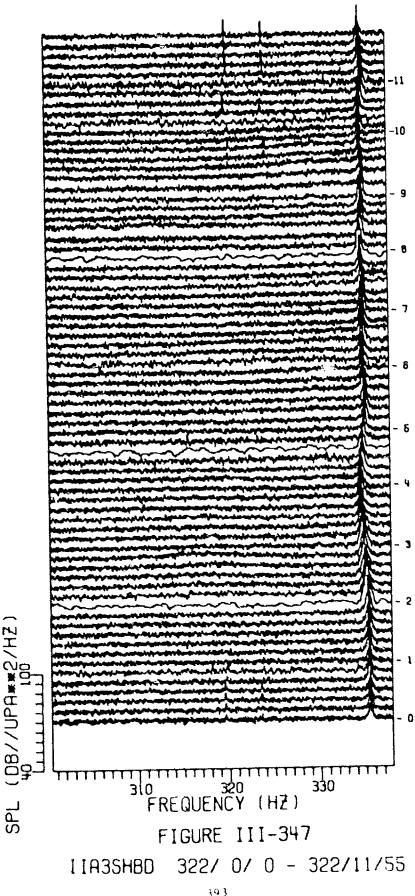
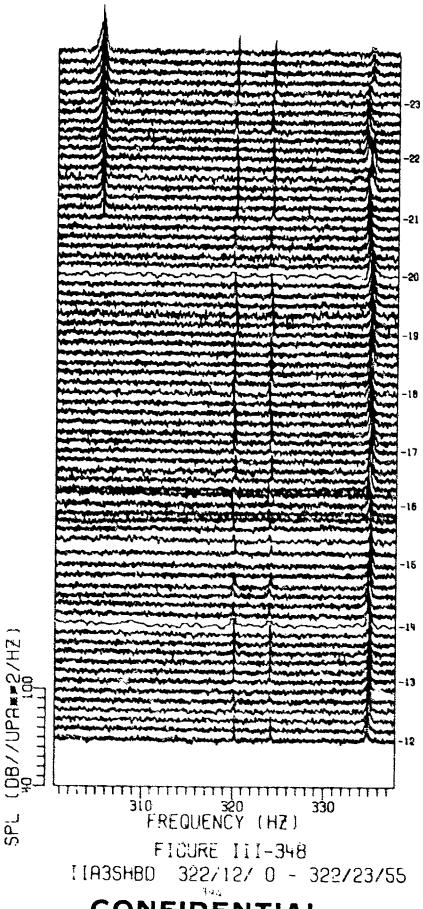


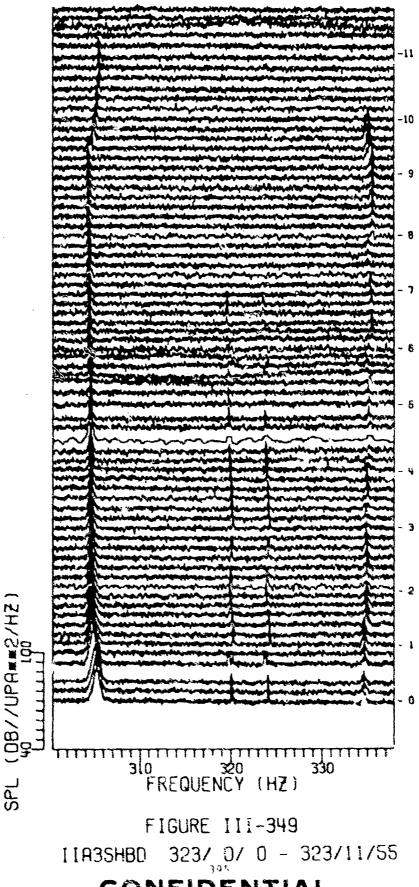
FIGURE III-345 IIA2SHBD 321/12/ 0 - 321/18/55

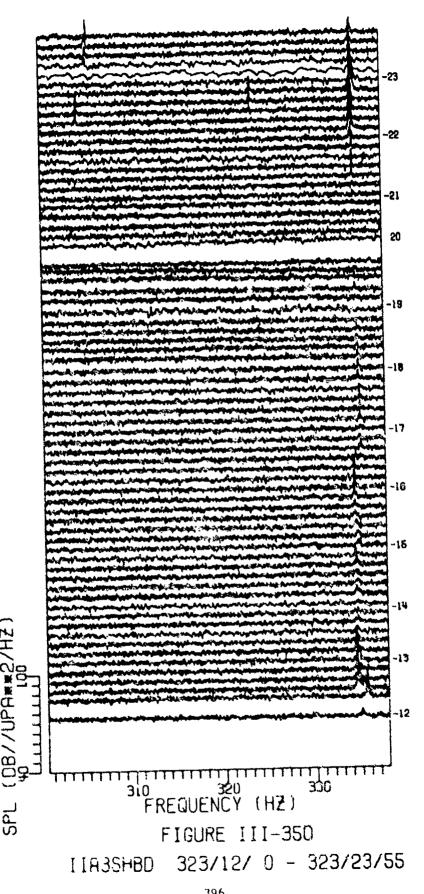


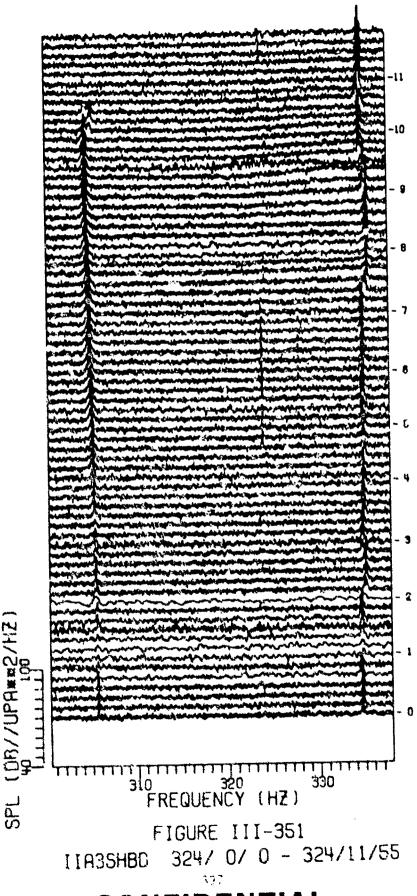
392

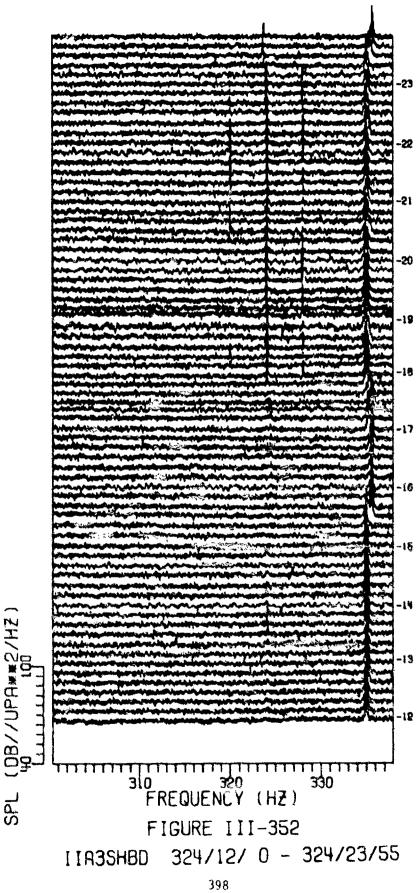


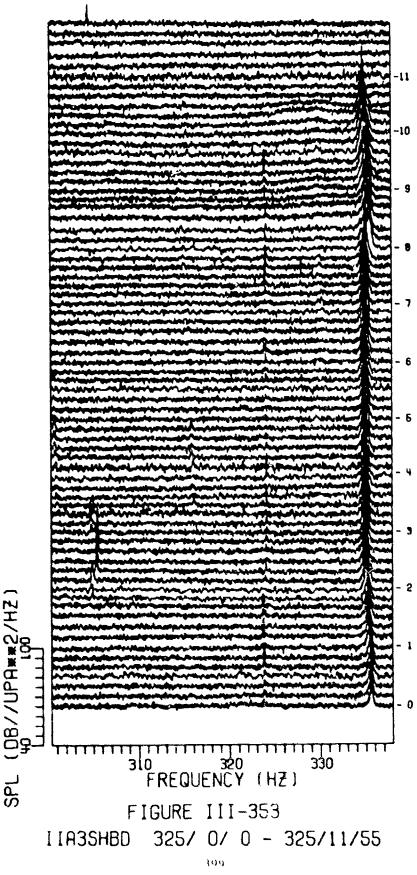


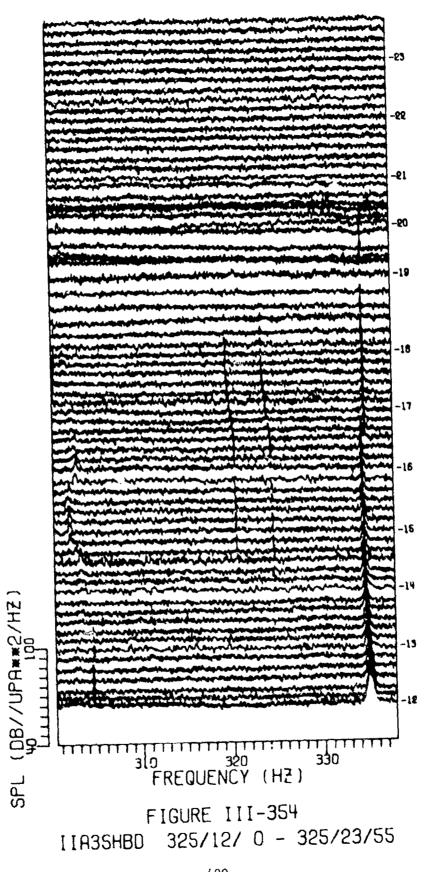












400

SECRET UNCLASSIFIED

(This page is unclassified)

31 December 1978

DISTRIBUTION LIST FOR ARI.-TR-78-3

FINAL REPORT UNDER CONTRACT NOO039-77-C-0003, (ITEMS 0003 AND 0004) SECRET

Copy No.

```
Commander
       Naval Electronic Systems Command
       Department of the Navy
       Washington, DC 20360
       Attn: PME 124
 1
              PME 124-30
              PME 124-40
              PME 124-60
              PME 124TA
              ELEX 320
 7
       Office of Assistant Secretary of the Navy
       (RE&S) Room 5E813, Pentagon
       Washington, DC 20360
       Attn: Mr. G. Cann
       Chief of Naval Operations
       Department of the Navy
       Washington, DC 20350
 8
       Attn: OP-095
 9
              OP-951F
10
              OP-951F1
11
              OP-981
       Commander
       Naval Air Development Center
       Department of the Navi
       Warminster, PA 18974
12
       Attn: Code 3091
              Code 303
13
14
       Commander
       Naval Air Systems Command
       Department of the Navy
       Washington, DC 20360
```

Attn: Code PMA-264A

SECRET

SECRET

UNCLASSIFIED

(This page is unclassified)

Dist. List for ARL-TR-78-3 under Contract N00039-77-C-0003, Items 0003 and 0004 (Cont'd)

Copy No.

- 15 Commanding Officer
 Naval Intelligence Support Center
 4301 Suitland Road
 Washington, DC 20390
 Attn: Code 222
- 16 Project Manager
 Anti-Submarine Warfare Systems Project Office
 Department of the Navy
 Washington, DC 20360
 Attn: ASW OIT

Commanding Officer
Naval Ocean Research and Development Activity
Department of the Navy
NSTL Station, MS 39529

- 17 Attn: S. Marshall, Code 340 18 G. Lewis, Code 500
- 19 20 Commanding Officer and Director
 Defense Documentation Center
 Cameron Station, Building 5
 5010 Duke Street
 Alexandria, VA 22314
 - TRW, INC.
 TRW Defense and Space Systems Group
 Washington Operation
 7600 Colshire Drive
 McLean, VA 22101
 Attn: W. Morley
 - 22 Sanders Associates, Inc. 95 Canal Street Nashua, NH 03606 Attn: L. Gagne
 - 23 Office of Naval Research Resident Representative Room 508, Federal Building Austin, TX 78701
 - 24 Glen E. Ellis, ARL:UT
 - 25 Loyd D. Hampton, ARL:UT

SECRET

SECRET

UNCLASSIFIED

(This page is unclassified)

Dist. List for ARL-TR-78-3 under Contract NOO039-77-C-0003, Items 0003 and 0004 (Cont'd)

Copy No.

- 15 Commanding Officer Naval Intelligence Support Center 4301 Suitland Road Washington, DC 20390 Attn: Code 222
- 16 Project Manager Anti-Submarine Warfare Systems Project Office Department of the Navy Washington, DC 20360 Attn: ASW 01T

Commanding Officer Naval Ocean Research and Development Activity Department of the Navy NSTL Station, MS 39529

- 17 Attn: S. Marshall, Code 340 18 G. Lewis, Code 500
- 19 20Commanding Officer and Director Defense Documentation Center Cameron Station, Building 5 5010 Duke Street Alexandria, VA 22314
 - 21 TRW, INC. TRW Defense and Space Systems Group Washington Operation 7600 Colshire Drive McLean, VA 22101 Attn: W. Morley
 - 22 Sanders Associates, Inc. 95 Canal Street Nashua, NH 03606 Attn: L. Gagne
 - 23 Office of Naval Research Resident Representative Room 508, Federal Building Austin, TX 78701
 - 24 Glen E. Ellis, ARL:UT
 - 25 Loyd D. Hampton, ARL:UT

SECRET

SECRET

(This page is UNCLASSIFIED.)

Dist. List for ARL-TR-78-3 under Contract NOOO39-77-C-0003, Items 0003 and 0004 (Cont*d)

Copy No.

30

Kenneth E. Hawker, ARL:UT
Stephen K. Mitchell, ARL:UT
Clark S. Penrod, ARL:UT
Jack A. Shooter, ARL:UT

Library, ARL:UT



DEPARTMENT OF THE NAVY

OFFICE OF NAVAL RESEARCH 875 NORTH RANDOLPH STREET SUITE 1425 ARLINGTON VA 22203-1995

IN REPLY REFER TO:

5510/1 Ser 321OA/011/06 31 Jan 06

MEMORANDUM FOR DISTRIBUTION LIST

Subj: DECLASSIFICATION OF LONG RANGE ACOUSTIC PROPAGATION PROJECT (LRAPP) DOCUMENTS

Ref:

(a) SECNAVINST 5510.36

Encl: (1) List of DECLASSIFIED LRAPP Documents

- 1. In accordance with reference (a), a declassification review has been conducted on a number of classified LRAPP documents.
- 2. The LRAPP documents listed in enclosure (1) have been downgraded to UNCLASSIFIED and have been approved for public release. These documents should be remarked as follows:

Classification changed to UNCLASSIFIED by authority of the Chief of Naval Operations (N772) letter N772A/6U875630, 20 January 2006.

DISTRIBUTION STATEMENT A: Approved for Public Release; Distribution is unlimited.

3. Questions may be directed to the undersigned on (703) 696-4619, DSN 426-4619.

BRIAN LINK

By direction

Subj: DECLASSIFICATION OF LONG RANGE ACOUSTIC PROPAGATION PROJECT (LRAPP) DOCUMENTS

DISTRIBUTION LIST:

NAVOCEANO (Code N121LC - Jaime Ratliff)

NRL Washington (Code 5596.3 – Mary Templeman)

PEO LMW Det San Diego (PMS 181)

DTIC-OCQ (Larry Downing)

ARL, U of Texas

Blue Sea Corporation (Dr.Roy Gaul)

ONR 32B (CAPT Paul Stewart)

ONR 321OA (Dr. Ellen Livingston)

APL, U of Washington

APL, Johns Hopkins University

ARL, Penn State University

MPL of Scripps Institution of Oceanography

WHOI

NAVSEA

NAVAIR

NUWC

SAIC

ENCL (1)

Declassified LRAPP Documents

				,		
Report Number	Personal Author	Title	Fublication Source (Originator)	rub. Date	Current Availability	Class.
Unavailable	Penrod, C. S., et al.	MOORED SURVEILLANCE SYSTEM FIELD VALIDATION TEST SENSOR PERFORMANCE ANALYSIS. VOLUME I. DATA COLLECTION AND MESUREMENT SYSTEM DESCRIPTION	University of Texas, Applied Research Laboratories	781231	ADC018009	C
Unavailable	Watkins, S. L., et al.	MOORED SURVEILLANCE SYSTEM FIELD VALIDATION TEST SENSOR PERFORMANCE ANALYSIS. VOLUME III. VERNIER RESOLUTION DATA PRODUCTS	University of Texas, Applied Research Laboratories	781231	ADC018373	C
Unavailable	Watkins, S. L., et al.	MOORED SURVEILLANCE SYSTEM FIELD VALIDATION TEST SENSOR PERFORMANCE ANALYSIS. VOLUME II. STANDARD RESOLUTION DATA PRODUCTS	University of Texas, Applied Research Laboratories	781231	ADC018374	C
NORDATN44	Bucca, P. J.	ENVIRONMENTAL VARIABILITY DURING THE CHURCH STROKE II CRUISE FIVE EXERCISE (U)	Naval Ocean R&D Activity	790201	ADC020353; NS; AU: ND	C
NADC7820830	Balonis, R. M.	TEST STEERED VERTICAL LINE ARRAY (TSVLA) MEASUREMENTS FOR BEARING STAKE SURVEYS (U)	Naval Air Systems Command	790301	ADC018003; NS;	C
USIControl674779	Williams, W., et al.	REPORT OF THE LRAPP EXERCISE PLANNING WORKSHOP TRACOR INC ROCKVILLE MD 16 - 17 OCTOBER 1978 (U)	Underwater Systems, Inc.	790302	NS; ND	C
NOSCTR357	Hamilton, E. L., et al.	GEOACOUSTIC MODELS OF THE SEAFLOOR: GULF OF OMAN, ARABIAN SEA, AND SOMALI BASIN (U)	Naval Ocean Systems Center	790615	QN	C
Unavailable	Unavailable	RAPIDLY DEPLOYABLE SURVEILLANCE SYST (RDSS) ACOUSTIC VALIDATION TEST (AVT) EXERCISE PLAN (U)	Naval Electronic Systems Command	790625	AU	C
LRAPPRC79027	Brunson, B. A., et al.	GULF OF MEXICO AND CARIBBEAN SEA DATA AND MODEL BASE REPORT (U)	Tracor, Inc.	790701	ADC019153; NS; ND	C
Unavailable	Unavailable	BEARING STAKE BMS DATA QUALITY ASSESSMENT REPORT (U)	University of Texas, Applied Research Laboratories	790705	AU	C
PME12430	Unavailable	RAPIDLY DEPLOYABLE SURVEILLANCE SYSTEM (RDSS) ACOUSTIC VALIDATION TEST (AVT) DATA REDUCTION AND ANALYSIS PLAN (U)	Naval Electronic Systems Command	790815	NS; AU	C
Unavailable	Unavailable	RAPIDLY DEPLOYABLE SURVEILLANCE SYSTEM (RDSS) ACOUSTIC VALIDATION TEST (AVT) EXERCISE PLAN (U)	Naval Electronic Systems Command	790917	AU	C
NOSCTR467	Pedersen, M. A., et al.	PROPAGATION LOSS ASSESSMENT OF THE BEARING STAKE EXERCISE (U)	Naval Ocean Systems Center	790928	ADC020845; NS; AU; ND	C
NOSCTR466	Anderson, A. L., et al.	BEARING STAKE ACOUSTIC ASSESSMENT (U)	Naval Ocean Systems Center	790928	ADC020797; NS; AU; ND	С